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### Bis(4-aminopyridinium) $\mu_6$ -oxido-dodeca- $\mu_2$ -oxido-hexaoxido[rhenium(VII)tetratungsten(VI)vanadium(V)]ate heptahydrate

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Key indicators: single-crystal X-ray study; T = 298 K; mean  $\sigma$ (C–C) = 0.014 Å; disorder in main residue; R factor = 0.069; wR factor = 0.192; data-to-parameter ratio = 31.8.

In the title organic-inorganic hybrid compound,  $(C_5H_7N_2)_2$  [ReVW<sub>4</sub>O<sub>19</sub>]·7H<sub>2</sub>O, the Lindqvist-type polyoxido anion has crystallographically imposed mm2 symmetry and is built up by six  $MO_6$  (M = W, V, Re) edge-sharing distorted octahedra. The Re and V atoms share the same crystallographic site in a 0.5:0.5 ratio. The 4-aminopyridinium cations lie on a mirror plane. Three of the four independent water O atoms in the asymmetric unit are located on a mirror plane whereas the remaining O atom has mm2 site symmetry. In the crystal, the cations, anions and water molecules are linked into a three-dimensional network through  $O-H \cdots O$  and N-H···O hydrogen-bonding interactions.

#### **Related literature**

For applications of polyoxidometalates, see: Pope & Müller (1991, 1994). For bond-valence calculations, see: Brown & Altermatt (1985). For related structures, see: Lindqvist (1953); Bannani *et al.* (2007); Besecker *et al.* (1982); Wang *et al.* (2011); Wang *et al.* (2006); Meng *et al.* (2006). For NMR investigations of related compounds, see: Chen *et al.* (2004); Domaille (1984); Fedotov & Maksimovskaya (2006); Leparulo-Loftus & Pope (1987).



Z = 2

Ag  $K\alpha$  radiation  $\lambda = 0.56087$  Å

 $0.43 \times 0.27 \times 0.15 \text{ mm}$ 

 $\mu = 9.22 \text{ mm}^{-1}$ 

T = 298 K

#### Experimental

Crystal data  $(C_{5}H_{7}N_{2})_{2}[ReVW_{4}O_{19}]\cdot7H_{2}O$   $M_{r} = 1592.90$ Orthorhombic, *Pmma*  a = 17.837 (2) Å b = 9.163 (4) Å c = 10.552 (3) Å V = 1724.5 (9) Å<sup>3</sup>

#### Data collection

Enraf–Nonius CAD-4 diffractometer Absorption correction: multi-scan (Blessing, 1995)  $T_{min} = 0.100, T_{max} = 0.306$ 6539 measured reflections

#### Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.069$  $wR(F^2) = 0.192$ S = 1.034385 reflections 138 parameters 4385 independent reflections 2083 reflections with  $I > 2\sigma(I)$  $R_{int} = 0.052$ 2 standard reflections every 120 min intensity decay: none

 $\begin{array}{l} 17 \text{ restraints} \\ \text{H-atom parameters constrained} \\ \Delta \rho_{\text{max}} = 2.94 \text{ e } \text{ Å}^{-3} \\ \Delta \rho_{\text{min}} = -2.83 \text{ e } \text{ Å}^{-3} \end{array}$ 

### Table 1

Hydrogen-bond geometry (Å,  $^{\circ}$ ).

| $D - H \cdot \cdot \cdot A$                | D-H                     | $H \cdots A$ | $D \cdots A$  | $D - \mathbf{H} \cdot \cdot \cdot A$ |
|--|-------------------------|--------------|---------------|--------------------------------------|
| $N1-H1A\cdotsO1W$                          | 0.86                    | 2.40         | 3.078 (14)    | 136                                  |
| $N1 - H1A \cdots O1E$                      | 0.86                    | 2.58         | 3.184 (14)    | 129                                  |
| $N2-H2A\cdots O3^{i}$                      | 0.86                    | 2.39         | 3.181 (12)    | 152                                  |
| $O1W - H1W1 \cdots O1E$                    | 0.81                    | 2.50         | 3.188 (18)    | 144                                  |
| $O2W - H1W2 \cdot \cdot \cdot O3E^{ii}$    | 0.85                    | 2.10         | 2.836 (18)    | 144                                  |
| $O4W - H1W4 \cdots O2W$                    | 0.85                    | 1.87         | 2.40 (7)      | 119                                  |
| $O4W - H2W4 \cdots O4W^{iii}$              | 0.85                    | 2.31         | 2.65 (15)     | 106                                  |
| Symmetry codes: (i)<br>-x + 1, -y, -z + 2. | $x + \frac{1}{2}, y, -$ | z + 1; (ii)  | -x + 1, -y, - | -z + 1; (iii)                        |

Data collection: *CAD-4 EXPRESS* (Enraf–Nonius, 1994); cell refinement: *CAD-4 EXPRESS*; data reduction: *XCAD4* (Harms & Wocadlo, 1996); program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *ORTEP-3 for Windows* (Farrugia, 2012) and *DIAMOND* (Brandenburg & Putz, 2005); software used to prepare material for publication: *WinGX* (Farrugia, 2012).

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: RZ5088).

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# supporting information

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## Bis(4-aminopyridinium) $\mu_6$ -oxido-dodeca- $\mu_2$ -oxidohexaoxido[rhenium(VII)tetratungsten(VI)vanadium(V)]ate heptahydrate

### Ahlem Maaloui, Samah Akriche Toumi and Mohamed Rzaigui

#### S1. Comment

Polyoxidometalate are of great interest in different fields such as medecine, biology, catalysis, material sciences, chemical analysis (Pope & Müller, 1991; Pope & Müller, 1994). Among this large class of compounds, Lindqvist anions  $[M_6O_{19}]^{n-}$  have been intensively studied since the early characterization of Na<sub>7</sub>HNb<sub>6</sub>O<sub>19</sub>.15H<sub>2</sub>O (Lindqvist, 1953). However, studies of substituted hexatungstate  $[M_nW_{6-n}O_{19}]^{(2+n)-}$  are relatively scarce. Up to now, few compounds are cited in the literature, such as  $[(n-C_4H_9)_4N]_3MW_5O_{19}$  (M = Nb, V) (Bannani *et al.*, 2007), { $[(C_7H_8)Rh]_5(Nb_2W_4O_{19})_2$ }[ $(n-C_4H_9)N]_3$  (Besecker *et al.*, 1982), [Cu(phen)(H<sub>2</sub>O)<sub>3</sub>]<sub>2</sub>[V<sub>2</sub>W<sub>4</sub>O<sub>19</sub>] and [Cu(bpy)(H<sub>2</sub>O)]<sub>2</sub>[V<sub>2</sub>W<sub>4</sub>O<sub>19</sub>]·4H<sub>2</sub>O (Wang *et al.*, 2011) and [Ni(bpy)<sub>3</sub>]<sub>2</sub>[W<sub>4</sub>V<sub>2</sub>O19] (Wang *et al.*, 2006), whereas substituted Lindqvist-type polyoxotungstates based on  $[M_nM'_pW_{6-n-p}O_{19}]^{(2+n+p)-}$  anions have not been reported hitherto. On the best of our knowledge the reported title salt, (C<sub>5</sub>H<sub>7</sub>N<sub>2</sub>)<sub>2</sub>·[ReVW<sub>4</sub>O<sub>19</sub>]·7H<sub>2</sub>O (I), is the first example of this kind of substituted Lindqvist structure.

