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Crystal structure of *N*-(2-{[2,6-bis(2,2,2-trifluoroacetamido)phenyl]disulfanyl}-3-(2,2,2-trifluoroacetamido)phenyl)-2,2,2-trifluoroacetamide

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The title compound, $C_{20}H_{10}F_{12}N_4O_4S_2$, is an organic diaryl disulfide compound with trifluoroacetamide substituents at the *ortho*-positions of each benzene ring. There are two molecules (labeled A and B) in the asymmetric unit. The F atoms of three of the $-CF_3$ groups exhibit rotational disorder over two positions each. The S–S bond distances are 2.0914 (7) and 2.0827 (6) Å for molecules A and B, respectively. The dihedral angle between the S–S–C and S–C–C planes is 103.05 (15)° for molecule A and 104.09 (15)° for molecule B. The three-dimensional supramolecular architecture of the crystal is sustained by numerous N–H···O, N–H···S and C–H···O interactions.

Keywords: crystal structure; diaryl disulfide; S—S bonds; N—H···S interactions; N—H···F interactions; C—H···O interactions..

CCDC reference: 1415414

1. Related literature

For the synthesis of dithiobis(*N*-phenylamide) compounds, see: Ueyama *et al.* (1995); Lumb *et al.* (2014). For related crystal structures, see: Ueyama *et al.* (1995); Raftery *et al.* (2009). For applications of the title compound and related compounds, see: Klingele *et al.* (2013); Xu *et al.* (2006); Enemark & Cooney (2004); Yu *et al.* (2008); Smith *et al.* (2005); Ueyama *et al.* (1995, 1998); Reichardt *et al.* (2003); Dance (1986).



2. Experimental

2.1. Crystal data

 $C_{20}H_{10}F_{12}N_4O_4S_2$ $M_r = 662.44$ Monoclinic, $P2_1/n$ a = 19.0538 (10) Å b = 13.1466 (7) Å c = 19.961 (1) Å $\beta = 96.0042$ (9)°

2.2. Data collection

Bruker APEX CCD diffractometer
Absorption correction: multi-scan
(SADABS; Bruker, 2002)
$T_{\rm min} = 0.808, T_{\rm max} = 0.954$

2.3. Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.047$ $wR(F^2) = 0.135$ S = 1.0012375 reflections 865 parameters 393 restraints 91119 measured reflections 12375 independent reflections 10553 reflections with $I > 2\sigma(I)$

V = 4972.7 (4) Å³

Mo $K\alpha$ radiation

 $0.65 \times 0.25 \times 0.14 \text{ mm}$

 $\mu = 0.34 \text{ mm}^-$

T = 100 K

 $R_{\rm int} = 0.033$

Z = 8

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H atoms treated by a mixture of
independent and constrained
refinement
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$$\Delta \rho_{\rm max} = 1.37 \ {\rm e} \ {\rm \AA}^{-3}$$

 $\Delta \rho_{\rm min} = -1.09 \text{ e } \text{\AA}^{-3}$

Table 1Hydrogen-bond geometry (Å, °).

$D - H \cdot \cdot \cdot A$	D-H	$H \cdot \cdot \cdot A$	$D \cdot \cdot \cdot A$	$D - \mathbf{H} \cdot \cdot \cdot A$
$N1A - H1AN \cdots O4B$	0.89 (3)	2.19 (3)	2.988 (2)	149 (2)
$N2A - H2AN \cdot \cdot \cdot S1A$	0.84(3)	2.42 (3)	2.9425 (18)	121 (2)
$N2A - H2AN \cdots S2A$	0.84(3)	2.96 (3)	3.4543 (18)	120 (2)
$N3A - H3AN \cdots O1A^{i}$	0.84(3)	2.12(3)	2.857 (2)	146 (2)
$C5A - H5A \cdots O2A$	0.95	2.34	2.952 (3)	122
$C13A - H13A \cdots F5B'^{ii}$	0.95	2.54	3.207 (4)	127
$C15A - H15A \cdots O4A$	0.95	2.25	2.883 (3)	123
$N1B - H1BN \cdot \cdot \cdot O2A^{iii}$	0.80(3)	2.42 (3)	2.983 (2)	128 (2)
$N3B - H3BN \cdots O1B^{iv}$	0.79 (3)	2.24 (3)	2.848 (2)	135 (3)
$N4B - H4BN \cdot \cdot \cdot O3B^{iv}$	0.85 (3)	2.47 (3)	3.032 (2)	125 (2)
$C5B - H5B \cdots O2B$	0.95	2.27	2.896 (3)	122
$C15B - H15B \cdots O3A$	0.95	2.56	3.229 (3)	128
$C15B - H15B \cdots O4B$	0.95	2.27	2.898 (3)	123
Symmetry codes: (i)	$-x + \frac{1}{2}, y - \frac{1}{2}$	$, -z + \frac{1}{2};$ (ii	$) -x + \frac{3}{2}, y - \frac{1}{2},$	$-z + \frac{1}{2};$ (iii)

 $x + \frac{1}{2}, -y + \frac{3}{2}, z - \frac{1}{2}$; (iv) $-x + \frac{3}{2}, y + \frac{1}{2}, -z + \frac{1}{2}$.

Data collection: *SMART* (Bruker, 2007); cell refinement: *SAINT*; data reduction: *SAINT* (Bruker, 2007); program(s) used to solve structure: *SHELXS* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL2014* (Sheldrick, 2015); molecular graphics: *SHELXL2002*; software used to prepare material for publication: *SHELXL2014*.

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Supporting information for this paper is available from the IUCr electronic archives (Reference: HB7457).

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Crystal structure of *N*-(2-{[2,6-bis(2,2,2-trifluoroacetamido)phenyl]disulfanyl}-3-(2,2,2-trifluoroacetamido)phenyl)-2,2,2-trifluoroacetamide

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S1. Introduction

Thiolate coordination to metal centers are common in metalloproteins (Enemark *et al.*, 2004), and several crystal structures of thiolate complexes are known (Klingele *et al.*, 2013; Dance, 1986). Further, dithio-bis-*N*-phenyl compounds such as the title compound, C₂₀H₁₀F₁₂N₄O₄S₂, have often been used as precursors for the synthesis of metal thiolate complexes (Yu *et al.*, 2008; Smith *et al.*, 2005; Ueyama *et al.*, 1998; Ueyama *et al.*, 1996; Xu *et al.*, 2006). Only a handful of crystal structures of dithio-bis-*N*-phenylamide compounds are known (Ueyama *et al.*, 1995; Raftery *et al.*, 2009). We now report the crystal structure of the known compound 2,2'-dithio-bis(N-phenyl-2,2,2-trifluoroacetamide) (Ueyama *et al.*, 1998; Ueyama, *et al.*, 1995) (Fig. 1). There are two formula units (molecule A and molecule B) per asymmetric unit of the cell. The S–S bond distances are 2.0914 (7) Å for molecule A, and 2.0827 (6) Å, for molecule B. The dihedral angles between the S–S–C planes and the S–C–C planes are 103.05 (15) ° for molecule A, and 104.09 (15) ° for molecule B.

S2. Experimental

The title compound, $C_{20}H_{10}F_{12}N_4O_4S_2$, was prepared as reported in the literature (Ueyama *et al.*, 1998; Ueyama, *et al.*, 1995) to give 90% isolated yield of the yellow product. IR (KBr, cm⁻¹): $v_{NH} = 3362$, 3335; $v_{CO} = 1741$, 1730. ¹⁹F NMR (CDCl₃, ppm): δ –75.61 (s, *CF*₃). ¹H NMR (CDCl₃, ppm): δ 8.59 (s, 4H, N*H*); 8.21 (d, *J* = 8.7 Hz, 4H, phenyl-*H*); 7.62 (t, *J* = 8.7 Hz, 2H, phenyl-*H*). Single crystals of the compound were obtained by a slow evaporation of a methylene chloride/ hexane (2:1) solution of the compound.

