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## Barium dierbium(III) tetrasulfide

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Key indicators: single-crystal X-ray study; $T=100 \mathrm{~K}$; mean $\sigma(\mathrm{Er}-\mathrm{S})=0.001 \AA$; $R$ factor $=0.017 ; w R$ factor $=0.050$; data-to-parameter ratio $=27.4$.

Barium dierbium(III) tetrasulfide, $\mathrm{BaEr}_{2} \mathrm{~S}_{4}$, crystallizes with four formula units in the orthorhombic space group Pnma in the $\mathrm{CaFe}_{2} \mathrm{O}_{4}$ structure type. The asymmetric unit contains two Er , one Ba , and four S atoms, each with.$m$. site symmetry. The structure consists of channels formed by corner- and edgesharing $\mathrm{ErS}_{6}$ octahedra in which Ba atoms reside. The resultant coordination of Ba is that of a bicapped trigonal prism.

## Related literature

The unit-cell parameters of $\mathrm{BaEr}_{2} \mathrm{~S}_{4}$, which crystallizes in the $\mathrm{CaFe}_{2} \mathrm{O}_{4}$ structure type (Decker \& Kasper, 1957), were previously determined from X-ray powder diffraction data (Patrie et al., 1964). For related structures, see: Bugaris \& Ibers (2009); Narducci et al. (2000); Carpenter \& Hwu (1992); Flahaut et al. (1965); Schurz \& Schleid (2011). For synthetic details, see: Bugaris \& Ibers (2008); Haneveld \& Jellinek (1969). For standardization of structural data, see: Gelato \& Parthé (1987).

## Experimental

## Crystal data

$\mathrm{BaEr}_{2} \mathrm{~S}_{4}$
$M_{r}=600.10$
Orthorhombic, Pnma
$a=12.1455$ (3) A
$b=3.9884$ (1) $\AA$
$c=14.3837(4) \AA$
$V=696.76(3) \AA^{3}$
$Z=4$
Mo $K \alpha$ radiation
$\mu=30.53 \mathrm{~mm}^{-1}$
$T=100 \mathrm{~K}$
$0.16 \times 0.03 \times 0.02 \mathrm{~mm}$

## Data collection

Bruker APEXII CCD
diffractometer
Absorption correction: numerical face indexed (Sheldrick, 2008a)
$T_{\text {min }}=0.084, T_{\text {max }}=0.528$

## Refinement

$R\left[F^{2}>2 \sigma\left(F^{2}\right)\right]=0.017$
$w R\left(F^{2}\right)=0.050$
$S=1.87$
1207 reflections

9866 measured reflections
1207 independent reflections
1196 reflections with $I>2 \sigma(I)$ $R_{\text {int }}=0.030$

$$
\begin{aligned}
& 44 \text { parameters } \\
& \Delta \rho_{\max }=2.46 \mathrm{e} \AA^{-3} \\
& \Delta \rho_{\min }=-2.58 \mathrm{e}^{-3}
\end{aligned}
$$

Data collection: APEX2 (Bruker, 2009); cell refinement: SAINT (Bruker, 2009); data reduction: SAINT; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008b); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008b); molecular graphics: CrystalMaker (Palmer, 2012); software used to prepare material for publication: SHELXL97.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: BR2222).

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# supporting information 

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## Barium dierbium(III) tetrasulfide

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## S1. Comment

Orange needles of $\mathrm{BaEr}_{2} \mathrm{~S}_{4}$ were obtained in a solid-state reaction. The compound was synthesized previously (Patrie et al., 1964), and its unit cell parameters were determined from X-powder diffraction data. In the $\mathrm{BaLn}_{2} \mathrm{~S}_{4}$ family ( $\mathrm{Ln}=$ rare earth element) no structures have been determined from single-crystal data but that of the closely related compound $\mathrm{BaLu}_{2} \mathrm{~S}_{4}$ has (Schurz \& Schleid, 2011). Here, from X-ray diffraction single-crystal data we find that $\mathrm{BaEr}_{2} \mathrm{~S}_{4}$ crystallizes in the $\mathrm{CaFe}_{2} \mathrm{O}_{4}$ structure type (Decker \& Kasper, 1957) with four formula units in space group Pnma of the orthorhombic system. In the asymmetric unit there are two Er , one Ba , and four S atoms, each with site symmetry .m. A projection of the structure down [010] is shown in Figure 1. The structure consists of $\mathrm{ErS}_{6}$ octahedra that form dimers by edge-sharing. Four such dimers form an infinite channel by corner-sharing in the (010) plane. Each channel is filled by one Ba atom. Each Er1 atom is octahedrally coordinated to one S2, three S3, and two S4 atoms; each Er2 atom is coordinated to three S1, two S2, and one S4 atom. The interatomic Er - S distances at 2.6706 (10) to 2.7376 (7) $\AA$ compare favorably to those of 2.672 (4) to 2.720 (4) $\AA$ in the structure of $\mathrm{BaLu}_{2} \mathrm{~S}_{4}$ (Schurz \& Schleid, 2011). As there are no $\mathrm{S}-\mathrm{S}$ bonds in the structure, formal oxidation states may be assigned as $\mathrm{Ba}^{2+}, \mathrm{Er}^{3+}$, and $\mathrm{S}^{2-}$.