The asymmetric unit of (I) contains 1.75 water molecules, one half of a 4-aminopyridinium cation and one fourth of a  $[\text{ReVW}_{4}\text{O}_{19}]^{2^{-}}$  polyanion, in which Re and V metals share the same site in a 0.5:0.5 ratio. All constituents are completed by imposed crystallographic symmetries (Fig. 1). Three out of the four independent water O atoms in the asymmetric unit have mirror symmetry, while a fouth O atom has mm2 site symmetry. It is to be mentioned that the O3W and O4W oxygen atoms associated to water molecules have relatively high thermal desorder and could not be anisotropically refined. In the crystal packing, cations and solvent water molecules assemble the discrete  $[ReVW_4O_{19}]^{2-}$  anion complexes through OW—H…O and N—H…O hydrogen bonding interactions (Table 1) to form a supramolecular three-dimensional network as shown in Figure 2. The structure of the  $[\text{ReVW}_4O_{19}]^2$  polyanion is basically the same as that of Lindqvist-type anion (Lindqvist, 1953). It is built upby six  $MO_6$  (M = W, V, Re) edge-sharing distorted octahedra and exhibits the characteristic M—O bond-length range, with the shortest bonds being the M—O terminal bonds and the longest being those involving the central O atom. The geometry features of the polyanion are in agreement with those of the Lindqvisttype polyoxidotungstate reported by Meng et al. (2006). The valence bond calculation (Brown & Altermatt, 1985) gives effective bond valences of 4.9847 for the V cation, 7.1447 for the Re cation and 6.0697 and 6.1369 for the two independent W cations. These values are consistent with the oxidation states V(V), Re(VII) and W(VI). In an attempt to shed more light on the structure of the hexametalate anion, we contemplated <sup>51</sup>V and <sup>183</sup>W NMR studies on the title complex. In fact, regarding the  $[M_6O_{19}]^{n}$  complex structure, the vanadium and rhenium heteroatoms may occupy *cis* or trans positions in the octahedral structure. The <sup>183</sup>W NMR study shows two signals with relative intensity of ca 2:2, which can be assigned to the two equatorial (Weq) and the two axial (Wax) tungsten atoms respectively. On the other hand, the <sup>51</sup>V NMR spectrum presents one signal at 508.7 ppm. These results are consistent with the  $C_{2v}$  symmetry of the disubstitued hexametalate structure with preferential *cis* configuration as reported in literature (Chen *et al.*, 2004; Domaille, 1984; Fedotov & Maksimovskava, 2006; Leparulo-Loftus & Pope, 1987). All these observations corroborate

the structural results in suggesting that both rhenium and vanadium atoms (with 0.5/0.5 occupation) occupy preferentially the same site thus leading to a *cis*- $[X_2W_4O_{19}]^2$  ( $X = \text{Re}_{0.5}V_{0.5}$ ) anion configuration.

#### **S2. Experimental**

The title compound was prepared by the reaction of vanadium(V) oxide (0.18 g, 1 mmol), rhenium(VII) oxide (0.48 g, 1 mmol), Na<sub>2</sub>WO<sub>4</sub>.2H<sub>2</sub>O (2 g, 6 mmol) and 4-aminopyridine (0.19 g, 2 mmol) dissolved in 50 ml of distilled water and then stirred for 1 h. Yellowish single crystals were obtained after two weeks by slow evaporation at room temperature (yield: 59% based on W). Anal. Calc. for C<sub>10</sub>H<sub>28</sub>N<sub>4</sub>O<sub>26</sub>ReVW<sub>4</sub>: H 1.76, C 7.53, N 3.52, Re 11.69, V 3.20, W 46.16%; Found: H 1.81, C 7.57, N 3.50, Re 11.71, V 3.23, W 46.14%. <sup>183</sup>W NMR  $\delta$  (p.p.m.): 86.5, 65.4; <sup>51</sup>V NMR  $\delta$  (p.p.m.): 508.7.

#### **S3. Refinement**

An initial attempt to refine the crystal structure with the Re atom disordered over three independent sites resulted in rather high atomic displacement parameters for the heaviest atoms (Re1, W1 and W2) as a possible consequence of the large number of restraints required by this model. The refinement of a model implying the Re atom sharing only the site occupied by the vanadium atom with an occupancy factor of 0.5 rapidly converged to a plausible result with low residuals. These observations are also supported by NMR study as detailed in Comment section. In spite the crystal selected for the X-ray analysis appeared to be of good quality, its diffraction ability was very poor. This may account for the rather high residual peaks, high R values and unresolved disorder affecting part of the water molecules. In fact, anisotropical refinement of the O atoms associated to water molecules resulted in unreasonable  $U_{ij}$  values for atoms O3W and O4W, which were therefore isotropically refined. The water H atoms could not be located and were placed geometrically sensible positions using restraints [O—H = 0.85 (1) Å, H…H = 1.44 (2) Å and  $U_{iso}(H) = 1.5U_{eq}(O)$ . H atoms attached to C and N atoms were fixed geometrically and treated as riding, with C—H = 0.93 Å and N—H = 0.86 Å with  $U_{iso}(H) = 1.2U_{eq}(C, N)$ . In the final difference Fourier map, the highest residual electron density peak and the deepest hole are located 0.78 and 0.64 Å respectively from W2.



#### Figure 1

A view of the title compound with displacement ellipsoids drawn at the 30% probability level. H atoms are represented as small spheres of arbitrary radii. Hydrogen bonds are shown as dashed lines. Symmetry codes: (i) 1/2 + x, -y, 1 - z; (ii) 1/2 + x, y, 1 - z; (iii) x, 1 - y, z.



#### Figure 2

Packing diagram of the title compound. Hydrogen bonds are shown as dashed lines. Hydrogen atoms not involved in hydrogen bonding are omitted.