S3. Refinement

H atoms were located geometrically and refined using a riding model on their parent atoms, with C-H = 0.95 Å for aromatic, with $U_{iso}(H) = 1.2-1.5U_{eq}(C)$. The F atoms of three of the CF₃ groups exhibit rotational disorder over two positions each. The occupancies of atoms F4A - F6A were refined to 0.538 (10) and 0.462 (10) for the unprimed and primed atoms. The occupancies of atoms F10A – F12A were refined to 0.509 (7) and 0.491 (7) for the A and C labeled atoms. The occupancies of atoms F4B – F6B were refined to 0.658 (7) and 0.342 (7) for the unprimed and primed atoms. Restraints on the positional and displacement parameters of the disordered atoms were required. The final difference map had maxima and minima of 1.375 and -1.087 e/Å³, respectively, which were located close to the disordered F atoms. Specifically, the largest peak was located close to F12A and the smallest hole was located close to F12C.



Figure 1

The molecular structure of the title compound, showing displacement ellipsoids drawn at the 50% probability level. Aromatic H atoms and disordered groups have been omitted for clarity.



Figure 2

The packing diagram.

 $N-(2-\{[2,6-Bis(2,2,2-trifluoroacetamido) phenyl] disulfanyl\}-3-(2,2,2-trifluoroacetamido) phenyl)-2,2,2-trifluoroacetamido) phenyl] disulfanyl\}-3-(2,2,2-trifluoroacetamido) phenyl] disulfanyl\}-3-(2,2,2-trifluoroacetamido) phenyl] disulfanyl] di$

trifluoroacetamide

Crystal data

 $C_{20}H_{10}F_{12}N_4O_4S_2$ $M_r = 662.44$ Monoclinic, $P2_1/n$ a = 19.0538 (10) Å b = 13.1466 (7) Å c = 19.961 (1) Å $\beta = 96.0042$ (9)° V = 4972.7 (4) Å³ Z = 8 F(000) = 2640 $D_x = 1.770 \text{ Mg m}^{-3}$ Mo $K\alpha$ radiation, $\lambda = 0.71073 \text{ Å}$ Cell parameters from 7979 reflections $\theta = 2.6-28.2^{\circ}$ $\mu = 0.34 \text{ mm}^{-1}$ T = 100 KPrism, black $0.65 \times 0.25 \times 0.14 \text{ mm}$ Data collection

Bruker APEX CCD diffractometer φ and ω scans Absorption correction: multi-scan (<i>SADABS</i> ; Bruker, 2002) $T_{\min} = 0.808, T_{\max} = 0.954$ 91119 measured reflections	12375 independent reflections 10553 reflections with $I > 2\sigma(I)$ $R_{int} = 0.033$ $\theta_{max} = 28.3^\circ$, $\theta_{min} = 1.4^\circ$ $h = -25 \rightarrow 25$ $k = -17 \rightarrow 17$ $l = -26 \rightarrow 26$
Refinement	
Refinement on F^2	Hydrogen site location: mixed
Least-squares matrix: full	H atoms treated by a mixture of independent
$R[F^2 > 2\sigma(F^2)] = 0.047$	and constrained refinement
$wR(F^2) = 0.135$	$w = 1/[\sigma^2(F_o^2) + (0.076P)^2 + 6.P]$
S = 1.00	where $P = (F_o^2 + 2F_c^2)/3$
12375 reflections	$(\Delta/\sigma)_{\rm max} = 0.012$
865 parameters	$\Delta \rho_{\rm max} = 1.37 \ { m e} \ { m \AA}^{-3}$
393 restraints	$\Delta \rho_{\min} = -1.09 \text{ e } \text{\AA}^{-3}$
Special details	

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $(Å^2)$

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	Occ. (<1)
S1A	0.19690 (2)	0.84332 (4)	0.20932 (2)	0.02061 (10)	
S2A	0.20039 (2)	0.68776 (4)	0.23136 (2)	0.02119 (10)	
F1A	0.23377 (7)	0.89398 (14)	0.02002 (7)	0.0434 (4)	
F2A	0.30695 (9)	1.01596 (12)	0.00909 (7)	0.0431 (4)	
F3A	0.34531 (7)	0.86410 (11)	0.03116 (7)	0.0357 (3)	
F4A	0.0781 (2)	0.8272 (5)	0.36999 (16)	0.0461 (11)	0.538 (10)
F5A	0.0872 (3)	0.8762 (5)	0.4716 (3)	0.0753 (15)	0.538 (10)
F6A	0.1246 (3)	0.7287 (3)	0.4482 (4)	0.0715 (16)	0.538 (10)
F4A'	0.0882 (3)	0.7822 (7)	0.3719 (2)	0.0701 (17)	0.462 (10)
F5A'	0.1213 (3)	0.7535 (4)	0.4753 (3)	0.0546 (14)	0.462 (10)
F6A'	0.0761 (3)	0.8950 (3)	0.4463 (4)	0.0617 (14)	0.462 (10)
F7A	0.42433 (8)	0.74860 (13)	0.45323 (7)	0.0437 (4)	
F8A	0.39524 (10)	0.59029 (12)	0.45287 (8)	0.0501 (4)	
F9A	0.31648 (7)	0.70381 (10)	0.42694 (6)	0.0302 (3)	
F10A	0.1024 (3)	0.6932 (5)	-0.07119 (14)	0.0464 (13)	0.509(7)
F11A	0.0700(2)	0.6129 (5)	0.0155 (3)	0.0885 (17)	0.509 (7)
F12A	0.09429 (19)	0.7685 (3)	0.0215 (2)	0.0633 (13)	0.509 (7)
F10C	0.1026 (3)	0.7185 (5)	-0.06545 (18)	0.0508 (14)	0.491 (7)
F11C	0.0893 (2)	0.5786 (3)	-0.0144 (2)	0.0672 (13)	0.491 (7)
F12C	0.0773 (2)	0.7136 (6)	0.0395 (2)	0.0849 (16)	0.491 (7)
01A	0.25566 (9)	1.02169 (12)	0.13452 (8)	0.0315 (3)	
O2A	0.22941 (8)	0.89280 (12)	0.47115 (7)	0.0281 (3)	

O3A	0.45890 (9)	0.68634 (17)	0.33375 (9)	0.0423 (4)	
O4A	0.23430 (10)	0.64932 (16)	-0.02549(8)	0.0431 (4)	
N1A	0.33815 (9)	0.89887 (13)	0.16183 (8)	0.0227 (3)	
H1AN	0.3731 (14)	0.862 (2)	0.1483 (13)	0.027*	
N2A	0.20760 (9)	0.87028 (14)	0.35637 (9)	0.0234 (3)	
H2AN	0.1753 (15)	0.854 (2)	0.3262 (14)	0.028*	
N3A	0.34280 (9)	0.64515 (13)	0.30362 (8)	0.0226 (3)	
H3AN	0.3053 (15)	0.633 (2)	0.3209 (13)	0.027*	
N4A	0.20769 (10)	0.66134 (15)	0.08449 (9)	0.0276 (4)	
H4AN	0.1734 (16)	0.673 (2)	0.1056 (15)	0.033*	
CIA	0 27294 (10)	0.88575(14)	0 26082 (9)	0.0199(3)	
C2A	0.27291(10) 0.33560(10)	0.000799(11)	0.23293(10)	0.0216(4)	
C3A	0 39579 (11)	0.93739 (16)	0.23233(11)	0.0269(4)	
НЗА	0.4382	0.95739 (10)	0.2545	0.0209 (1)	
C4A	0.39344 (11)	0.9322	0.34279 (11)	0.032	
	0.4348	0.94497 (17)	0.3706	0.034*	
C54	0.33101 (11)	0.9040	0.3700 0.37207 (10)	0.034 0.0247 (4)	
U5A	0.3309	0.92556 (15)	0.4194	0.0247 (4)	
C6A	0.3307 0.27135 (10)	0.89603 (14)	0.33090(10)	0.030 0.0207 (4)	
	0.27133(10) 0.29602(10)	0.09003(14)	0.11896 (10)	0.0207(4)	
	0.29648(11)	0.93193(18)	0.04348(11)	0.0241(4) 0.0285(4)	
	0.29048(11) 0.10261(11)	0.95195 (18)	0.04348(11) 0.42072(10)	0.0283(4)	
	0.19201(11) 0.11802(12)	0.80097(15)	0.42072(10)	0.0244(4)	
CIUA	0.11892(12) 0.27654(10)	0.62341(10)	0.42730(9) 0.10208(10)	0.0305(3)	
CI2A	0.27034(10) 0.24000(10)	0.03281(14)	0.19298(10)	0.0200(4)	
C12A	0.34090(10) 0.40107(11)	0.03000(14)	0.23209(10) 0.20217(10)	0.0207(4)	
	0.40107 (11)	0.01034 (10)	0.20217 (10)	0.0248 (4)	
HI3A CI4A	0.4444	0.5908	0.2287	0.030^{*}	
UI4A	0.39672 (12)	0.60491 (16)	0.13240 (11)	0.0279 (4)	
HI4A	0.4381	0.5891	0.1118	0.033^{*}	
CI5A	0.33420 (12)	0.62171 (16)	0.09191 (11)	0.02//(4)	
HISA	0.3328	0.61//	0.0443	0.033*	
CI6A	0.2/341(11)	0.64465 (15)	0.12229 (10)	0.0232(4)	
CI/A	0.39951 (11)	0.6/082 (16)	0.34650 (10)	0.0250 (4)	
CI8A	0.38331 (12)	0.67836 (17)	0.42094 (11)	0.0288 (4)	
C19A	0.19369 (13)	0.66172 (19)	0.01649 (11)	0.0354 (5)	
C20A	0.11558 (16)	0.6769 (2)	-0.00550 (10)	0.0597 (8)	
SIB	0.76647 (2)	0.76045 (4)	0.08659 (2)	0.01966 (10)	
S2B	0.76118 (2)	0.85065 (3)	0.17168 (2)	0.01906 (10)	
F1B	0.57541 (7)	0.59534 (12)	0.09799 (9)	0.0438 (4)	
F2B	0.57993 (9)	0.44061 (15)	0.06322 (10)	0.0607 (5)	
F3B	0.55214 (8)	0.47312 (16)	0.16212 (10)	0.0610 (5)	
F4B	0.94973 (17)	0.9556 (3)	0.0933 (2)	0.0350 (8)	0.658 (7)
F5B	0.9957 (2)	0.9478 (2)	0.19691 (12)	0.0541 (9)	0.658 (7)
F6B	1.06209 (11)	0.9342 (2)	0.1184 (2)	0.0579 (10)	0.658 (7)
F4B′	0.9405 (3)	0.9559 (5)	0.1081 (4)	0.0391 (18)	0.342 (7)
F5B'	1.0320 (4)	0.9589 (4)	0.1824 (3)	0.0731 (18)	0.342 (7)
F6B′	1.0413 (4)	0.9165 (4)	0.0809 (4)	0.0782 (18)	0.342 (7)
F7B	0.95251 (7)	0.75811 (11)	0.28940 (7)	0.0338 (3)	