## S2. Experimental

In an exploration of the quaternary solid-state $\mathrm{Ba} / \mathrm{Er} / \mathrm{U} / \mathrm{S}$ system, orange needles of $\mathrm{BaEr}_{2} \mathrm{~S}_{4}$ were obtained instead in a two-step reaction. Uranium powder was obtained by hydridization and decomposition of ${ }^{238} \mathrm{U}$ turnings (Oak Ridge National Laboratory) (Bugaris \& Ibers, 2008; Haneveld \& Jellinek, 1969). The other reactants were used as obtained. In the first step, a mixture consisting of powdered ${ }^{238} \mathrm{U}(20.9 \mathrm{mg}, 0.088 \mathrm{mmol}), \mathrm{Er}(14.0 \mathrm{mg}, 0.084 \mathrm{mmol}), \mathrm{BaS}(42.7 \mathrm{mg}$, $0.252 \mathrm{mmol})$, and $\mathrm{S}(8.0 \mathrm{mg}, 0.25 \mathrm{mmol})$ was loaded into a carbon-coated fused-silica tube under an Ar atmosphere in a glove box. The tube was evacuated to $10^{-4} \mathrm{Torr}$, and flame sealed. It was placed in computer-contolled furnace, heated to 1273 K in 48 h , held there for 8 d , then cooled to 293 K at $3 \mathrm{~K} / \mathrm{h}$. In the second step, the resultant black powder was ground and mixed thoroughly with 50 mg of $\mathrm{Sb}_{2} \mathrm{~S}_{3}$. This mixture was re-loaded into a carbon-coated fused-silica tube, evacuated, sealed, and then placed in a computer-controlled furnace The tube was heated to 1273 K in 24 h , held there for 4 d , then cooled to 293 K at $2 \mathrm{~K} / \mathrm{h}$. Orange needles were obtained in about $50 \mathrm{wt} \%$ yield. Analysis of these orange crystals on an EDX- equipped Hitachi S-3400 SEM showed the presence of $\mathrm{Ba}, \mathrm{Er}$, and S in the approximate ratio 1:2:4 but no U . The other products were black crystals of $\mathrm{Sb}_{2} \mathrm{~S}_{3}$ and $\mathrm{US}_{2}$.

## S3. Refinement

The structure was standardized by means of the program STRUCTURE TIDY ((Gelato \& Parthé, 1987). The highest peak in the difference electron density map $\left(2.46\right.$ e. $\left.\AA^{-3}\right)$ was $0.47 \AA$ from atom Er1 and the deepest hole $\left(-2.58 \mathrm{e} . \AA^{-3}\right)$ was $0.20 \AA$ from atom Ba1.


Figure 1
Structure of $\mathrm{BaEr}_{2} \mathrm{~S}_{4}$ viewed approximatly down [010]. Displacement ellipsoids are drawn at $95 \%$ probability level.

## Barium dierbium(III) tetrasulfide

## Crystal data

## $\mathrm{BaEr}_{2} \mathrm{~S}_{4}$

$M_{r}=600.10$
Orthorhombic, Pnma
Hall symbol: -P 2ac 2n
$a=12.1455$ (3) $\AA$
$b=3.9884$ (1) $\AA$
$c=14.3837(4) \AA$
$V=696.76$ (3) $\AA^{3}$
$Z=4$

## Data collection

Bruker APEXII CCD
diffractometer
Radiation source: fine-focus sealed tube
Graphite monochromator
$\varphi$ and $\omega$ scans
$F(000)=1024$
$D_{\mathrm{x}}=5.721 \mathrm{Mg} \mathrm{m}^{-3}$
Mo $K \alpha$ radiation, $\lambda=0.71073 \AA$
Cell parameters from 8150 reflections
$\theta=2.3-30.5^{\circ}$
$\mu=30.53 \mathrm{~mm}^{-1}$
$T=100 \mathrm{~K}$
Needle, orange
$0.16 \times 0.03 \times 0.02 \mathrm{~mm}$