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F(000) = 1436

 $\mu = 9.22 \text{ mm}^{-1}$ 

Prism, yellow

 $0.43 \times 0.27 \times 0.15$  mm

 $\theta_{\rm max} = 28.0^\circ, \ \theta_{\rm min} = 2.3^\circ$ 

intensity decay: none

4385 independent reflections

2083 reflections with  $I > 2\sigma(I)$ 

2 standard reflections every 120 min

 $\theta = 9 - 11^{\circ}$ 

T = 298 K

 $R_{\rm int} = 0.052$ 

 $h = -29 \rightarrow 2$ 

 $k = -2 \rightarrow 15$ 

 $l = -17 \rightarrow 2$ 

 $D_{\rm x} = 3.068 {\rm Mg} {\rm m}^{-3}$ 

Ag Ka radiation,  $\lambda = 0.56087$  Å

Cell parameters from 25 reflections

#### Crystal data

 $(C_{5}H_{7}N_{2})_{2}[ReVW_{4}O_{19}]\cdot7H_{2}OM_{r} = 1592.90$ Orthorhombic, *Pmma* Hall symbol: -P 2a 2a a = 17.837 (2) Å b = 9.163 (4) Å c = 10.552 (3) Å V = 1724.5 (9) Å<sup>3</sup> Z = 2

#### Data collection

Enraf–Nonius CAD-4 diffractometer Radiation source: fine-focus sealed tube Graphite monochromator non–profiled  $\omega$  scans Absorption correction: multi-scan (Blessing, 1995)  $T_{\min} = 0.100, T_{\max} = 0.306$ 6539 measured reflections

#### Refinement

Refinement on  $F^2$ Secondary atom site location: difference Fourier Least-squares matrix: full map  $R[F^2 > 2\sigma(F^2)] = 0.069$ Hydrogen site location: inferred from  $wR(F^2) = 0.192$ neighbouring sites S = 1.03H-atom parameters constrained 4385 reflections  $w = 1/[\sigma^2(F_o^2) + (0.0813P)^2 + 4.9537P]$ where  $P = (F_0^2 + 2F_c^2)/3$ 138 parameters 17 restraints  $(\Delta/\sigma)_{\rm max} = 0.003$  $\Delta \rho_{\rm max} = 2.94 \ {\rm e} \ {\rm \AA}^{-3}$ Primary atom site location: structure-invariant  $\Delta \rho_{\rm min} = -2.83 \text{ e} \text{ Å}^{-3}$ direct methods

#### Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes. **Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(A^2)$ 

|     | x           | у            | Ζ            | $U_{ m iso}$ */ $U_{ m eq}$ | Occ. (<1) |
|-----|-------------|--------------|--------------|-----------------------------|-----------|
| W1  | 0.37770 (3) | 0.0000       | 0.34550 (7)  | 0.03479 (18)                |           |
| W2  | 0.2500      | 0.17748 (8)  | 0.18441 (8)  | 0.0497 (2)                  |           |
| Re1 | 0.2500      | 0.18032 (13) | 0.49071 (13) | 0.0505 (3)                  | 0.50      |

| V1   | 0.2500     | 0.18032 (13) | 0.49071 (13) | 0.0505 (3)  | 0.50 |
|------|------------|--------------|--------------|-------------|------|
| O1C  | 0.2500     | 0.0000       | 0.3367 (12)  | 0.023 (2)   |      |
| O1E  | 0.2500     | 0.3071 (16)  | 0.6049 (16)  | 0.068 (4)   |      |
| O2E  | 0.2500     | 0.3115 (18)  | 0.0720 (17)  | 0.081 (5)   |      |
| O3E  | 0.4740 (6) | 0.0000       | 0.3427 (13)  | 0.050 (3)   |      |
| 01   | 0.2500     | 0.0000       | 0.0922 (13)  | 0.048 (4)   |      |
| O2   | 0.3545 (4) | 0.1420 (9)   | 0.2154 (9)   | 0.0466 (19) |      |
| O3   | 0.2500     | 0.2888 (11)  | 0.3345 (12)  | 0.042 (3)   |      |
| O4   | 0.3529 (3) | 0.1446 (8)   | 0.4650 (8)   | 0.0375 (16) |      |
| O5   | 0.2500     | 0.0000       | 0.5902 (15)  | 0.039 (3)   |      |
| N1   | 0.3903 (7) | 0.5000       | 0.6867 (14)  | 0.057 (4)   |      |
| H1A  | 0.3422     | 0.5000       | 0.6901       | 0.068*      |      |
| N2   | 0.6091 (7) | 0.5000       | 0.6435 (17)  | 0.057 (4)   |      |
| H2A  | 0.6343     | 0.4198       | 0.649        | 0.069*      |      |
| C1   | 0.4219 (6) | 0.6284 (14)  | 0.6845 (14)  | 0.056 (3)   |      |
| H1   | 0.3939     | 0.7134       | 0.6938       | 0.067*      |      |
| C2   | 0.4963 (6) | 0.6327 (12)  | 0.6681 (13)  | 0.043 (3)   |      |
| H2   | 0.5214     | 0.7216       | 0.6642       | 0.052*      |      |
| C3   | 0.5363 (7) | 0.5000       | 0.6570 (16)  | 0.038 (3)   |      |
| O1W  | 0.2500     | 0.5000       | 0.8564 (14)  | 0.063 (6)   |      |
| H1W1 | 0.2500     | 0.4226       | 0.8198       | 0.095*      |      |
| O2W  | 0.3772 (8) | 0.0000       | 0.7518 (15)  | 0.079 (5)   |      |
| H1W2 | 0.410      | 0.0000       | 0.694        | 0.119*      |      |
| H2W2 | 0.332      | 0.0000       | 0.727        | 0.119*      |      |
| O3W  | 0.553 (3)  | 0.5000       | 0.960 (5)    | 0.27 (3)*   |      |
| H1W3 | 0.5644     | 0.5876       | 0.9741       | 0.402*      |      |
| O4W  | 0.429 (4)  | 0.0000       | 0.962 (6)    | 0.34 (3)*   |      |
| H1W4 | 0.386      | 0.0000       | 0.928        | 0.510*      |      |
| H2W4 | 0.466      | 0.0000       | 0.910        | 0.510*      |      |
|      |            |              |              |             |      |