F8B	0.94940 (8)	0.70254 (12)	0.39064 (7)	0.0394 (3)
F9B	0.98062 (7)	0.60249 (12)	0.31369 (8)	0.0405 (3)
F10B	0.57446 (7)	0.96551 (14)	0.05725 (8)	0.0468 (4)
F11B	0.46691 (7)	0.97928 (10)	0.07994 (7)	0.0337 (3)
F12B	0.49804 (7)	0.85087 (12)	0.02331 (7)	0.0392 (3)
O1B	0.68797 (8)	0.43192 (12)	0.18963 (8)	0.0310 (3)
O2B	1.03946 (8)	0.74409 (13)	0.16381 (10)	0.0368 (4)
O3B	0.84306 (9)	0.55663 (12)	0.32275 (10)	0.0395 (4)
O4B	0.48416 (8)	0.81527 (13)	0.16359 (8)	0.0315 (3)
N1B	0.71462 (9)	0.55321 (14)	0.11416 (9)	0.0241 (3)
H1BN	0.6955 (14)	0.587 (2)	0.0841 (14)	0.029*
N2B	0.92272 (9)	0.76337 (13)	0.12265 (9)	0.0233 (3)
H2BN	0.8947 (15)	0.808 (2)	0.1056 (13)	0.028*
N3B	0.81672 (9)	0.71875 (14)	0.28596 (9)	0.0236 (3)
H3BN	0.8331 (15)	0.772 (2)	0.2790 (13)	0.028*
N4B	0.60340 (9)	0.84012 (13)	0.15931 (9)	0.0225 (3)
H4BN	0.6307 (14)	0.880 (2)	0.1408 (13)	0.027*
C1B	0.81979 (10)	0.65657 (14)	0.11839 (9)	0.0196 (3)
C2B	0.78839 (10)	0.56231 (15)	0.12953 (9)	0.0205 (4)
C3B	0.82932 (11)	0.47958 (15)	0.15394 (10)	0.0244 (4)
H3B	0.8080	0.4158	0.1612	0.029*
C4B	0.90147 (11)	0.49212 (16)	0.16734 (11)	0.0278 (4)
H4B	0.9295	0.4360	0.1840	0.033*
C5B	0.93418 (11)	0.58450 (16)	0.15708 (11)	0.0263 (4)
H5B	0.9838	0.5914	0.1669	0.032*
C6B	0.89356 (10)	0.66657 (15)	0.13236 (10)	0.0216 (4)
C7B	0.67175 (11)	0.49148 (15)	0.14464 (10)	0.0230 (4)
C8B	0.59362 (12)	0.49961 (18)	0.11635 (13)	0.0336 (5)
C9B	0.98979 (10)	0.79415 (16)	0.14079 (10)	0.0258 (4)
C10B	0.99935 (9)	0.90797 (19)	0.13293 (11)	0.0434 (6)
C11B	0.70913 (10)	0.77559 (14)	0.22181 (10)	0.0202 (3)
C12B	0.74232 (10)	0.71432 (15)	0.27340 (10)	0.0220 (4)
C13B	0.70246 (12)	0.65474 (16)	0.31323 (11)	0.0279 (4)
H13B	0.7249	0.6118	0.3473	0.033*
C14B	0.62966 (12)	0.65928 (17)	0.30223 (11)	0.0293 (4)
H14B	0.6024	0.6191	0.3295	0.035*
C15B	0.59506 (11)	0.72048 (16)	0.25274 (10)	0.0254 (4)
H15B	0.5450	0.7229	0.2466	0.030*
C16B	0.63503 (10)	0.77851 (14)	0.21210 (10)	0.0209 (4)
C17B	0.85908 (11)	0.64340 (16)	0.31062 (10)	0.0255 (4)
C18B	0.93663 (12)	0.67737 (17)	0.32606 (11)	0.0287 (4)
C19B	0.53419 (10)	0.85090 (15)	0.13889 (10)	0.0225 (4)
C20B	0.51895 (11)	0.91349 (18)	0.07366 (10)	0.0273 (4)

Atomic displacement parameters $(Å^2)$

	U^{11}	U ²²	U^{33}	U^{12}	U^{13}	<i>U</i> ²³
S1A	0.0177 (2)	0.0242 (2)	0.0198 (2)	0.00157 (16)	0.00127 (16)	-0.00039 (16)