Absorption correction: numerical
face indexed (Sheldrick, 2008a)
$T_{\text {min }}=0.084, T_{\text {max }}=0.528$
9866 measured reflections
1207 independent reflections
1196 reflections with $I>2 \sigma(I)$

$$
\begin{aligned}
& R_{\text {int }}=0.030 \\
& \theta_{\max }=30.5^{\circ}, \theta_{\min }=2.2^{\circ} \\
& h=-17 \rightarrow 17
\end{aligned}
$$

## Refinement

Refinement on $F^{2}$
Least-squares matrix: full
$R\left[F^{2}>2 \sigma\left(F^{2}\right)\right]=0.017$
$w R\left(F^{2}\right)=0.050$
$S=1.87$
1207 reflections
44 parameters
0 restraints
Primary atom site location: structure-invariant direct methods
$k=-5 \rightarrow 5$
$l=-20 \rightarrow 20$

Secondary atom site location: difference Fourier map
$1 /\left[\mathrm{s}^{2}\left(F_{\mathrm{o}}{ }^{2}\right)+\left(0.0192 F_{\mathrm{o}}{ }^{2}\right)^{2}\right]$
$(\Delta / \sigma)_{\text {max }}=0.002$
$\Delta \rho_{\text {max }}=2.46 \mathrm{e}^{-3}$
$\Delta \rho_{\text {min }}=-2.58$ e $\AA^{-3}$
Extinction correction: SHELXL97 (Sheldrick, 2008a), $\mathrm{Fc}^{*}=\mathrm{kFc}\left[1+0.001 \mathrm{xFc}^{2} \lambda^{3} / \sin (2 \theta)\right]^{-1 / 4}$
Extinction coefficient: 0.00257 (16)

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters ( $A^{2}$ )

|  | $x$ | $y$ | $z$ | $U_{\text {iso }} * / U_{\text {eq }}$ |
| :--- | :--- | :--- | :--- | :--- |
| Er1 | $0.079448(16)$ | 0.2500 | $0.398817(12)$ | $0.00349(8)$ |
| Er2 | $0.566211(16)$ | 0.2500 | $0.608465(12)$ | $0.00444(8)$ |
| Ba1 | $0.24191(2)$ | 0.2500 | $0.662667(18)$ | $0.00705(9)$ |
| S1 | $0.08229(8)$ | 0.2500 | $0.07671(7)$ | $0.00485(18)$ |
| S2 | $0.29294(9)$ | 0.2500 | $0.33808(7)$ | $0.00537(18)$ |
| S3 | $0.37564(8)$ | 0.2500 | $0.02341(7)$ | $0.00449(18)$ |
| S4 | $0.47727(8)$ | 0.2500 | $0.78311(7)$ | $0.00490(18)$ |

Atomic displacement parameters $\left(\hat{A}^{2}\right)$

|  | $U^{11}$ | $U^{22}$ | $U^{33}$ | $U^{12}$ | $U^{13}$ | $U^{23}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Er1 | $0.00359(11)$ | $0.00300(12)$ | $0.00388(11)$ | 0.000 | $0.00010(5)$ | 0.000 |
| Er2 | $0.00495(12)$ | $0.00349(12)$ | $0.00487(11)$ | 0.000 | $-0.00020(5)$ | 0.000 |
| Ba1 | $0.00595(14)$ | $0.00835(14)$ | $0.00683(13)$ | 0.000 | $0.00015(8)$ | 0.000 |
| S1 | $0.0057(4)$ | $0.0040(4)$ | $0.0049(4)$ | 0.000 | $-0.0004(3)$ | 0.000 |
| S2 | $0.0037(4)$ | $0.0044(4)$ | $0.0080(4)$ | 0.000 | $-0.0006(3)$ | 0.000 |
| S3 | $0.0046(4)$ | $0.0037(4)$ | $0.0052(4)$ | 0.000 | $0.0009(3)$ | 0.000 |
| S4 | $0.0061(4)$ | $0.0039(4)$ | $0.0047(4)$ | 0.000 | $0.0015(3)$ | 0.000 |