Atomic displacement parameters  $(Å^2)$ 

| $U^{11}$   | $U^{22}$   | $U^{33}$   | $U^{12}$  | $U^{13}$   | $U^{23}$   |
|------------|--|--|---|--|--|
| 0.0230 (2) | 0.0289 (3)   | 0.0525 (4)   | 0.000   | 0.0066 (2)   | 0.000  |
| 0.0455 (4) | 0.0462 (4)   | 0.0574 (5)   | 0.000   | 0.000  | 0.0195 (3)   |
| 0.0337 (5) | 0.0436 (6)   | 0.0743 (8)   | 0.000   | 0.000  | -0.0133 (5)  |
| 0.0337 (5) | 0.0436 (6)   | 0.0743 (8)   | 0.000   | 0.000  | -0.0133 (5)  |
| 0.019 (4)  | 0.017 (5)  | 0.032 (6)  | 0.000   | 0.000  | 0.000  |
| 0.035 (5)  | 0.062 (9)  | 0.108 (12)   | 0.000   | 0.000  | -0.029 (9)   |
| 0.083 (11) | 0.078 (11)   | 0.082 (10)   | 0.000   | 0.000  | 0.065 (9)  |
| 0.023 (4)  | 0.046 (6)  | 0.081 (9)  | 0.000   | 0.012 (5)  | 0.000  |
| 0.066 (10) | 0.061 (11)   | 0.016 (6)  | 0.000   | 0.000  | 0.000  |
| 0.040 (4)  | 0.037 (4)  | 0.063 (5)  | 0.000 (4)   | 0.013 (4)  | 0.006 (4)  |
| 0.030 (4)  | 0.021 (4)  | 0.076 (8)  | 0.000   | 0.000  | 0.000 (5)  |
| 0.019 (2)  | 0.030 (3)  | 0.063 (5)  | 0.000 (3)   | 0.001 (3)  | -0.012 (3)   |
| 0.027 (6)  | 0.047 (9)  | 0.043 (8)  | 0.000   | 0.000  | 0.000  |
| 0.028 (6)  | 0.076 (12)   | 0.066 (11)   | 0.000   | -0.006 (6)   | 0.000  |
| 0.029 (5)  | 0.077 (12)   | 0.066 (10)   | 0.000   | 0.013 (6)  | 0.000  |
|            | $U^{11}$ 0.0230 (2) 0.0455 (4) 0.0337 (5) 0.0337 (5) 0.019 (4) 0.035 (5) 0.083 (11) 0.023 (4) 0.066 (10) 0.040 (4) 0.030 (4) 0.019 (2) 0.027 (6) 0.028 (6) 0.029 (5) | $U^{11}$ $U^{22}$ $0.0230$ (2) $0.0289$ (3) $0.0455$ (4) $0.0462$ (4) $0.0337$ (5) $0.0436$ (6) $0.0337$ (5) $0.0436$ (6) $0.019$ (4) $0.017$ (5) $0.035$ (5) $0.062$ (9) $0.083$ (11) $0.078$ (11) $0.023$ (4) $0.046$ (6) $0.066$ (10) $0.061$ (11) $0.040$ (4) $0.037$ (4) $0.030$ (4) $0.021$ (4) $0.019$ (2) $0.030$ (3) $0.027$ (6) $0.047$ (9) $0.028$ (6) $0.077$ (12) | $U^{11}$ $U^{22}$ $U^{33}$ 0.0230 (2)0.0289 (3)0.0525 (4)0.0455 (4)0.0462 (4)0.0574 (5)0.0337 (5)0.0436 (6)0.0743 (8)0.0337 (5)0.0436 (6)0.0743 (8)0.019 (4)0.017 (5)0.032 (6)0.035 (5)0.062 (9)0.108 (12)0.083 (11)0.078 (11)0.082 (10)0.023 (4)0.046 (6)0.081 (9)0.066 (10)0.061 (11)0.016 (6)0.030 (4)0.021 (4)0.076 (8)0.019 (2)0.030 (3)0.063 (5)0.027 (6)0.047 (9)0.043 (8)0.028 (6)0.076 (12)0.066 (10)0.029 (5)0.077 (12)0.066 (10) | $U^{11}$ $U^{22}$ $U^{33}$ $U^{12}$ 0.0230 (2)0.0289 (3)0.0525 (4)0.0000.0455 (4)0.0462 (4)0.0574 (5)0.0000.0337 (5)0.0436 (6)0.0743 (8)0.0000.0337 (5)0.0436 (6)0.0743 (8)0.0000.019 (4)0.017 (5)0.032 (6)0.0000.035 (5)0.062 (9)0.108 (12)0.0000.083 (11)0.078 (11)0.082 (10)0.0000.023 (4)0.046 (6)0.081 (9)0.0000.066 (10)0.061 (11)0.016 (6)0.0000.030 (4)0.021 (4)0.076 (8)0.0000.019 (2)0.030 (3)0.063 (5)0.000 (3)0.027 (6)0.047 (9)0.043 (8)0.0000.028 (6)0.076 (12)0.066 (10)0.0000.029 (5)0.077 (12)0.066 (10)0.000 | $U^{11}$ $U^{22}$ $U^{33}$ $U^{12}$ $U^{13}$ $0.0230(2)$ $0.0289(3)$ $0.0525(4)$ $0.000$ $0.0066(2)$ $0.0455(4)$ $0.0462(4)$ $0.0574(5)$ $0.000$ $0.000$ $0.0337(5)$ $0.0436(6)$ $0.0743(8)$ $0.000$ $0.000$ $0.0337(5)$ $0.0436(6)$ $0.0743(8)$ $0.000$ $0.000$ $0.0337(5)$ $0.0436(6)$ $0.0743(8)$ $0.000$ $0.000$ $0.0337(5)$ $0.0436(6)$ $0.0743(8)$ $0.000$ $0.000$ $0.0337(5)$ $0.0436(6)$ $0.0743(8)$ $0.000$ $0.000$ $0.019(4)$ $0.017(5)$ $0.032(6)$ $0.000$ $0.000$ $0.035(5)$ $0.062(9)$ $0.108(12)$ $0.000$ $0.000$ $0.033(11)$ $0.078(11)$ $0.082(10)$ $0.000$ $0.000$ $0.023(4)$ $0.046(6)$ $0.081(9)$ $0.000$ $0.012(5)$ $0.066(10)$ $0.061(11)$ $0.016(6)$ $0.000$ $0.000$ $0.040(4)$ $0.037(4)$ $0.063(5)$ $0.000(4)$ $0.013(4)$ $0.030(4)$ $0.021(4)$ $0.063(5)$ $0.000(3)$ $0.001(3)$ $0.027(6)$ $0.047(9)$ $0.043(8)$ $0.000$ $0.000$ $0.028(6)$ $0.076(12)$ $0.066(11)$ $0.000$ $-0.006(6)$ $0.029(5)$ $0.077(12)$ $0.066(10)$ $0.000$ $0.013(6)$ |

# supporting information

| C1  | 0.033 (5) | 0.053 (7)  | 0.080 (10) | 0.017 (5) | -0.014 (5) | 0.006 (7)  |  |
|-----|-----------|------------|------------|-----------|------------|------------|--|
| C2  | 0.037 (4) | 0.023 (4)  | 0.069 (8)  | 0.001 (4) | 0.003 (5)  | -0.001 (5) |  |
| C3  | 0.029 (5) | 0.029 (6)  | 0.056 (9)  | 0.000     | -0.015 (6) | 0.000      |  |
| O1W | 0.034 (7) | 0.13 (2)   | 0.027 (8)  | 0.000     | 0.000      | 0.000      |  |
| O2W | 0.057 (8) | 0.109 (14) | 0.071 (11) | 0.000     | 0.007 (7)  | 0.000      |  |

Geometric parameters (Å, °)