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S2A	0.0180 (2)	0.0237 (2)	0.0220 (2)	-0.00232 (17)	0.00287 (16)	-0.00006 (17)
F1A	0.0276 (7)	0.0669 (10)	0.0350 (7)	-0.0050 (7)	-0.0001 (6)	-0.0083 (7)
F2A	0.0544 (9)	0.0457 (8)	0.0314 (7)	0.0047 (7)	0.0155 (6)	0.0133 (6)
F3A	0.0334 (7)	0.0455 (8)	0.0289 (7)	0.0092 (6)	0.0060 (5)	-0.0061 (6)
F4A	0.0219 (14)	0.077 (3)	0.0389 (16)	-0.0043 (16)	0.0008 (11)	0.0146 (15)
F5A	0.059 (2)	0.121 (3)	0.053 (3)	-0.016 (2)	0.038 (2)	-0.023(2)
F6A	0.055 (2)	0.068 (2)	0.088 (3)	-0.0292 (19)	-0.010(2)	0.033 (2)
F4A′	0.039 (2)	0.130 (4)	0.042 (2)	-0.039 (3)	0.0065 (17)	-0.018(2)
F5A'	0.0361 (19)	0.066 (3)	0.059 (3)	-0.0242(19)	-0.0043(19)	0.023 (2)
F6A'	0.040(2)	0.082(3)	0.068 (3)	0.0201 (19)	0.034 (2)	0.032(2)
F7A	0.0360(8)	0.0631(10)	0.0304(7)	-0.0060(7)	-0.0045(6)	-0.0148(7)
F8A	0.0771(12)	0.0432 (8)	0.0305(7)	0.0261 (8)	0.0079 (7)	0.0101 (6)
F9A	0.0316(7)	0.0339(7)	0.0260 (6)	0.0009(5)	0.0075(7)	-0.0031(5)
F10A	0.0510(7)	0.0333(1)	0.0260(0) 0.0267(17)	0.0325(18)	-0.0101(15)	-0.0094(14)
F11A	0.002(2)	0.140(4)	0.0207(17)	-0.026(2)	-0.013(2)	0.050(3)
F12A	0.010(2) 0.0270(17)	0.126(3)	0.078(2)	0.020(2)	0.013(2)	-0.022(2)
F10C	0.0270(17)	0.054(3)	0.0327(19)	0.024(2)	-0.0083(17)	-0.0022(2)
F11C	0.005(3)	0.031(3) 0.129(3)	0.0327(17)	-0.027(2)	-0.0018(15)	0.0099(17)
F12C	0.035(2)	0.129(3) 0.180(4)	0.036(2)	0.027(2)	0.0010(15)	-0.019(2)
014	0.030(2)	0.100(4)	0.030(2)	0.019(3)	0.0074 (6)	0.010(5)
024	0.0347(8)	0.0295(0)	0.0311(0) 0.0200(7)	-0.0013(6)	0.0074 (6)	-0.0015(6)
034	0.0347(8)	0.0293(7)	0.0200(7) 0.0340(9)	-0.0019(8)	0.0024(0) 0.0051(7)	-0.0121(8)
044	0.0251(0) 0.0459(10)	0.0704(13) 0.0608(12)	0.0340(9) 0.0224(8)	-0.0016(9)	0.0031(7)	-0.0057(8)
N1A	0.0703(8)	0.0000(12)	0.0224(8)	0.0010(0)	0.0020(7)	0.0057(0)
	0.0203(8)	0.0202(0)	0.0224(8)	-0.0023(0)	0.0037 (0)	-0.0003(0)
N2A	0.0193(8)	0.0322(9)	0.0189(8) 0.0202(8)	-0.0009(7)	0.0023(0)	0.0024(0)
NJA NJA	0.0197(8)	0.0282(8) 0.0331(0)	0.0202(8)	-0.0007(0)	0.0039(0)	-0.0012(0)
C1A	0.0281(9)	0.0331(9)	0.0211(8)	0.0003(7)	0.0009(7)	-0.0019(7)
	0.0130(8)	0.0195(8)	0.0210(9)	0.0013(7)	0.0011(7)	0.0000(7)
C2A C2A	0.0217(9)	0.0200(8)	0.0229(9)	-0.0012(7)	0.0047(7)	0.0014(7)
CIA	0.0200(9)	0.0299(10)	0.0303(10)	-0.0044(8)	0.0032(8)	0.0019(8)
C4A	0.0244(10)	0.0294(10)	0.0293(10)	-0.0003(8)	-0.0020(8)	0.0001(8)
CSA	0.0270(10)	0.0229 (9)	0.0239(9)	-0.0024(7)	0.0009(7)	-0.0012(7)
COA	0.0200 (8)	0.0195(8)	0.0229 (9)	0.0013(7)	0.0032(7)	0.0002 (7)
C/A	0.0218(9)	0.0258(9)	0.0254(9)	0.0000(7)	0.0061(7)	0.0022(7)
C8A	0.0238 (10)	0.0366 (11)	0.0256 (10)	0.0020 (8)	0.0053 (8)	0.0024 (8)
C9A	0.0251(9)	0.0268(9)	0.0219(9)	0.0027(8)	0.0050(7)	-0.0005(7)
CIUA	0.0268 (11)	0.05/3(14)	0.0261 (10)	-0.0036 (10)	0.0061 (8)	0.0018 (10)
CIIA	0.0204 (9)	0.0192 (8)	0.0226 (9)	-0.0012 (7)	0.0047(7)	-0.0001 (/)
CI2A CI2A	0.0216 (9)	0.0194 (8)	0.0216 (9)	-0.0018(7)	0.0045 (7)	0.0002 (7)
CI3A	0.0225 (9)	0.0254 (9)	0.0269 (10)	0.0018 (7)	0.0048 (7)	-0.0004 (8)
CI4A	0.0277 (10)	0.0277 (10)	0.0299 (10)	0.0014 (8)	0.0106 (8)	-0.0025 (8)
CI5A	0.0342 (11)	0.0273 (10)	0.0226 (9)	0.0002 (8)	0.0074 (8)	-0.0028 (8)
Cl6A	0.0268 (10)	0.0200 (9)	0.0225 (9)	-0.0023(7)	0.0009 (7)	-0.0020 (7)
C17A	0.0225 (9)	0.0294 (10)	0.0230 (9)	0.0024 (8)	0.0015 (7)	-0.0011 (8)
C18A	0.0306 (11)	0.0309 (10)	0.0244 (10)	0.0058 (8)	-0.0001 (8)	-0.0005 (8)
C19A	0.0388 (13)	0.0433 (13)	0.0231 (10)	-0.0036 (10)	-0.0019 (9)	-0.0022 (9)
C20A	0.0391 (14)	0.112 (3)	0.0264 (12)	-0.0073 (16)	-0.0034 (10)	-0.0018 (14)
S1B	0.0197 (2)	0.0210(2)	0.0182 (2)	0.00084 (16)	0.00150 (16)	0.00107 (16)