Geometric parameters ( $\AA$, ${ }^{\circ}$ )

| Er1-S4 ${ }^{\text {i }}$ | 2.6872 (6) | $\mathrm{Ba}-\mathrm{S} 4$ | 3.3426 (11) |
| :---: | :---: | :---: | :---: |
| Er1—S4 $4^{\text {ii }}$ | 2.6872 (6) | $\mathrm{Ba} 1-\mathrm{Er} 2{ }^{\mathrm{x}}$ | 3.9231 (3) |
| Er1—S3 ${ }^{\text {iii }}$ | 2.7164 (10) | $\mathrm{Ba} 1-\mathrm{Ba} 1^{\text {xi }}$ | 3.9884 (1) |
| Er1-S3 ${ }^{\text {iv }}$ | 2.7360 (7) | $\mathrm{Ba} 1-\mathrm{Ba} 1^{\text {xii }}$ | 3.9884 |
| Er1-S3 ${ }^{\text {}}$ | 2.7360 (7) | $\mathrm{S} 1-\mathrm{Er} 2{ }^{\text {iii }}$ | 2.6706 (10) |
| Er1-S2 | 2.7362 (11) | S1-Er2 ${ }^{\text {i }}$ | 2.7273 (7) |
| Er1-Ba1 | 4.2774 (3) | S1-Er2ii | 2.7273 (7) |
| Er2-S1 ${ }^{\text {vi }}$ | 2.6706 (10) | $\mathrm{S} 1-\mathrm{Ba} 1^{\text {ii }}$ | 3.1725 (8) |
| Er2-S1 ${ }^{\text {v }}$ | 2.7274 (7) | $\mathrm{S} 1-\mathrm{Ba} 1^{\text {i }}$ | 3.1725 (8) |
| Er2-S $1^{\text {iv }}$ | 2.7274 (7) | $\mathrm{S} 2-\mathrm{Er} 2^{\text {vii }}$ | 2.7376 (7) |