| 01C—W1                      | 2.2796 (8) | C2—C1                    | 1.339 (15)  |
|-----------------------------|------------|--------------------------|-------------|
| O1C—W1 <sup>i</sup>         | 2.2796 (8) | C2—H2                    | 0.9300      |
| O1C—W2 <sup>i</sup>         | 2.286 (9)  | C1—N1                    | 1.305 (13)  |
| O1C—W2                      | 2.286 (9)  | C1—H1                    | 0.9300      |
| O1C—Re1                     | 2.318 (9)  | N1—C1 <sup>ii</sup>      | 1.305 (13)  |
| O1C—V1 <sup>i</sup>         | 2.318 (9)  | N1—H1A                   | 0.8600      |
| O1C—Re1 <sup>i</sup>        | 2.318 (9)  | O2E—W2                   | 1.707 (12)  |
| O3—W2                       | 1.883 (12) | W1—O4 <sup>iii</sup>     | 1.882 (7)   |
| O3—Re1                      | 1.925 (12) | W1—O2 <sup>iii</sup>     | 1.936 (9)   |
| O1E—Re1                     | 1.674 (14) | W1—Re1 <sup>i</sup>      | 3.2040 (11) |
| O4—W1                       | 1.882 (7)  | W1—Re1                   | 3.2040 (11) |
| O4—Re1                      | 1.885 (6)  | $W2-O2^{iv}$             | 1.921 (8)   |
| O5                          | 1.958 (9)  | W2—Re1                   | 3.2322 (18) |
| O5—Re1 <sup>i</sup>         | 1.958 (9)  | Re1—O4 <sup>iv</sup>     | 1.885 (6)   |
| O5—Re1                      | 1.958 (9)  | Re1—W1 <sup>i</sup>      | 3.2040 (11) |
| O3E—W1                      | 1.718 (10) | N2—H2A                   | 0.8600      |
| O2—W2                       | 1.921 (8)  | O1W—H1W1                 | 0.81        |
| O2—W1                       | 1.936 (9)  | O2W—H1W2                 | 0.85        |
| O1—W2                       | 1.895 (7)  | O2W—H2W2                 | 0.85        |
| O1—W2 <sup>i</sup>          | 1.895 (7)  | O3W—H1W3                 | 0.84        |
| C3—N2                       | 1.307 (17) | O4W—H1W4                 | 0.85        |
| C3—C2 <sup>ii</sup>         | 1.414 (12) | O4W—H2W4                 | 0.85        |
| C3—C2                       | 1.414 (12) |                          |             |
|                             |            |                          |             |
| W1-O1C-W1 <sup>i</sup>      | 175.3 (6)  | O2—W1—Re1                | 80.8 (2)    |
| W1-O1C-W2 <sup>i</sup>      | 91.6 (2)   | O1C—W1—Re1               | 46.3 (2)    |
| $W1^{i}$ — $O1C$ — $W2^{i}$ | 91.6 (2)   | Re1 <sup>i</sup> —W1—Re1 | 62.09 (5)   |
| W1—O1C—W2                   | 91.6 (2)   | O2E—W2—O3                | 101.2 (8)   |
| W1 <sup>i</sup> —O1C—W2     | 91.6 (2)   | O2E—W2—O1                | 105.1 (8)   |
| W2 <sup>i</sup> —O1C—W2     | 90.7 (4)   | O3—W2—O1                 | 153.7 (5)   |
| W1—O1C—Re1                  | 88.4 (2)   | O2E—W2—O2                | 103.9 (3)   |
| W1 <sup>i</sup> —O1C—Re1    | 88.4 (2)   | O3—W2—O2                 | 87.1 (3)    |
| W2 <sup>i</sup> —O1C—Re1    | 179.9 (4)  | O1—W2—O2                 | 86.7 (3)    |
| W2—O1C—Re1                  | 89.19 (5)  | $O2E$ — $W2$ — $O2^{iv}$ | 103.9 (3)   |
| W1-O1C-V1 <sup>i</sup>      | 88.4 (2)   | $O3$ — $W2$ — $O2^{iv}$  | 87.1 (3)    |
| $W1^{i}$ — $O1C$ — $V1^{i}$ | 88.4 (2)   | $O1$ — $W2$ — $O2^{iv}$  | 86.7 (3)    |
| $W2^{i}$ — $O1C$ — $V1^{i}$ | 89.19 (5)  | $O2$ — $W2$ — $O2^{iv}$  | 152.2 (5)   |
| $W2-O1C-V1^i$               | 179.9 (4)  | O2E—W2—O1C               | 179.4 (7)   |
| Re1-O1C-V1 <sup>i</sup>     | 90.9 (4)   | O3—W2—O1C                | 78.1 (4)    |
| W1-O1C-Re1 <sup>i</sup>     | 88.4 (2)   | O1—W2—O1C                | 75.6 (4)    |

| WHI OLD DI                            |                      | 00 W/0 010                        |                       |
|---------------------------------------|----------------------|-----------------------------------|-----------------------|
| W1 <sup>1</sup> —O1C—Re1 <sup>1</sup> | 88.4 (2)             | 02—W2—O1C                         | 76.1 (3)              |
| W2 <sup>i</sup> —O1C—Re1 <sup>i</sup> | 89.19 (5)            | $O2^{iv}$ —W2—O1C                 | 76.1 (3)              |
| W2—O1C—Re1 <sup>i</sup>               | 179.9 (4)            | O2E—W2—Re1                        | 133.6 (7)             |
| Re1—O1C—Re1 <sup>i</sup>              | 90.9 (4)             | O3—W2—Re1                         | 32.3 (3)              |
| W2—O3—Re1                             | 116.1 (5)            | O1—W2—Re1                         | 121.4 (4)             |
| W1                                    | 116.6 (4)            | O2—W2—Re1                         | 80.3 (3)              |
| V1 <sup>i</sup> —O5—Re1               | 115.1 (8)            | O2 <sup>iv</sup> —W2—Re1          | 80.3 (3)              |
| Re1 <sup>i</sup> —O5—Re1              | 115.1 (8)            | O1C—W2—Re1                        | 45.8 (2)              |
| W2                                    | 116.2 (4)            | O1E—Re1—O4                        | 102.9 (2)             |
| $W2-O1-W2^{i}$                        | 118.2 (7)            | $O1E$ —Re1— $O4^{iv}$             | 102.9 (2)             |
| N2—C3—C2 <sup>ii</sup>                | 120.6 (6)            | O4—Re1—O4 <sup>iv</sup>           | 154.0 (4)             |
| N2—C3—C2                              | 120.6 (6)            | O1E—Re1—O3                        | 105.0 (7)             |
| C2 <sup>ii</sup> —C3—C2               | 118.6 (12)           | O4—Re1—O3                         | 88.1 (3)              |
| C1—C2—C3                              | 119.0 (11)           | O4 <sup>iv</sup> —Re1—O3          | 88.1 (3)              |
| C1—C2—H2                              | 120.5                | O1E—Re1—O5                        | 101.5 (7)             |
| С3—С2—Н2                              | 120.5                | O4—Re1—O5                         | 86.0 (3)              |
| N1—C1—C2                              | 117.1 (12)           | O4 <sup>iv</sup> —Re1—O5          | 86.0 (3)              |
| N1—C1—H1                              | 121.4                | O3—Re1—O5                         | 153.5 (5)             |
| С2—С1—Н1                              | 121.4                | O1E—Re1—O1C                       | 178.5 (7)             |
| $C1^{ii}$ —N1—C1                      | 128.8 (14)           | 04—Re1— $01C$                     | 77.0 (2)              |
| $C1^{ii}$ $N1$ $H1A$                  | 115.6                | $O4^{iv}$ —Re1—O1C                | 77.0(2)               |
| C1—N1—H1A                             | 115.6                | $O_3$ —Re1—O1C                    | 76.6 (4)              |
| O3E - W1 - O4                         | 104 2 (4)            | 05—Re1—01C                        | 77.0 (4)              |
| $O3E - W1 - O4^{iii}$                 | 1042(4)              | $\Omega IE Re1 W1^{i}$            | $134\ 60\ (4)$        |
| $04 - W1 - 04^{iii}$                  | 89 5 (5)             | O4—Re1—W1 <sup>i</sup>            | 1273(2)               |
| $O3F - W1 - O2^{iii}$                 | 101.6(4)             | $O4^{iv}$ Re1 $W1^{i}$            | 31.7(2)               |
| $O_4 W_1 O_2^{iii}$                   | 154.0(3)             | $O_3$ Rel Wl <sup>i</sup>         | $\frac{31.7}{2}$      |
| $O^{iii}$ W1 $O^{2iii}$               | 873(4)               | O5 Rel Wl <sup>i</sup>            | 70.7(3)               |
| $O_{4} = W_{1} = O_{2}$               | 101.6(4)             | O1C Re1 W1 <sup>i</sup>           | 15.7 (5)<br>15.33 (2) |
| 0.5E - W1 - 0.2                       | 87.3(4)              | O1E $Pe1$ $W1$                    | +3.33(2)              |
| 04 - W1 - 02                          | 57.3(4)              | $O_1 = M_1$ $O_2 = M_1$           | 134.00(4)             |
| $O_4 = W_1 = O_2$                     | 134.0(3)             | $O_4$ Ref W1                      | 31.7(2)               |
| $02 - w_1 - 02$                       | 1767(6)              | $O_4 = Re1 = W1$                  | 122.3(2)              |
| 0.05E - WI - 0.1C                     | 1/0.7(0)             | $O_5 = Re1 = W1$                  | 31.0(2)               |
| 04 - WI - 01C                         | 78.1 (3)<br>78.1 (2) | $O_{1}C_{1}$ $D_{2}1_{1}$ $W_{1}$ | 79.7 (3)<br>45.22 (2) |
| 04 <sup></sup> —w1—01C                | 78.1(3)              | VIC—KeI—WI                        | 45.55 (2)             |
| $02^{}$ wi $-010^{}$                  | 70.0(3)              | WI - KeI - WI                     | 90.62 (4)             |
| 02 - WI - OIC                         | /6.0 (3)             | OIE—ReI—W2                        | 136.5 (6)             |
| $O_{3E}$ WI Rel                       | 130.0(3)             | O4—ReI—W2                         | 81.7 (3)              |
| O4-WI-ReI1                            | 82.9 (2)             | $O4^{W}$ —Re1—W2                  | 81.7 (3)              |
| $O4^{m} - WI - ReI^{n}$               | 31.75 (19)           | O3—Rel—W2                         | 31.5 (3)              |
| O2 <sup>m</sup> —W1—Rel <sup>1</sup>  | 80.8 (2)             | O5—ReI—W2                         | 122.0 (4)             |
| $O2-W1-Rel^{1}$                       | 122.3 (2)            | OIC—ReI—W2                        | 45.0 (2)              |
| OIC—WI—Rel <sup>1</sup>               | 46.3 (2)             | W1 <sup>i</sup> —Re1—W2           | 61.16(3)              |
| O3E—W1—Rel                            | 136.0 (3)            | WI—Rel—W2                         | 61.16 (3)             |
| O4—W1—Re1                             | 31.75 (19)           | C3—N2—H2A                         | 121                   |
| $O4^{m}$ —W1—Re1                      | 82.9 (2)             | H1W2—O2W—H2W2                     | 116                   |
| O2 <sup>iii</sup> —W1—Re1             | 122.3 (2)            | H1W4—O4W—H2W4                     | 116                   |