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S2B	0.0181 (2)	0.0179(2)	0.0214(2)	-0.00131 (16)	0.00369 (16)	-0.00046(16)
F1B	0.0259 (7)	0.0403 (8)	0.0630 (10)	0.0011 (6)	-0.0056 (6)	0.0145 (7)
F2B	0.0470 (10)	0.0589 (11)	0.0699 (12)	-0.0105 (8)	-0.0240(9)	-0.0159 (9)
F3B	0.0246 (7)	0.0814 (13)	0.0776 (13)	-0.0024(8)	0.0084 (7)	0.0411 (10)
F4B	0.0316 (13)	0.0272 (13)	0.0443 (17)	-0.0061(10)	-0.0050(13)	0.0079 (11)
F5B	0.070 (2)	0.0371(13)	0.0536 (15)	-0.0191(14)	-0.0006(13)	-0.0121(11)
F6B	0.0247(12)	0.0452(15)	0.101 (3)	-0.0127(10)	-0.0059(13)	0.0268 (16)
F4B'	0.037(3)	0.031(3)	0.050(3)	-0.001(2)	0.008(2)	-0.002(2)
F5B'	0.057(3)	0.031(3)	0.118 (4)	-0.013(2)	-0.037(3)	-0.012(3)
F6B'	0.047(3)	0.061(3)	0 130 (4)	-0.016(2)	0.022(3)	0.027(3)
F7B	0.0260(6)	0.001(3) 0.0369(7)	0.0373(7)	-0.0034(5)	-0.0021(5)	0.0104 (6)
F8B	0.0200(0) 0.0378(8)	0.0522(9)	0.0272(7)	-0.0071(6)	-0.0021(6)	0.0001 (6)
F9B	0.0370(0)	0.0322(9)	0.0202(7)	0.0125 (6)	-0.002(6)	0.0035 (6)
F10B	0.0301(7)	0.0736(11)	0.0170(0)	-0.0125(0)	-0.0023(6)	0.0035(0) 0.0275(7)
F11B	0.0200(7) 0.0342(7)	0.0328 (7)	0.0378(7)	0.0155(7)	-0.0027(5)	0.0275(7)
F12B	0.0342(7) 0.0325(7)	0.0520(7) 0.0570(9)	0.0320(7) 0.0267(7)	0.0034 (5)	-0.0027(5)	-0.0121(6)
01B	0.0323(7)	0.0376(8)	0.0207(7)	-0.0003(6)	0.0020(5)	0.0121(0)
01D 02B	0.0213(7)	0.0326(8)	0.0531(0)	-0.0009(6)	-0.0017(7)	0.0113(0)
02D 03B	0.0211(7) 0.0365(9)	0.0340(3) 0.0232(7)	0.0530(11) 0.0579(11)	0.0013(7)	0.0017(7)	0.0048(7) 0.0053(7)
03D 04B	0.0303(7)	0.0252(7)	0.0397 (9)	0.0013(7)	0.0001 (6)	0.0053(7)
N1B	0.0203(7)	0.0350 (8)	0.0397(9)	-0.0013(0)	-0.0034(0)	0.0103(7)
N2B	0.0204(8)	0.0200 (8)	0.0291(0)	-0.0017(0)	0.0029(0)	-0.0037(7)
N3B	0.0191(8) 0.0229(8)	0.0209(8)	0.0298(9) 0.0254(8)	-0.0003(0)	0.0020(0)	0.0013(0)
N/B	0.0225(0)	0.0220(8)	0.0234(8)	-0.0038(6)	0.0007(0)	0.0035 (6)
C1R	0.0189(7)	0.0203(8)	0.0230(8)	0.0038(0)	0.0032(0)	-0.0005(0)
C1B C2B	0.0109(0)	0.0208(8) 0.0227(9)	0.0187(8)	0.0023(7)	0.0013(7)	-0.0005(0)
C2D C2P	0.0201(9)	0.0227(9)	0.0137(3)	0.0000(7)	0.0013(7)	0.0003(7)
CJB C/B	0.0243(9)	0.0207(9)	0.0278(10) 0.0346(11)	0.0012(7)	0.0009(8)	0.0008(7)
C4D C5P	0.0231(10)	0.0232(9)	0.0340(11)	0.0049(8)	0.0009(8)	-0.0003(8)
C5B C6B	0.0200(9)	0.0239(10)	0.0328(10)	-0.0029(7)	0.0013(8) 0.0032(7)	-0.0038(8)
C0D C7P	0.0208(9)	0.0221(9)	0.0223(9)	-0.0004(7)	0.0032(7)	-0.0027(7)
	0.0233(3)	0.0213(9) 0.0238(11)	0.0242(9)	-0.0017(7)	-0.0013(7)	0.0011(7)
COR	0.0247(10)	0.0338(11) 0.0278(10)	0.0412(12) 0.0287(10)	-0.0009(9) -0.0023(8)	-0.0017(9)	-0.0020(8)
C10D	0.0209(9)	0.0278(10) 0.0307(11)	0.0287(10)	-0.0023(8)	-0.0050(7)	0.0029(8)
CIUD	0.0230(11)	0.0307(11) 0.0187(8)	0.0710(17)	-0.0007(9) -0.0025(7)	-0.0033(11)	-0.0020(11)
C12P	0.0208(9)	0.0187(8)	0.0210(9)	-0.0023(7)	0.0043(7)	-0.0017(7)
C12D C12P	0.0224(9)	0.0213(9) 0.0278(10)	0.0223(9)	-0.0009(7)	0.0024(7)	-0.0018(7)
C14D	0.0310(11)	0.0278(10)	0.0231(10)	-0.0056(8)	0.0039(8)	0.0039(8)
C14D	0.0297(11) 0.0228(0)	0.0310(10)	0.0283(10)	-0.0030(8)	0.0091(3)	-0.0007(8)
C16D	0.0228(9)	0.0277(10)	0.0204(10)	-0.0037(8)	0.0038(7)	-0.0018(7)
C10D C17D	0.0214(9)	0.0207(8)	0.0208(9)	-0.0012(7)	0.0029(7)	-0.0018(7)
	0.0209(10)	0.0242(9)	0.0249 (9)	0.0012(8)	0.0000(8)	-0.0010(7)
CIOD	0.0203(10)	0.0293(10)	0.0273(10)	0.0025(8)	0.0033(8)	-0.0039(8)
COD	0.0209(9)	0.0223(9) 0.0277(11)	0.0244(9)	-0.0003(7)	0.0024(7)	-0.0023(7)
C20B	0.0197 (9)	0.0377(11)	0.0244 (10)	-0.0023 (8)	0.0011 (7)	0.0009 (8)

Geometric parameters (Å, °)

S1A—C1A	1.7763 (19)	C19A—C20A	1.520 (4)
S1A—S2A	2.0914 (7)	S1B—C1B	1.7791 (19)
S2A—C11A	1.7707 (19)	S1B—S2B	2.0827 (6)
F1A—C8A	1.334 (3)	S2B—C11B	1.7794 (19)
F2A—C8A	1.327 (3)	F1B—C8B	1.346 (3)
F3A—C8A	1.330 (3)	F2B—C8B	1.318 (3)
F4A—C10A	1.320 (3)	F3B—C8B	1.316 (3)
F5A-C10A	1.315 (3)	F4B—C10B	1.325 (3)
F6A—C10A	1.312 (3)	F5B—C10B	1.388 (2)
F4A'—C10A	1.318 (3)	F6B—C10B	1.306 (2)
F5A'—C10A	1.321 (3)	F4B'	1.336 (3)
F6A'C10A	1.325 (3)	F5B'—C10B	1.297 (3)
F7A—C18A	1.332 (3)	F6B'	1.380 (3)
F8A—C18A	1.330 (3)	F7B—C18B	1.342 (3)
F9A—C18A	1.334 (3)	F8B—C18B	1.328 (3)
F10A—C20A	1.326 (3)	F9B—C18B	1.333 (3)
F11A—C20A	1.309 (3)	F10B—C20B	1.329 (2)
F12A—C20A	1.396 (3)	F11B—C20B	1.332 (3)
F10C—C20A	1.315 (3)	F12B—C20B	1.328 (3)
F11C—C20A	1.390 (3)	O1B—C7B	1.207 (3)
F12C—C20A	1.307 (3)	O2B—C9B	1.204 (3)
O1A—C7A	1.213 (3)	O3B—C17B	1.212 (3)
O2A—C9A	1.214 (3)	O4B—C19B	1.212 (2)
O3A—C17A	1.203 (3)	N1B—C7B	1.342 (3)
O4A—C19A	1.210 (3)	N1B—C2B	1.412 (2)
N1A—C7A	1.345 (3)	N1B—H1BN	0.80 (3)
N1A—C2A	1.430 (2)	N2B—C9B	1.353 (3)
N1A—H1AN	0.89 (3)	N2B—C6B	1.410 (3)
N2A—C9A	1.345 (2)	N2B—H2BN	0.84 (3)
N2A—C6A	1.406 (2)	N3B—C17B	1.339 (3)
N2A—H2AN	0.84 (3)	N3B—C12B	1.415 (3)
N3A—C17A	1.349 (3)	N3B—H3BN	0.79 (3)
N3A—C12A	1.418 (2)	N4B—C19B	1.346 (3)
N3A—H3AN	0.84 (3)	N4B—C16B	1.413 (3)
N4A—C19A	1.356 (3)	N4B—H4BN	0.85 (3)
N4A—C16A	1.410 (3)	C1B—C2B	1.404 (3)
N4A—H4AN	0.83 (3)	C1B—C6B	1.410 (3)
C1A—C2A	1.400 (3)	C2B—C3B	1.396 (3)
C1A—C6A	1.409 (3)	C3B—C4B	1.383 (3)
C2A—C3A	1.390 (3)	C3B—H3B	0.9500
C3A—C4A	1.387 (3)	C4B—C5B	1.390 (3)
СЗА—НЗА	0.9500	C4B—H4B	0.9500
C4A—C5A	1.388 (3)	C5B—C6B	1.388 (3)
C4A—H4A	0.9500	C5B—H5B	0.9500
C5A—C6A	1.399 (3)	C7B—C8B	1.540 (3)
С5А—Н5А	0.9500	C9B—C10B	1.517 (3)

