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# Dimethyl 2-[24-acetyl-28-oxo-8,11,14trioxa-24,27-diazapentacyclo-[19.5.1.1<sup>22,26</sup>.0<sup>2,7</sup>.0<sup>15,20</sup>]octacosa-2,4,6,15(20),16,18-hexaen-27-yl]but-2-enedioate

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Key indicators: single-crystal X-ray study; T = 100 K; mean  $\sigma$ (C–C) = 0.002 Å; R factor = 0.045; wR factor = 0.111; data-to-parameter ratio = 22.0.

The title compound,  $C_{31}H_{34}N_2O_9$ , is a product of the Michael addition of the cyclic secondary amine subunit of the (bispidino)aza-14-crown-4 ether to dimethyl acetylene-dicarboxylate. The molecule comprises a tricyclic system containing the aza-14-crown-3 ether macrocycle and two sixmembered piperidinone rings. The aza-14-crown-3-ether ring adopts a bowl conformation with a dihedral angle between the planes of the fused benzene rings of 51.14 (5)°. The central piperidone ring adopts a chair conformation. The dimethyl ethylenedicarboxylate fragment has a *cis* configuration with a dihedral angle of 56.56 (7)° between the two carboxylate groups. The crystal packing is stabilized by weak  $C-H \cdots O$  hydrogen bonds.

# **Related literature**

For general background, see: Hiraoka (1982); Pedersen (1988); Schwan & Warkentin (1988); Gokel & Murillo (1996); Bradshaw & Izatt (1997). For related compounds, see: Levov *et al.* (2006, 2008); Komarova *et al.* (2008); Anh *et al.* (2008); Anh, Hieu, Soldatenkov, Kolyadina & Khrustalev (2012*a,b*); Anh, Hieu, Soldatenkov, Soldatova & Khrustalev (2012); Hieu *et al.* (2011); Khieu *et al.* (2011); Sokol *et al.* (2011).



V = 2875.6 (3) Å<sup>3</sup>

Mo Ka radiation

 $0.30 \times 0.20 \times 0.20$  mm

36500 measured reflections

8396 independent reflections

6209 reflections with  $I > 2\sigma(I)$ 

 $\mu = 0.10 \text{ mm}^{-3}$ 

T = 100 K

 $R_{\rm int} = 0.045$ 

*Z* = 4

### **Experimental**

Crystal data  $C_{31}H_{34}N_2O_9$  $M_r = 578.60$ 

Monoclinic,  $P2_1/c$  a = 9.6634 (6) Å b = 26.3883 (18) Å c = 11.4375 (8) Å  $\beta = 99.614$  (1)°

# Data collection

Bruker APEXII CCD diffractometer Absorption correction: multi-scan (SADABS; Sheldrick, 2003)  $T_{min} = 0.971, T_{max} = 0.981$ 

Refinement

$R[F^2 > 2\sigma(F^2)] = 0.045 \qquad 382 \text{ parameters}$	
$wR(F^2) = 0.111$ H-atom parameters cons	strained
$S = 1.00 \qquad \qquad \Delta \rho_{\text{max}} = 0.40 \text{ e } \text{\AA}^{-3}$	
$\Delta \rho_{\rm min} = -0.26 \text{ e } \text{\AA}^{-3}$	

### Table 1

Hydrogen-bond geometry (Å, °).

$D - H \cdots A$	D-H	$H \cdot \cdot \cdot A$	$D \cdots A$	$D - \mathbf{H} \cdot \cdot \cdot A$
C18-H18···O35 <sup>i</sup>	0.95	2.47	3.1735 (17)	131
$C25-H25A\cdots O33^{ii}$	0.99	2.30	3.2091 (17)	152
C34–H34A···O35 <sup>iii</sup>	0.98	2.53	3.5045 (19)	174

Symmetry codes: (i)  $x, -y + \frac{1}{2}, z + \frac{1}{2}$ ; (ii) x - 1, y, z; (iii)  $x, -y + \frac{1}{2}, z - \frac{1}{2}$ .

Data collection: *APEX2* (Bruker, 2005); cell refinement: *SAINT* (Bruker, 2001); data reduction: *SAINT*; program(s) used to solve structure: *SHELXTL* (Sheldrick, 2008); program(s) used to refine structure: *SHELXTL*; molecular graphics: *SHELXTL*; software used to prepare material for publication: *SHELXTL*.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: RK2370).