| N2-C3-C2-C1                                | -178.7 (16) | W1 <sup>i</sup> —O1C—Re1—W2        | -91.7 (2)   |
|--|-------------|------------------------------------|-------------|
| C2 <sup>ii</sup> —C3—C2—C1                 | -2 (3)      | O3E—W1—Re1—O1E                     | -5.6 (10)   |
| C3—C2—C1—N1                                | -1 (2)      | O4—W1—Re1—O1E                      | -3.2 (10)   |
| C2-C1-N1-C1 <sup>ii</sup>                  | 6 (3)       | O4 <sup>iii</sup> —W1—Re1—O1E      | 97.6 (9)    |
| Re1—O4—W1—O3E                              | 178.3 (5)   | O2—W1—Re1—O1E                      | -102.8(9)   |
| Re1—O4—W1—O4 <sup>iii</sup>                | -77.1 (5)   | O1C—W1—Re1—O1E                     | 177.8 (9)   |
| Re1-04-W1-02 <sup>iii</sup>                | 5.6 (11)    | Rel <sup>i</sup> —W1—Re1—O1E       | 122.9 (9)   |
| Re1—O4—W1—O2                               | 77.0 (5)    | O3E—W1—Re1—O4                      | -2.4 (7)    |
| Re1—O4—W1—O1C                              | 0.7 (4)     | O4 <sup>iii</sup> —W1—Re1—O4       | 100.7 (7)   |
| Re1-O4-W1-Re1 <sup>i</sup>                 | -46.0 (4)   | O2 <sup>iii</sup> —W1—Re1—O4       | -177.1 (6)  |
| W2-02-W1-03E                               | 179.7 (5)   | O2—W1—Re1—O4                       | -99.7 (6)   |
| W2-02-W1-04                                | -76.3 (5)   | O1C—W1—Re1—O4                      | -179.0 (6)  |
| W2-02-W1-04 <sup>iii</sup>                 | 6.9 (12)    | Rel <sup>i</sup> —W1—Re1—O4        | 126.1 (5)   |
| W2-02-W1-02 <sup>iii</sup>                 | 78.9 (5)    | $O3E$ — $W1$ — $Re1$ — $O4^{iv}$   | 179.8 (6)   |
| W2-02-W1-01C                               | 2.0 (4)     | O4—W1—Re1—O4 <sup>iv</sup>         | -177.8 (8)  |
| W2—O2—W1—Re1 $^{i}$                        | 3.5 (6)     | $O4^{iii}$ —W1—Re1— $O4^{iv}$      | -77.05 (19) |
| W2-O2-W1-Re1                               | -45.1 (4)   | $O2^{iii}$ —W1—Re1— $O4^{iv}$      | 5.1 (4)     |
| W2 <sup>i</sup> —O1C—W1—O4                 | 179.3 (4)   | O2—W1—Re1—O4 <sup>iv</sup>         | 82.5 (4)    |
| W2-01C-W1-04                               | 88.6 (3)    | $O1C$ — $W1$ — $Re1$ — $O4^{iv}$   | 3.2 (4)     |
| Re1—O1C—W1—O4                              | -0.5 (3)    | $Re1^{i}$ W1 Re1 O4 <sup>iv</sup>  | -51.7 (3)   |
| V1 <sup>i</sup> —O1C—W1—O4                 | -91.5 (4)   | O3E—W1—Re1—O3                      | 97.4 (5)    |
| Rel <sup>i</sup> —O1C—W1—O4                | -91.5 (4)   | O4—W1—Re1—O3                       | 99.8 (5)    |
| W2 <sup>i</sup> —O1C—W1—O4 <sup>iii</sup>  | -88.6 (3)   | O4 <sup>iii</sup> —W1—Re1—O3       | -159.5 (3)  |
| W2-01C-W1-04 <sup>iii</sup>                | -179.3 (4)  | O2 <sup>iii</sup> —W1—Re1—O3       | -77.3 (4)   |
| Re1—O1C—W1—O4 <sup>iii</sup>               | 91.5 (4)    | O2—W1—Re1—O3                       | 0.1 (3)     |
| V1 <sup>i</sup> O1CW1O4 <sup>iii</sup>     | 0.5 (3)     | O1C—W1—Re1—O3                      | -79.2 (4)   |
| Re1 <sup>i</sup> —O1C—W1—O4 <sup>iii</sup> | 0.5 (3)     | Rel <sup>i</sup> —W1—Re1—O3        | -134.1 (2)  |
| W2 <sup>i</sup> —O1C—W1—O2 <sup>iii</sup>  | 1.5 (3)     | O3E—W1—Re1—O5                      | -101.6 (6)  |
| W2-O1C-W1-O2 <sup>iii</sup>                | -89.2 (4)   | O4—W1—Re1—O5                       | -99.2 (6)   |
| Re1—O1C—W1—O2 <sup>iii</sup>               | -178.3 (4)  | O4 <sup>iii</sup> —W1—Re1—O5       | 1.5 (4)     |
| V1 <sup>i</sup> —O1C—W1—O2 <sup>iii</sup>  | 90.7 (3)    | O2 <sup>iii</sup> —W1—Re1—O5       | 83.7 (4)    |
| Re1 <sup>i</sup> —O1C—W1—O2 <sup>iii</sup> | 90.7 (3)    | O2—W1—Re1—O5                       | 161.1 (4)   |
| W2 <sup>i</sup> -O1C-W1-O2                 | 89.2 (4)    | O1C—W1—Re1—O5                      | 81.8 (4)    |
| W2-01C-W1-02                               | -1.5 (3)    | Rel <sup>i</sup> —W1—Re1—O5        | 26.9 (3)    |
| Re1—O1C—W1—O2                              | -90.7 (3)   | O3E—W1—Re1—O1C                     | 176.6 (6)   |
| V1 <sup>i</sup>                            | 178.3 (4)   | O4—W1—Re1—O1C                      | 179.0 (6)   |
| Re1 <sup>i</sup> —O1C—W1—O2                | 178.3 (4)   | O4 <sup>iii</sup> —W1—Re1—O1C      | -80.3 (4)   |
| W2 <sup>i</sup> —O1C—W1—Re1 <sup>i</sup>   | -89.14 (5)  | O2 <sup>iii</sup> —W1—Re1—O1C      | 1.9 (4)     |
| W2-O1C-W1-Rel <sup>i</sup>                 | -179.9 (4)  | O2—W1—Re1—O1C                      | 79.3 (4)    |
| Re1—O1C—W1—Re1 <sup>i</sup>                | 91.0 (4)    | Rel <sup>i</sup> —W1—Re1—O1C       | -54.9 (3)   |
| V1 <sup>i</sup> —O1C—W1—Re1 <sup>i</sup>   | 0.0         | O3E—W1—Re1—W1 <sup>i</sup>         | 179.0 (5)   |
| W2 <sup>i</sup> —O1C—W1—Re1                | 179.9 (4)   | O4—W1—Re1—W1 <sup>i</sup>          | -178.6 (5)  |
| W2-O1C-W1-Re1                              | 89.14 (5)   | $O4^{iii}$ —W1—Re1—W1 <sup>i</sup> | -77.9 (2)   |
| V1 <sup>i</sup> —O1C—W1—Re1                | -91.0 (4)   | $O2^{iii}$ —W1—Re1—W1 <sup>i</sup> | 4.3 (3)     |
| Re1 <sup>i</sup> —O1C—W1—Re1               | -91.0 (4)   | O2-W1-Re1-W1 <sup>i</sup>          | 81.7 (3)    |
| Re1—O3—W2—O2                               | -76.4 (2)   | O1C-W1-Re1-W1 <sup>i</sup>         | 2.4 (3)     |
| Re1-03-W2-02 <sup>iv</sup>                 | 76.4 (2)    | $Re1^{i}$ W1 Re1 $W1^{i}$          | -52.53 (4)  |
| W2 <sup>i</sup> -O1-W2-O2                  | 76.5 (3)    | O3E—W1—Re1—W2                      | 122.8 (5)   |
|  |             |                                    |             |