C7A—C8A	1.542 (3)	C11B—C12B	1.405 (3)
C9A—C10A	1.536 (3)	C11B—C16B	1.406 (3)
C11A—C12A	1.406 (3)	C12B—C13B	1.396 (3)
C11A—C16A	1.410 (3)	C13B—C14B	1.383 (3)
C12A—C13A	1.395 (3)	C13B—H13B	0.9500
C13A—C14A	1.387 (3)	C14B—C15B	1,386 (3)
C13A—H13A	0.9500	C14B—H14B	0.9500
C14A - C15A	1 386 (3)	C15B-C16B	1 396 (3)
C14A - H14A	0.9500	C15B—H15B	0.9500
C_{15A} C_{16A}	1.305(3)	C17B C18B	1.543(3)
C_{15A} H_{15A}	0.0500	C10P $C20P$	1.543(3)
C17A $C18A$	0.9300	C19B—C20B	1.342 (3)
CI/A—CIðA	1.552 (5)		
C1A—S1A—S2A	100.33 (6)	F10A-C20A-C19A	112.6 (3)
C11A—S2A—S1A	99.91 (6)	F11C-C20A-C19A	104.0 (2)
C7A—N1A—C2A	120.29 (17)	F12A-C20A-C19A	108.5 (2)
C7A—N1A—H1AN	122.0 (17)	C1B—S1B—S2B	102.74 (6)
C2A—N1A—H1AN	1169(17)	C11B—S2B—S1B	102.73 (6)
C9A - N2A - C6A	12910(18)	C7B - N1B - C2B	126 31 (18)
C9A = N2A = H2AN	117.4 (18)	C7B—N1B—H1BN	1150(19)
C6A = N2A = H2AN	117.1(10) 113.5(18)	C^2B N1B H1BN	118.6(19)
C174 - N34 - C124	126 14 (17)	C9B = N2B = C6B	127.43(18)
C17A = N3A = C12A	120.14(17) 116.5(18)	C9B = N2B = C0B	127.43(10) 116.1(10)
C12A N2A H2AN	110.3(18) 117.2(18)	C6D N2D H2DN	110.1(19)
CI2A—INSA—HSAN	117.3(10)	C0B - N2B - R2DN	110.4(19)
C19A - N4A - C16A	127.4 (2)	CI/B—N3B—CI2B	126.10 (18)
CI9A—N4A—H4AN	115 (2)	CI/B—N3B—H3BN	119 (2)
CI6A—N4A—H4AN	117 (2)	C12B—N3B—H3BN	114 (2)
C2A—C1A—C6A	118.86 (17)	C19B—N4B—C16B	127.87 (17)
C2A—C1A—S1A	120.89 (15)	C19B—N4B—H4BN	115.3 (18)
C6A—C1A—S1A	120.25 (14)	C16B—N4B—H4BN	116.4 (18)
C3A—C2A—C1A	120.71 (18)	C2B—C1B—C6B	118.91 (17)
C3A—C2A—N1A	119.54 (18)	C2B—C1B—S1B	119.82 (14)
C1A—C2A—N1A	119.74 (17)	C6B—C1B—S1B	121.27 (15)
C4A—C3A—C2A	119.44 (19)	C3B—C2B—C1B	120.75 (18)
С4А—С3А—Н3А	120.3	C3B—C2B—N1B	121.12 (18)
С2А—С3А—НЗА	120.3	C1B—C2B—N1B	118.12 (17)
C3A—C4A—C5A	121.44 (19)	C4B—C3B—C2B	118.84 (19)
СЗА—С4А—Н4А	119.3	C4B—C3B—H3B	120.6
С5А—С4А—Н4А	119.3	C2B—C3B—H3B	120.6
C4A—C5A—C6A	119.01 (19)	C3B—C4B—C5B	121.86 (19)
С4А—С5А—Н5А	120.5	C3B—C4B—H4B	119.1
С6А—С5А—Н5А	120.5	C5B—C4B—H4B	119.1
C5A—C6A—N2A	122.99 (18)	C6B—C5B—C4B	119.32 (19)
C5A—C6A—C1A	120.50 (18)	C6B—C5B—H5B	120.3
N2A—C6A—C1A	116.43 (17)	C4B—C5B—H5B	120.3
O1A - C7A - N1A	125.97 (19)	C5B—C6B—N2B	122.50(18)
01A - C7A - C8A	117 83 (19)	C5B-C6B-C1B	120 33 (18)
NIA—C7A—C8A	116 09 (18)	N2B-C6B-C1B	117 12 (17)
	110,07 (10)		· · / · · · · · / / / / / / / / / / / /

	109.47(17)	OID C7D NID	127.52(10)
$F_2A = C_0A = F_1A$	108.47(17)	OID - C/D - NID	127.33 (19)
$F_2A = C_8A = F_1A$	107.90 (18)	$OIB - C/B - C\delta B$	118.70 (18)
F3A—C8A—FIA	107.61 (19)		113.76(18)
F2A—C8A—C/A	110.34 (19)	F3B—C8B—F2B	108.7 (2)
F3AC8AC/A	113.38 (17)	F3B—C8B—F1B	106.3 (2)
F1A—C8A—C7A	108.97 (17)	F2B—C8B—F1B	107.9 (2)
O2A—C9A—N2A	128.4 (2)	F3B—C8B—C7B	110.79 (19)
O2A—C9A—C10A	119.01 (17)	F2B—C8B—C7B	110.9 (2)
N2A—C9A—C10A	112.60 (17)	F1B—C8B—C7B	112.12 (18)
F6A-C10A-F5A	108.6 (3)	O2B—C9B—N2B	128.4 (2)
F6A—C10A—F4A	109.3 (3)	O2B—C9B—C10B	118.72 (18)
F5A—C10A—F4A	107.0 (3)	N2B-C9B-C10B	112.80 (17)
F4A'-C10A-F5A'	107.5 (3)	F6B—C10B—F4B	110.8 (3)
F4A'-C10A-F6A'	107.3 (3)	F5B'—C10B—F4B'	110.9 (4)
F5A'-C10A-F6A'	105.5 (3)	F5B'—C10B—F6B'	105.2 (3)
F6A-C10A-C9A	109.6 (3)	F4B'—C10B—F6B'	102.2 (4)
F5A—C10A—C9A	110.5 (3)	F6B—C10B—F5B	103.9 (2)
F4A' - C10A - C9A	114.1 (3)	F4B— $C10B$ — $F5B$	105.7(3)
F4A - C10A - C9A	111.7(2)	$F_{5B'}$ C10B C9B	103.7(3) 118.9(3)
F5A' C10A C9A	111.7(2) 111.1(3)	F6B C10B C9B	110.9(3)
$F_{0A} = C_{0A} = C_{0A}$	111.1(3) 110.0(3)	$F_{4B} = C_{10B} = C_{3B}$	114.0(2)
$\begin{array}{c} 10A - C10A - C9A \\ C12A - C11A - C16A \end{array}$	110.9(3)	$F_{4}D = C_{1}OD = C_{2}D$	110.2(2) 112.5(2)
C12A = C11A = C10A	119.00(17) 120.17(15)	$F4B \longrightarrow C10B \longrightarrow C9B$	113.3(3)
C12A - C11A - S2A	120.17(15)		104.1(3)
CI6A—CIIA—S2A	120.13 (15)	FSB—CI0B—C9B	104.97 (19)
CI3A—CI2A—CIIA	119.99 (18)	C12B—C11B—C16B	119.05 (17)
C13A—C12A—N3A	121.37 (18)	C12B—C11B—S2B	119.72 (15)
C11A—C12A—N3A	118.64 (17)	C16B—C11B—S2B	121.21 (15)
C14A—C13A—C12A	119.02 (19)	C13B—C12B—C11B	120.62 (19)
C14A—C13A—H13A	120.5	C13B—C12B—N3B	121.13 (18)
C12A—C13A—H13A	120.5	C11B—C12B—N3B	118.17 (17)
C15A—C14A—C13A	122.35 (19)	C14B—C13B—C12B	118.80 (19)
C15A—C14A—H14A	118.8	C14B—C13B—H13B	120.6
C13A—C14A—H14A	118.8	C12B—C13B—H13B	120.6
C14A—C15A—C16A	118.84 (19)	C13B—C14B—C15B	122.18 (19)
C14A—C15A—H15A	120.6	C13B—C14B—H14B	118.9
C16A—C15A—H15A	120.6	C15B—C14B—H14B	118.9
C15A—C16A—N4A	122.16 (18)	C14B— $C15B$ — $C16B$	118.92 (19)
C15A - C16A - C11A	120.08 (19)	C14B— $C15B$ — $H15B$	120.5
N4A - C16A - C11A	117 76 (18)	C_{16B} C_{15B} H_{15B}	120.5
$O_3A = C_17A = N_3A$	1281(2)	C15B $C16B$ $C11B$	120.5
$O_{3A} = C_{17A} = C_{18A}$	120.1(2) 118 51 (10)	C15B C16B N/B	120.40(18)
$N_{2A} = C_{17A} = C_{18A}$	110.31(19) 112.40(19)	C11P C16P N4P	122.04(18) 117.54(17)
$N_{A} = C_{1/A} = C_{10A}$	113.40(18) 108.02(10)	C11D - C10B - N4B	117.34(17)
$ \begin{array}{c} \Gamma \circ A \longrightarrow \\ \Gamma \circ A \longrightarrow $	106.05(19)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	120.0(2)
гол—Стол—ГУА Гла Стол Гол	100.99 (19)		119.23 (19)
F/A = C18A = F9A	10/.46 (18)		112.78 (18)
F8A-C18A-C1/A	111.23 (18)	F8B-C18B-F9B	108.00 (17)
F7A—C18A—C17A	110.01 (18)	F8B—C18B—F7B	107.65 (18)
F9A—C18A—C17A	112.91 (17)	F9B—C18B—F7B	107.53 (18)