| Er2-S4 | 2.7345 (9) |
| :---: | :---: |
| Er2-S2 ${ }^{\text {vii }}$ | 2.7376 (7) |
| Er2-S2 ${ }^{\text {viii }}$ | 2.7376 (7) |
| Er2-Bal ${ }^{\text {ix }}$ | 3.9231 (3) |
| Er2-Ba1 | 4.0153 (3) |
| $\mathrm{Ba} 1-\mathrm{S} 3{ }^{\text {v }}$ | 3.1666 (8) |
| $\mathrm{Ba} 1-\mathrm{S3}{ }^{\text {iv }}$ | 3.1666 (8) |
| $\mathrm{Ba} 1-\mathrm{S} 1^{\text {iv }}$ | 3.1725 (8) |
| $\mathrm{Ba} 1-\mathrm{S} 1^{v}$ | 3.1725 (8) |
| $\mathrm{Ba} 1-\mathrm{S} 2{ }^{\text {iv }}$ | 3.2438 (9) |
| $\mathrm{Ba} 1-\mathrm{S} 2^{\text {v }}$ | 3.2438 (9) |
| Ba1-S4 ${ }^{\text {x }}$ | 3.3074 (11) |
| S4 ${ }^{\text {i }}$ - Er1—S $4^{\text {ii }}$ | 95.82 (3) |
| S4i-Er1-S3 ${ }^{\text {iii }}$ | 91.23 (3) |
| S4ii-Er1—S3 ${ }^{\text {iii }}$ | 91.23 (3) |
| S 4 - $\mathrm{Er} 1-\mathrm{S} 3{ }^{\text {iv }}$ | 176.07 (3) |
| S4ii-Errl-S3 ${ }^{\text {iv }}$ | 85.17 (2) |
| S3 ${ }^{\text {iii }}$ - $\mathrm{Er} 1-\mathrm{S} 3{ }^{\text {iv }}$ | 84.95 (3) |
| $\mathrm{S} 4^{\mathrm{i}}$ - $\mathrm{Er} 1-\mathrm{S} 3^{\text {v }}$ | 85.17 (2) |
| S4iil ${ }^{\text {ii }}$ Er $1-\mathrm{S} 3{ }^{\text {v }}$ | 176.07 (3) |
| S3 ${ }^{\text {iii- }}$ Er1-S3 ${ }^{\text {v }}$ | 84.95 (3) |
| S3 ${ }^{\text {iv }}-\mathrm{Er} 1-\mathrm{S} 3{ }^{\text {v }}$ | 93.58 (3) |
| S4i-Er1-S2 | 92.59 (3) |
| $\mathrm{S} 4{ }^{\text {ii }}$-Er1-S2 | 92.59 (3) |
| S3 ${ }^{\text {iii- }}$ - $\mathrm{Er} 1-\mathrm{S} 2$ | 174.30 (3) |
| S3 ${ }^{\text {iv }}$-Er1-S2 | 91.16 (3) |
| S3 ${ }^{\text {- }} \mathrm{Er} 1-\mathrm{S} 2$ | 91.16 (3) |
| S 4 - $\mathrm{Er} 1-\mathrm{Ba} 1$ | 131.894 (15) |
| S4ii-Er1-Ba1 | 131.894 (15) |
| S3iii-Er1-Bal | 93.15 (2) |
| S3 ${ }^{\text {iv }}$-Er $1-\mathrm{Ba} 1$ | 47.693 (15) |
| S3 ${ }^{\text {v }}$-Er1-Ba 1 | 47.693 (15) |
| S2-Er1-Bal | 81.15 (2) |
| $\mathrm{S} 1{ }^{\text {vi}}-\mathrm{Er} 2-\mathrm{S} 1^{v}$ | 83.18 (3) |
| S1 ${ }^{\text {vi}}-\mathrm{Er} 2-\mathrm{S} 1^{\mathrm{iv}}$ | 83.18 (3) |
| $\mathrm{S} 1{ }^{\mathrm{v}}$-Er2-S1 ${ }^{\text {iv }}$ | 93.97 (3) |
| S1 ${ }^{\text {vi}}$ - $\mathrm{Er} 2-\mathrm{S} 4$ | 160.92 (3) |
| S1 ${ }^{\text {v }}$-Er2-S4 | 83.84 (3) |
| $\mathrm{S} 1{ }^{\text {iv }}$ - $\mathrm{Er} 2-\mathrm{S} 4$ | 83.84 (3) |
| S1 ${ }^{\text {vi }}$-Er2- $\mathrm{S}^{\text {vii }}$ | 103.56 (3) |
| S1 ${ }^{v}$-Er2-S2 ${ }^{\text {vii }}$ | 173.17 (3) |
| $\mathrm{S} 1^{\text {iv }}$-Er2-S2 ${ }^{\text {vii }}$ | 85.85 (2) |
| S4-Er2—S2 ${ }^{\text {vii }}$ | 89.36 (3) |
| $\mathrm{S} 1^{\text {vi }}$-Er2-S2 ${ }^{\text {viii }}$ | 103.56 (3) |
| $\mathrm{S} 1^{\mathrm{v}}$-Er2—-S2 ${ }^{\text {viii }}$ | 85.85 (2) |
| $\mathrm{S} 1^{\text {iv }}-\mathrm{Er} 2-\mathrm{S} 2{ }^{\text {viii }}$ | 173.17 (3) |
| S4—Er2—S2 ${ }^{\text {viii }}$ | 89.36 (3) |


| S2—Er2 ${ }^{\text {viii }}$ | 2.7376 (7) |
| :---: | :---: |
| $\mathrm{S} 2-\mathrm{Ba} 1^{\mathrm{i}}$ | 3.2437 (9) |
| $\mathrm{S} 2-\mathrm{Ba} 1^{\text {ii }}$ | 3.2437 (9) |
| S3-Er1 ${ }^{\text {vi }}$ | 2.7163 (10) |
| S3-Er1 ${ }^{\text {i }}$ | 2.7360 (7) |
| S3-Er1 ${ }^{\text {ii }}$ | 2.7360 (7) |
| S3-Ba1i ${ }^{\text {ii }}$ | 3.1666 (8) |
| $\mathrm{S} 3-\mathrm{Ba} 1^{\text {i }}$ | 3.1666 (8) |
| $\mathrm{S} 4-\mathrm{Er} 1^{\text {iv }}$ | 2.6873 (6) |
| S4-Er1 ${ }^{\text {v }}$ | 2.6873 (6) |
| $\mathrm{S} 4-\mathrm{Ba} 1^{\mathrm{ix}}$ | 3.3074 (11) |