| $W2^{i}$ —O1—W2—O2 <sup>iv</sup>     | -76.5(3)  | O4—W1—Re1—W2   | 125.2 (5)                  |
|--------------------------------------|-----------|--|----------------------------|
| W1                                   | 177.3 (8) | $O4^{iii}$ —W1—Re1—W2  | -134.1 (2)                 |
| W1—O2—W2—O3                          | 76.5 (6)  | $O2^{iii}$ —W1—Re1—W2  | -51.9(3)                   |
| W1                                   | -78.0 (6) | O2—W1—Re1—W2   | 25.5 (3)                   |
| W1-02-W2-02 <sup>iv</sup>            | -1.5 (16) | O1C—W1—Re1—W2  | -53.8 (3)                  |
| W1-02-W2-01C                         | -2.0(4)   | $Re1^{i}$ W1 Re1 W2  | -108.71(2)                 |
| W1-O2-W2-Re1                         | 44.6 (4)  | O2—W2—Re1—O1E  | 100.0 (3)                  |
| W1-01C-W2-02                         | 1.5 (3)   | $O2^{iv}$ —W2—Re1—O1E  | -100.0(3)                  |
| $W1^{i}-O1C-W2-O2$                   | 178.2 (4) | O2E - W2 - Re1 - O4  | -100.0(2)                  |
| Re1-O1C-W2-O2                        | 89.9 (3)  | $O_3 - W_2 - Re_1 - O_4$   | -100.0(2)                  |
| $W1 - O1C - W2 - O2^{iv}$            | -178.2(4) | O1-W2-Re1-O4   | 80.0 (2)                   |
| $W1^{i}$ — $O1C$ — $W2$ — $O2^{iv}$  | -1.5(3)   | O2-W2-Re1-O4   | -0.1(3)                    |
| $Re1 - O1C - W2 - O2^{iv}$           | -899(3)   | $O2^{iv} W^2 Re1 O1$   | 160.0(3)                   |
| W1 - 04 - Re1 - 01E                  | 177.7(7)  | O1C - W2 - Re1 - O4  | 80.0(2)                    |
| $W1 - O4 - Re1 - O4^{iv}$            | 43(15)    | $\Omega^2 F W^2 Re1 \Omega^{iv}$   | 100.0(2)                   |
| W1 - 04 - Re1 - 03                   | -774(5)   | $M^{2}$ $M^{2$ | 100.0(2)                   |
| W1 - 04 - Re1 - 05                   | 76.8 (6)  | $\Omega_1 - W_2 - Re_1 - \Omega_4^{iv}$  | -80.0(2)                   |
| W1 - O4 - Re1 - O1C                  | -0.7(4)   | $\Omega^2 - W^2 - Re1 - \Omega^{4iv}$  | -160.0(2)                  |
| $W1 - O4 - Re1 - W1^{i}$             | 16(6)     | $\Omega^{2iv}$ W2 Ref Of<br>$\Omega^{2iv}$ W2 Ref $\Omega^{4iv}$   | 01(3)                      |
| W1 = 04 Re1 = $W2$                   | -46.3(4)  | $\Omega_1 C - W^2 - Re^{1} - \Omega_1^{iv}$  | -80.0(2)                   |
| $W^{2} = 0^{3} = Re^{1} = 0^{4}$     | 77 1 (2)  | O2F - W2 - Re1 - O3  | 0.000(2)                   |
| $W_2 = 0.3 = Re1 = 0.4^{iv}$         | -771(2)   | $01 - W^2 - Re1 - 03$  | 180,000,(2)                |
| $W^{2} = O^{3} = Re^{1} = W^{1^{i}}$ | -45.92(4) | $\Omega^2 - W^2 - Re1 - \Omega^3$  | 100.000(2)<br>100.0(3)     |
| $W^2 = O^3 = Re1 = W^1$              | 45 92 (4) | $\Omega^{2iv}$ W2 Rel $\Omega^{3}$   | -100.0(3)                  |
| $V1^{i}$ 05Re104                     | -77.6(2)  | $01C - W^2 - Re1 - 03$   | 180,000,(2)                |
| $Re1^{i} - 05 - Re1 - 04$            | -77.6(2)  | $\Omega^{2}F_{W^{2}}=Re1=\Omega^{5}$   | 180.000(2)<br>180.000(1)   |
| $V1^{i}$ _05_Re1_04^{iv}             | 77.6 (2)  | $M^{2} = W^{2} = Re1 = 05$   | 180.000(1)                 |
| $Re1^{i} - 05 - Re1 - 04^{iv}$       | 77.6 (2)  | $0.1 - W^2 - Re1 - 0.5$  | 0.000(1)                   |
| $V1^{i}$ 05 Re1 $V1^{i}$             | 46.26(5)  | $\Omega^2 - W^2 - Re1 - \Omega^5$  | -80.0(3)                   |
| $Re1^{i} - O5 - Re1 - W1^{i}$        | 46.26 (5) | $\Omega^{2iv}$ W2 Rel $\Omega^{5}$   | 80.0 (3)                   |
| $V1^{i}$ 05 Re1 W1                   | -46.26(5) | $02 - W^2 - Re^1 - 05$   | 0.00(3)                    |
| $Re1^{i} - O5 - Re1 - W1$            | -46.26(5) | O2F - W2 - Re1 - O1C   | 180.0                      |
| W1 - 01C - Re1 - 04                  | 0.5(3)    | $M^{2} = W^{2} = Re1 = 01C$  | 180.0                      |
| $W1^{i}$ $-01C$ $Re1$ $-04$          | 177 2 (4) | $0.1 - W^2 - Re1 - 0.1C$   | 0.0                        |
| $V1^{i}$ $O1C$ $Re1$ $O4$            | 88 9 (3)  | $\Omega^2 - W^2 - Re1 - \Omega^1 C$  | -80.0(3)                   |
| $Rel^{i}$ OlC Rel O4                 | 88.9(3)   | $\Omega^{2iv}$ W2 Ref 010  | 80.0 (3)                   |
| $W_1 = O_1C = Re_1 = O_4^{iv}$       | -1772(4)  | $O2F W2 Re1 W1^{i}$  | $125\ 752\ (18)$           |
| $W1^{i}$ $O1C$ $Re1$ $O4^{iv}$       | -0.5(3)   | $O_2L = W_2 = Re1 = W_1^i$   | 125.752(18)<br>125.752(18) |
| $V1^{i}$ $O1C$ $Re1$ $O4^{iv}$       | -889(3)   | $0.1 - W^2 - Re^1 - W^{1i}$  | $-54\ 248\ (18)$           |
| $Re1^{i} - O1C - Re1 - O4^{iv}$      | -889(3)   | $\Omega^2 - W^2 - Re1 - W1^{i}$  | -1343(3)                   |
| $W_1 = 01C = Re1 = 05$               | -883(2)   | $\Omega^{2iv}$ W2 Ref W1   | $25 \ 8 \ (3)$             |
| $W1^{i}$ $O1C$ $Re1$ $O5$            | 88 3 (2)  | $O1C - W2 - Re1 - W1^{i}$  | -54.248(18)                |
| $W1 = O1C = Re1 = W1^{i}$            | -1767(4)  | O2F W2 Re1 W1  | -125 752 (18)              |
| $V1^{i}$ $O1C$ $Re1$ $W1^{i}$        | -883(2)   | $M^{2} = W^{2} = W^{2}$  | -125.752(18)               |
| $Re1^{i} - O1C - Re1 - W1^{i}$       | -883(2)   | 01 - W2 - Re1 - W1   | 54 248 (18)                |
| $W1^{i}$ $O1C$ $Re1$ $W1$            | 176.7(4)  | $O_2 W_2 Re1 W_1$  | -25 & (3)                  |
| $V1^{i}$ $O1C$ $Re1$ $W1$            | 88 3 (2)  | $\Omega^{2iv}$ W2 Re1 W1   | 134 3 (3)                  |
| , I U I U I U I "W I                 | 00.0 (4)  |  | 107.0 (0)                  |