O4A—C19A—N4A	128.3 (2)	F8B—C18B—C17B	109.90 (18)
O4A—C19A—C20A	119.7 (2)	F9B—C18B—C17B	110.90 (18)
N4A—C19A—C20A	111.95 (19)	F7B—C18B—C17B	112.69 (17)
F12CC20AF10C	114.0 (4)	O4B—C19B—N4B	128.55 (19)
F11A-C20A-F10A	110.9 (3)	O4B—C19B—C20B	117.57 (18)
F12C—C20A—F11C	102.2 (3)	N4B—C19B—C20B	113.82 (17)
F10C—C20A—F11C	103.8 (3)	F12B-C20B-F10B	108.42 (18)
F11A-C20A-F12A	101.7 (3)	F12B—C20B—F11B	107.86 (17)
F10A—C20A—F12A	102.1 (3)	F10B-C20B-F11B	107.97 (19)
F12C-C20A-C19A	116.7 (3)	F12B-C20B-C19B	108.87 (18)
F11A—C20A—C19A	119.0 (3)	F10B-C20B-C19B	113.46 (17)
F10C—C20A—C19A	113.8 (3)	F11B—C20B—C19B	110.10 (17)
S2A—S1A—C1A—C2A	102.74 (15)	N4A—C19A—C20A—F11C	-94.1(3)
S2A = S1A = C1A = C6A	-76.26(15)	O4A— $C19A$ — $C20A$ — $F12A$	-123.9(3)
C6A—C1A—C2A—C3A	1.5 (3)	N4A—C19A—C20A—F12A	57.9 (3)
SIA—CIA—C2A—C3A	-177.49(16)	S2B = S1B = C1B = C2B	104.09 (15)
C6A - C1A - C2A - N1A	-17948(17)	S^2B S^1B C^1B C^2B	-7637(16)
S1A-C1A-C2A-N1A	15(3)	C6B-C1B-C2B-C3B	-0.1(3)
C7A—N1A— $C2A$ — $C3A$	-1194(2)	S1B - C1B - C2B - C3B	17948(15)
C7A—N1A— $C2A$ — $C1A$	61.6 (3)	C6B-C1B-C2B-N1B	-17892(17)
C1A - C2A - C3A - C4A	-0.2(3)	S1B— $C1B$ — $C2B$ — $N1B$	0.6.(2)
N1A - C2A - C3A - C4A	$-179\ 21\ (19)$	C7B $N1B$ $C2B$ $C3B$	310(3)
C_{2A} C_{3A} C_{4A} C_{5A}	-10(3)	C7B $N1B$ $C2B$ $C1B$	-1501(2)
$C_{2A} = C_{4A} = C_{5A} = C_{6A}$	0.9(3)	C1B $C2B$ $C3B$ $C4B$	0.3(3)
$C_{4A} = C_{5A} = C_{6A} = N_{2A}$	177 10 (19)	N1B-C2B-C3B-C4B	179 12 (19)
$C_{4A} = C_{5A} = C_{6A} = C_{1A}$	177.10(17)	C^{2B} C^{3B} C^{4B} C^{5B}	-0.1(3)
$C_{A} = C_{A} = C_{A} = C_{A}$	-11(3)	$C_{2B} = C_{3B} = C_{4B} = C_{5B} = C_{6B}$	-0.3(3)
$C_{A} = N_{A} = C_{A} = C_{A} = C_{A}$	1.1(5) 175 62 (10)	$C_{3}B_{-}C_{4}B_{-}C_{5}B_{-}C_{6}B_{-}N_{2}B_{-}$	177.00(10)
$C_{A} = N_{A} = C_{A} = C_{A} = C_{A}$	-1.7(3)	C4B = C5B = C6B = C1B	1/7.33(13)
C_{2A} C_{1A} C_{6A} C_{5A}	1.7(5) 177.24(15)	$C_{+B} = C_{-}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-}$	-68(3)
$C_{A} C_{A} C_{A} C_{A} C_{A} N_{A}$	-178.48(17)	$C_{9}D_{N2}D_{C0}C_{0}D_{C0}D_{C$	170.72(10)
C_{2A} C_{1A} C_{6A} N_{2A}	1/0.40(17)	$C_{2B} = C_{1B} = C_{0B} = C_{1B}$	-0.4(3)
$C_{A} = C_{A} = C_{A} = C_{A} = C_{A}$	0.3(2)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-170.02(15)
$C_{2A} = N_{1A} = C_{7A} = O_{1A}$	-172.00(17)	$C^{2} P C^{1} P C^{6} P N^{2} P$	179.92(13) -177.02(17)
C_{2A} N_{1A} C_{7A} C_{8A} E_{2A}	54.3 (3)	S1P C1P C6P N2P	177.92(17)
$\mathbf{V}_{\mathbf{A}} = \mathbf{C}_{\mathbf{A}} + $	-120.3(2)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.3(2)
$\mathbf{N}\mathbf{I}\mathbf{A} = \mathbf{C}\mathbf{I}\mathbf{A} = \mathbf{C}\mathbf{O}\mathbf{A} = \mathbf{F}\mathbf{I}\mathbf{A}$	129.3(2) 176.16(10)	C_{2D} N1D C_{7D} C_{9D}	1.1(4) 170.78(10)
VIA - C7A - C8A - F3A	-7.5(2)	C_{2D} NID C_{7D} Cod C_{2D} Cod C_{2D}	1/9.70(19)
NIA = C/A = C8A = F3A	-7.3(3)	$\begin{array}{c} 01B - 07B - 08D - 07B \\ 01B - 07B - 08B - 07B \\ 01B - 07B - 08B \\ 01B - 07B \\ 01B -$	20.0(3)
OIA - C/A - CoA - FIA	-04.0(3)	$NIB - C/B - C\delta B - F3B$	-134.2(2)
NIA - C/A - CoA - FIA	112.4(2)	$\begin{array}{c} \text{OIB} \hline \text{C}/\text{B} \hline \text{C} \text{OB} \hline \text{F} \text{2B} \\ \text{N1D} \hline \text{C} \text{7D} \hline \text{C} \text{SD} \hline \text{F} \text{2D} \\ \end{array}$	-94.2(3)
C6A = N2A = C9A = O2A	0.0(4)	$NIB - C/B - C\delta B - F2B$	85.0 (2)
COA = NZA = CYA = CIUA	-1/3.30(19)	$ \begin{array}{cccc} UID - U/B - U\delta B - FIB \\ \\ NID & C7D & C9D & FID \\ \end{array} $	143.1(2)
U_{A} U_{A	-1/.4(4)	$NID - U/B - U\delta B - FIB$	-35.7(3)
N_{A} U_{A} U_{A} U_{A} T_{A}	102.1(4)	COB = N2B = COB = C10D	0.5 (4)
U_{A} U_{A	42.5 (5)	COB = N2B = C9B = C10B	-1/0.46 (18)
NZA-CYA-CIUA-F5A	-138.2 (4)	02B - 02B - 010B - F5B'	-45.7 (5)
02A—C9A—C10A—F4A'	-169.2 (5)	N2B—C9B—C10B—F5B'	131.6 (5)