106.592 (19)
133.879 (16)
133.879 (16)
43.642 (15)
43.642 (15)
43.408 (16)
91.735 (18)
129.032 (11)
50.967 (11)
51.054 (12)
128.946 (12)
52.064 (12)
127.936 (12)
90.0
90.0
90.0
50.967 (11)
129.032 (11)
128.946 (12)
51.054 (12)
127.936 (12)
52.064 (12)
90.0
90.0
90.0
180.0
108.630 (19)
108.630 (19)
42.616 (14)
42.616 (14)
106.201 (19)
106.201 (19)
177.557 (18)
42.413 (17)
134.149 (8)

| S2 ${ }^{\text {vii- }}$ Er2—S $2^{\text {viii }}$ | 93.51 (3) |
| :---: | :---: |
| $\mathrm{S} 1{ }^{\text {vi }}$ - $\mathrm{Er} 2-\mathrm{Ba} 1^{\text {ix }}$ | 142.85 (2) |
| S1 ${ }^{\text {v }}$ - $\mathrm{Er} 2-\mathrm{Ba} 1^{\text {ix }}$ | 120.02 (2) |
| $\mathrm{S} 1{ }^{\text {iv }}-\mathrm{Er} 2-\mathrm{Ba} 1^{\text {ix }}$ | 120.02 (2) |
| S4-Er2-Ba1 ${ }^{\text {ix }}$ | 56.22 (2) |
| S2 ${ }^{\text {vii }}$-Er2——Ba1 ${ }^{\text {ix }}$ | 54.861 (19) |
| S2 ${ }^{\text {viii- }}$ - 2 2-Ba1 ${ }^{\text {ix }}$ | 54.861 (19) |
| S1 ${ }^{\text {vi- }} \mathrm{Er} 2-\mathrm{Ba} 1$ | 105.39 (2) |
| $\mathrm{S} 1{ }^{v}-\mathrm{Er} 2-\mathrm{Ba} 1$ | 51.961 (18) |
| S1 ${ }^{\text {iv }}$ - $\mathrm{Er} 2-\mathrm{Ba} 1$ | 51.961 (18) |
| S4-Er2-Ba1 | 55.53 (2) |
| $\mathrm{S} 2{ }^{\text {vii- }} \mathrm{Er} 2-\mathrm{Ba} 1$ | 123.95 (2) |
| S2 ${ }^{\text {viii- }} \mathrm{Er} 2-\mathrm{Ba} 1$ | 123.95 (2) |
| $\mathrm{Ba} 1^{\mathrm{ix}}$ - $\mathrm{Er} 2-\mathrm{Ba} 1$ | 111.755 (5) |
| S3 ${ }^{v}-\mathrm{Ba} 1-\mathrm{S} 3{ }^{\text {iv }}$ | 78.06 (2) |
| S3 ${ }^{v}-\mathrm{Ba} 1-\mathrm{Sl}^{\text {iv }}$ | 116.92 (2) |
| $\mathrm{S} 3{ }^{\text {iv }}-\mathrm{Ba} 1-\mathrm{S} 1^{\text {iv }}$ | 70.19 (2) |
| S3 ${ }^{v}-\mathrm{Ba} 1-\mathrm{S} 1^{v}$ | 70.19 (2) |
| $\mathrm{S} 3{ }^{\text {iv }}-\mathrm{Ba} 1-\mathrm{S} 1^{v}$ | 116.92 (2) |