# supporting information

| Rel <sup>i</sup> —O1C—Re1—W1 | 88.3 (2) | O1C—W2—Re1—W1 | 54.248 (18) |
|------------------------------|----------|---------------|-------------|
| W1—O1C—Re1—W2                | 91.7 (2) |               |             |

Symmetry codes: (i) -*x*+1/2, -*y*, *z*; (ii) *x*, -*y*+1, *z*; (iii) *x*, -*y*, *z*; (iv) -*x*+1/2, *y*, *z*.

### Hydrogen-bond geometry (Å, °)

| D—H···A                                  | D—H  | H···A | D··· $A$   | <i>D</i> —H··· <i>A</i> |
|--|------|-------|------------|-------------------------|
| N1—H1A····O1W                            | 0.86 | 2.40  | 3.078 (14) | 136                     |
| N1—H1 <i>A</i> ···O1 <i>E</i>            | 0.86 | 2.58  | 3.184 (14) | 129                     |
| N2—H2 $A$ ···O3 <sup>v</sup>             | 0.86 | 2.39  | 3.181 (12) | 152                     |
| O1 <i>W</i> —H1 <i>W</i> 1···O1 <i>E</i> | 0.81 | 2.50  | 3.188 (18) | 144                     |
| $O2W$ —H1 $W2$ ···O3 $E^{vi}$            | 0.85 | 2.10  | 2.836 (18) | 144                     |
| O4 <i>W</i> —H1 <i>W</i> 4···O2 <i>W</i> | 0.85 | 1.87  | 2.40 (7)   | 119                     |
| O4W— $H2W4$ ···O $4W$ <sup>vii</sup>     | 0.85 | 2.31  | 2.65 (15)  | 106                     |
|  |      |       |            |                         |

Symmetry codes: (v) *x*+1/2, *y*, -*z*+1; (vi) -*x*+1, -*y*, -*z*+1; (vii) -*x*+1, -*y*, -*z*+2.