N2A—C9A—C10A—F4A'	10.3 (5)	O2B—C9B—C10B—F6B	33.6 (3)
O2A—C9A—C10A—F4A	161.2 (3)	N2B—C9B—C10B—F6B	-149.1(3)
N2A—C9A—C10A—F4A	-19.2 (4)	O2B—C9B—C10B—F4B	164.3 (3)
O2A—C9A—C10A—F5A'	-47.4 (4)	N2B—C9B—C10B—F4B	-18.5 (4)
N2A—C9A—C10A—F5A'	132.1 (4)	O2B—C9B—C10B—F4B'	-178.9(4)
O2A—C9A—C10A—F6A'	69.5 (4)	N2B—C9B—C10B—F4B'	-1.6(5)
N2A—C9A—C10A—F6A'	-110.9 (4)	O2B—C9B—C10B—F6B'	70.8 (4)
S1A—S2A—C11A—C12A	103.05 (15)	N2B—C9B—C10B—F6B'	-111.9(4)
S1A—S2A—C11A—C16A	-75.07 (16)	O2B—C9B—C10B—F5B	-79.4 (3)
C16A—C11A—C12A—C13A	-0.7(3)	N2B—C9B—C10B—F5B	97.9 (3)
S2A-C11A-C12A-C13A	-178.81 (15)	S1B—S2B—C11B—C12B	97.17 (15)
C16A—C11A—C12A—N3A	179.69 (17)	S1B—S2B—C11B—C16B	-84.67 (16)
S2A—C11A—C12A—N3A	1.6 (2)	C16B-C11B-C12B-C13B	1.9 (3)
C17A - N3A - C12A - C13A	27.8 (3)	\$2B-C11B-C12B-C13B	-179.90(16)
C17A - N3A - C12A - C11A	-152.5(2)	C16B-C11B-C12B-N3B	-174.94(17)
C11A - C12A - C13A - C14A	2.0 (3)	S2B-C11B-C12B-N3B	3.3 (2)
N3A - C12A - C13A - C14A	-178.39(19)	C17B $N3B$ $C12B$ $C13B$	32.1(3)
C12A— $C13A$ — $C14A$ — $C15A$	-1.6(3)	C17B $N3B$ $C12B$ $C11B$	-151.1(2)
C13A - C14A - C15A - C16A	-0.2(3)	C11B— $C12B$ — $C13B$ — $C14B$	-1.8(3)
C14A - C15A - C16A - N4A	-179 12 (19)	N3B-C12B-C13B-C14B	174 96 (19)
C14A - C15A - C16A - C11A	1.5 (3)	C12B-C13B-C14B-C15B	0.4 (3)
C19A - N4A - C16A - C15A	-2.5(3)	C13B-C14B-C15B-C16B	0.8(3)
C19A - N4A - C16A - C11A	176.9 (2)	C14B-C15B-C16B-C11B	-0.7(3)
C12A—C11A—C16A—C15A	-1.1(3)	C14B—C15B—C16B—N4B	177.97 (19)
S2A—C11A—C16A—C15A	177.03 (16)	C12B—C11B—C16B—C15B	-0.7(3)
C12A—C11A—C16A—N4A	179.51 (18)	S2B-C11B-C16B-C15B	-178.83(15)
S2A—C11A—C16A—N4A	-2.4(3)	C12B—C11B—C16B—N4B	-179.36(17)
C12A—N3A—C17A—O3A	-3.4 (4)	S2B-C11B-C16B-N4B	2.5 (2)
C12A—N3A—C17A—C18A	177.69 (18)	C19B—N4B—C16B—C15B	-2.0(3)
O3A—C17A—C18A—F8A	-87.1 (3)	C19B—N4B—C16B—C11B	176.69 (19)
N3A—C17A—C18A—F8A	91.9 (2)	C12B—N3B—C17B—O3B	5.0 (4)
O3A—C17A—C18A—F7A	32.5 (3)	C12B—N3B—C17B—C18B	-173.19(18)
N3A—C17A—C18A—F7A	-148.47(19)	O3B-C17B-C18B-F8B	-82.9(3)
O3A - C17A - C18A - F9A	152.6 (2)	N3B-C17B-C18B-F8B	95.5 (2)
N3A—C17A—C18A—F9A	-28.4(3)	O3B-C17B-C18B-F9B	36.4 (3)
C16A - N4A - C19A - O4A	-1.1(4)	N3B-C17B-C18B-F9B	-145.18(18)
C16A - N4A - C19A - C20A	176.9 (2)	O3B-C17B-C18B-F7B	157.0 (2)
O4A— $C19A$ — $C20A$ — $F12C$	-164.1(4)	N3B - C17B - C18B - F7B	-24.6(3)
N4A—C19A—C20A—F12C	17.7 (5)	C16B—N4B—C19B—O4B	4.9 (4)
O4A—C19A—C20A—F11A	120.7 (5)	C16B—N4B—C19B—C20B	-172.29(18)
N4A—C19A—C20A—F11A	-57.5 (4)	O4B—C19B—C20B—F12B	-71.4 (2)
O4A—C19A—C20A—F10C	-28.2 (4)	N4B—C19B—C20B—F12B	106.10 (19)
N4A—C19A—C20A—F10C	153.6 (4)	O4B—C19B—C20B—F10B	167.8 (2)
O4A—C19A—C20A—F10A	-11.6 (5)	N4B—C19B—C20B—F10B	-14.7 (3)
N4A—C19A—C20A—F10A	170.2 (4)	O4B—C19B—C20B—F11B	46.7 (3)
O4A—C19A—C20A—F11C	84.1 (3)	N4B—C19B—C20B—F11B	-135.85 (18)
	× /		· /

D—H···A	<i>D</i> —Н	H···A	$D \cdots A$	D—H··· A
N1 <i>A</i> —H1 <i>AN</i> ···O4 <i>B</i>	0.89 (3)	2.19 (3)	2.988 (2)	149 (2)
N2A—H2AN…S1A	0.84 (3)	2.42 (3)	2.9425 (18)	121 (2)
N2A—H2AN····S2A	0.84 (3)	2.96 (3)	3.4543 (18)	120 (2)
N2A—H2AN…F4A	0.84 (3)	2.16 (3)	2.574 (4)	110 (2)
N2A—H2AN…F4A′	0.84 (3)	2.19 (3)	2.600 (5)	110 (2)
N3A—H3AN····O1A ⁱ	0.84 (3)	2.12 (3)	2.857 (2)	146 (2)
N4A—H4AN…S2A	0.83 (3)	2.52 (3)	2.9697 (19)	116 (2)
N4A—H4AN…F12C	0.83 (3)	2.21 (3)	2.643 (4)	113 (2)
C5 <i>A</i> —H5 <i>A</i> ···O2 <i>A</i>	0.95	2.34	2.952 (3)	122
C13A—H13A…F5B′ ⁱⁱ	0.95	2.54	3.207 (4)	127
C15A—H15A····O4A	0.95	2.25	2.883 (3)	123
N1 <i>B</i> —H1 <i>BN</i> ···O2 <i>A</i> ⁱⁱⁱ	0.80 (3)	2.42 (3)	2.983 (2)	128 (2)
N2B—H2BN…S1B	0.84 (3)	2.51 (3)	2.9892 (18)	117 (2)
N2 <i>B</i> —H2 <i>BN</i> …F4 <i>B</i>	0.84 (3)	2.23 (3)	2.657 (4)	112 (2)
N2 <i>B</i> —H2 <i>BN</i> …F4 <i>B</i> ′	0.84 (3)	2.13 (3)	2.574 (7)	113 (2)
N3 <i>B</i> —H3 <i>BN</i> ···O1 <i>B</i> ^{iv}	0.79 (3)	2.24 (3)	2.848 (2)	135 (3)
N4 <i>B</i> —H4 <i>BN</i> ···S2 <i>B</i>	0.85 (3)	2.53 (3)	2.9936 (17)	116 (2)
N4B—H4BN…F10B	0.85 (3)	2.20 (3)	2.634 (2)	112 (2)
N4 <i>B</i> —H4 <i>BN</i> ···O3 <i>B</i> ^{iv}	0.85 (3)	2.47 (3)	3.032 (2)	125 (2)
C5 <i>B</i> —H5 <i>B</i> ···O2 <i>B</i>	0.95	2.27	2.896 (3)	122
C15 <i>B</i> —H15 <i>B</i> ···O3 <i>A</i>	0.95	2.56	3.229 (3)	128
C15 <i>B</i> —H15 <i>B</i> ···O4 <i>B</i>	0.95	2.27	2.898 (3)	123

Hydrogen-bond geometry (Å, °)

Symmetry codes: (i) -x+1/2, y-1/2, -z+1/2; (ii) -x+3/2, y-1/2, -z+1/2; (iii) x+1/2, -y+3/2, z-1/2; (iv) -x+3/2, y+1/2, -z+1/2.