| $\mathrm{S} 1^{\mathrm{iv}}-\mathrm{Ba} 1-\mathrm{S} 1^{v}$ | 77.89 (2) |
| S3 ${ }^{v}-\mathrm{Ba} 1-\mathrm{S} 2^{\text {iv }}$ | 145.12 (3) |
| $\mathrm{S} 3{ }^{\text {iv }}-\mathrm{Ba} 1-\mathrm{S} 2{ }^{\text {iv }}$ | 92.639 (19) |
| $\mathrm{S} 1^{\mathrm{iv}}$ - $\mathrm{Ba} 1-\mathrm{S} 2{ }^{\text {iv }}$ | 90.26 (2) |
| S12-Ba1-S2 ${ }^{\text {iv }}$ | 141.02 (3) |
| S3 ${ }^{v}-\mathrm{Ba} 1-\mathrm{S} 2{ }^{\text {v }}$ | 92.639 (19) |
| $\mathrm{S} 3^{\text {iv }}-\mathrm{Ba} 1-\mathrm{S} 2{ }^{\text {v }}$ | 145.12 (3) |
| S1 ${ }^{\text {iv }}-\mathrm{Ba} 1-\mathrm{S} 2{ }^{\text {v }}$ | 141.02 (3) |
| $\mathrm{S} 1^{v}-\mathrm{Ba} 1-\mathrm{S} 2{ }^{\text {v }}$ | 90.26 (2) |
| $\mathrm{S} 2{ }^{\text {iv }}-\mathrm{Ba} 1-\mathrm{S} 2{ }^{\text {v }}$ | 75.87 (2) |
| S3 ${ }^{v}-\mathrm{Ba} 1-\mathrm{S} 4^{\text {x }}$ | 73.20 (2) |
| $\mathrm{S} 3^{\text {iv }}-\mathrm{Ba} 1-\mathrm{S} 4^{\text {x }}$ | 73.20 (2) |
| $\mathrm{S} 1^{\mathrm{iv}}-\mathrm{Ba} 1-\mathrm{S} 4^{\mathrm{x}}$ | 138.242 (15) |
| S1 ${ }^{\text {v }}$ - $\mathrm{Ba} 1-\mathrm{S} 4^{\text {x }}$ | 138.242 (15) |
| $\mathrm{S} 2^{\text {iv }}-\mathrm{Ba} 1-\mathrm{S} 4^{\text {x }}$ | 71.93 (2) |
| $\mathrm{S} 2^{\mathrm{v}}-\mathrm{Ba} 1-\mathrm{S} 4^{\mathrm{x}}$ | 71.93 (2) |
| S3 ${ }^{\text {v }}-\mathrm{Ba} 1-\mathrm{S} 4$ | 135.514 (16) |
| S3 ${ }^{\text {iv }}-\mathrm{Ba} 1-\mathrm{S} 4$ | 135.514 (16) |
| $\mathrm{S} 1^{\mathrm{iv}}-\mathrm{Ba} 1-\mathrm{S} 4$ | 68.06 (2) |
| $\mathrm{S} 1^{v}-\mathrm{Ba} 1-\mathrm{S} 4$ | 68.06 (2) |
| S2 ${ }^{\text {iv }}-\mathrm{Ba} 1-\mathrm{S} 4$ | 73.05 (2) |
| $\mathrm{S} 2^{\mathrm{v}}-\mathrm{Ba} 1-\mathrm{S} 4$ | 73.05 (2) |
| S4 - $\mathrm{Ba} 1-\mathrm{S} 4$ | 135.144 (10) |
| $\mathrm{S} 3{ }^{\mathrm{v}}-\mathrm{Ba} 1-\mathrm{Er}^{2}$ | 106.592 (19) |


| $\mathrm{Ba} 1{ }^{\text {xi }}-\mathrm{Ba} 1-\mathrm{Er} 2$ | 90.0 |
| :---: | :---: |
| $\mathrm{Ba} 1^{\text {xii }}$ - $\mathrm{Ba} 1-\mathrm{Er} 2$ | 90.0 |
| $\mathrm{Er} 2{ }^{\text {iiii- }} \mathrm{S} 1-\mathrm{Er} 2^{\text {i }}$ | 96.82 (3) |
| $\mathrm{Er} 2{ }^{\text {iii- }}$-S1-Er2 ${ }^{\text {ii }}$ | 96.82 (3) |
| $\mathrm{Er} 2 \mathrm{C}-\mathrm{S} 1-\mathrm{Er} 2^{\text {ii }}$ | 93.97 (3) |
| Er2 ${ }^{\text {iii }}$ - $\mathrm{S} 1-\mathrm{Ba} 1^{\text {ii }}$ | 115.97 (3) |
| Er2 ${ }^{\text {i }}$ - $\mathrm{S}^{\text {- }}$ - $\mathrm{Ba}^{1{ }^{\text {ii }}}$ | 147.08 (4) |
| $\mathrm{Er} 2{ }^{\text {ii }}-\mathrm{S} 1-\mathrm{Ba} 1{ }^{\text {ii }}$ | 85.422 (12) |
| $\mathrm{Er} 2^{\text {iii- }}$ - $\mathrm{S} 1-\mathrm{Ba} 1^{\mathrm{i}}$ | 115.97 (3) |
| Er2i-S1-Ba1 ${ }^{\text {i }}$ | 85.422 (12) |
| $\mathrm{Er} 2{ }^{\mathrm{ii}}-\mathrm{S} 1-\mathrm{Ba} 1^{\text {i }}$ | 147.08 (4) |
| $\mathrm{Ba} 1{ }^{\mathrm{ii}}-\mathrm{S} 1-\mathrm{Ba} 1^{\mathrm{i}}$ | 77.89 (2) |
| Er1-S2-Er2 ${ }^{\text {vii }}$ | 120.17 (3) |
| Er1-S2-Er2 ${ }^{\text {viii }}$ | 120.17 (3) |
| $\mathrm{Er} 2{ }^{\text {vii }}$-S2-Er2 ${ }^{\text {viii }}$ | 93.51 (3) |
| $\mathrm{Er} 1-\mathrm{S} 2-\mathrm{Ba} 1^{\text {i }}$ | 97.16 (3) |
| $\mathrm{Er} 2^{\text {vii }}$-S2- $\mathrm{Ba}^{\text {i }}{ }^{\text {i }}$ | 138.40 (4) |
| Er2 ${ }^{\text {viii- }}$ S2- $\mathrm{Ba}^{\text {i }}$ | 81.498 (14) |
| Er1-S2-Ba1 ${ }^{\text {ii }}$ | 97.16 (3) |
| $\mathrm{Er} 2{ }^{\text {vii }}$-S2- $\mathrm{Ba}^{\text {ii }}$ | 81.498 (14) |
| Er2 ${ }^{\text {viii- }}$ S2-Ba1 ${ }^{\text {ii }}$ | 138.40 (4) |
| $\mathrm{Ba} 1{ }^{\mathrm{i}}-\mathrm{S} 2-\mathrm{Ba} 1^{\text {ii }}$ | 75.87 (2) |
| Er1 ${ }^{\text {vi}}-\mathrm{S} 3-\mathrm{Er} 1^{\text {i }}$ | 95.05 (3) |
| Er1 ${ }^{\text {vi}}-\mathrm{S} 3-E r 1{ }^{\text {ii }}$ | 95.05 (3) |
| Er1 ${ }^{\text {i }}$-S3-Er1 ${ }^{\text {ii }}$ | 93.58 (3) |
| Er1 ${ }^{\text {vi }}$ - $\mathrm{S} 3-\mathrm{Ba} 1^{\text {ii }}$ | 98.65 (3) |
| Er1 ${ }^{\text {i }}$-S3- $31{ }^{1 i}$ | 164.41 (4) |
| Er1 ${ }^{\text {iii- }}$ S3- 3 a $1^{\text {ii }}$ | 92.590 (8) |
| Er1 ${ }^{\text {vi}}$ - $\mathrm{S} 3-\mathrm{Ba} 1^{\mathrm{i}}$ | 98.65 (3) |
| Er1 ${ }^{\text {i }}$-S3- 3 al ${ }^{\text {i }}$ | 92.590 (8) |
| $\mathrm{Er} 1^{\mathrm{ii}}-\mathrm{S} 3-\mathrm{Ba} 1^{\mathrm{i}}$ | 164.41 (4) |
| $\mathrm{Ba} 1{ }^{\mathrm{ii}}$ - $\mathrm{S} 3-\mathrm{Ba} 1^{\mathrm{i}}$ | 78.07 (2) |
| $\mathrm{Er} 1^{\mathrm{iv}}$ - $\mathrm{S} 4-\mathrm{Er} 1^{\mathrm{v}}$ | 95.82 (3) |
| Er1 ${ }^{\text {iv }}$-S4-Er2 | 132.085 (15) |
| Er1 ${ }^{\text {v }}$-S4-Er2 | 132.085 (15) |
| $\mathrm{Er} 1^{\mathrm{iv}}$ - $\mathrm{S} 4-\mathrm{Ba} 1^{\text {ix }}$ | 95.91 (3) |
| Er1 ${ }^{\mathrm{v}}$-S4--Ba1 ${ }^{\text {ix }}$ | 95.91 (3) |
| Er2-S4-Ba $1^{\text {ix }}$ | 80.37 (3) |
| Er1 ${ }^{\text {iv }}$-S4-Bal | 95.84 (3) |
| $\mathrm{Er} 1^{\mathrm{v}}$ - $\mathrm{S} 4-\mathrm{Ba} 1$ | 95.84 (3) |
| Er2-S4-Ba1 | 82.05 (3) |
| $\mathrm{Ba} 1{ }^{\mathrm{ix}}-\mathrm{S} 4-\mathrm{Ba} 1$ | 162.42 (3) |

[^0]
[^0]:    Symmetry codes: (i) $-x+1 / 2,-y, z-1 / 2$; (ii) $-x+1 / 2,-y+1, z-1 / 2$; (iii) $x-1 / 2, y,-z+1 / 2$; (iv) $-x+1 / 2,-y+1, z+1 / 2$; (v) $-x+1 / 2,-y, z+1 / 2$; (vi) $x+1 / 2, y$, $-z+1 / 2$; (vii) $-x+1,-y+1,-z+1$; (viii) $-x+1,-y,-z+1$; (ix) $x+1 / 2, y,-z+3 / 2$; (x) $x-1 / 2, y,-z+3 / 2$; (xi) $x, y+1, z$; (xii) $x, y-1, z$.