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# supporting information

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Dimethyl 2-[24-acetyl-28-oxo-8,11,14-trioxa-24,27-diazapentacyclo-[19.5.1.1<sup>22,26</sup>.0<sup>2,7</sup>.0<sup>15,20</sup>]octacosa-2,4,6,15(20),16,18-hexaen-27-yl]but-2enedioate

# Truong Hong Hieu, Le Tuan Anh, Anatoly T. Soldatenkov, Nadezhda M. Kolyadina and Victor N. Khrustalev

# S1. Comment

Azacrown ethers draw very great attention of investigators over the last half century owing to their great potential for both theoretical and practical interest (Hiraoka, 1982; Pedersen, 1988; Gokel & Murillo, 1996; Bradshaw & Izatt, 1997). Recently we have designed one more effective route to reach this fascinating region of macroheterocyclic compounds, namely, the effective method of synthesis of azacrown ethers containing piperidine (Levov *et al.*, 2006, 2008; Anh *et al.*, 2008; Anh, Hieu, Soldatenkov, Kolyadina & Khrustalev, 2012*a*; Anh, Hieu, Soldatenkov, Soldatova & Khrustalev, 2012), perhydropyrimidine (Hieu *et al.*, 2011), perhydrotriazine (Khieu *et al.*, 2011) and bispidine (Komarova *et al.*, 2008; Sokol *et al.*, 2011; Anh, Hieu, Soldatenkov, Kolyadina & Khrustalev, 2012*b*) subunits.

In attempts to develop the chemistry for new azacrown systems and to obtain macrocyclic ligands bringing the desirable functional groups, we studied the Michael addition of the cyclic secondary amine subunit of the (bispidino)aza-14crown-4 ether to dimethyl acetylenedicarboxylate. The expected reaction is well known (Schwan & Warkentin, 1988), but might be highly hindered in the case of (bispidino)azacrown system due to the steric reasons. We have found that the expected *N*-vynilation reaction of the (bispidino)azacrown ether proceeded smoothly to give an *N*-maleinate derivative of the azacrown system with a good yield (Fig. 1).

The molecule of I,  $C_{31}H_{34}N_2O_9$ , comprises a tricyclic system containing the aza-14-crown-3-ether macrocycle and two six-membered piperidinone rings (Fig. 2). The aza-14-crown-3-ether ring adopts a bowl conformation. The configuration of the C7–O8–C9–C10–O11–C12–C13–O14–C15 polyether chain is t-g(-)-t-t-g(+)-t (t = trans, 180°; g = gauche,  $\pm 60°$ ). The dihedral angle between the planes of the benzene rings fused to the aza-14-crown-4-ether moiety is 51.14 (5)°. The central piperidone ring has a boat conformation, whereas the terminal piperidone ring adopts a chair conformation. The nitrogen N24 atom has a trigonal-planar geometry (sum of the bond angles is 360.0°), while the nitrogen N27 atom adopts a trigonal-pyramidal geometry (sum of the bond angles is 340.5°). The dimethyl ethylenedicarboxylate fragment has a *cis* configuration with a dihedral angle of 56.56 (7)° between the two carboxylate groups.

The molecule of **I** possesses four asymmetric centers at the C1, C21, C22 and C26 carbon atoms and can have potentially numerous diastereomers. The crystal of **I** is racemic and consists of enantiomeric pairs with the following relative configuration of the centers: rac-1R\*, 21S\*,22R\*,26S\*.

In the crystal, the molecules of I are bound by the weak intermolecular C–H…O hydrogen bonding interactions into three-dimensional framework (Table 1).

# **S2. Experimental**

Dimethylacetylenedicarboxylate (0.24 g, 1.69 mmol) was added to a solution of (bispidino)aza-14-crown-4ether (0.25 g, 0.57 mmol) in chloroform (20 ml). The reaction mixture was stirred at 293 K for one day (monitoring by *TLC* until disappearance of the starting organic compounds spots). At the end of the reaction, the formed precipitate was separated, washed with cold chloroform (15 ml) and re-crystallized from ethanol to give 0.32 g of colourless crystals of **I**. Yield is 98%. *M*.p. = 522-524 K. IR (KBr), *v*/cm<sup>-1</sup>: 1603, 1651, 1715. <sup>1</sup>H NMR (CDCl<sub>3</sub>, 400 MHz, 300 K):  $\delta$  = 2.33 (s, 3H, CH<sub>3</sub>C=O), 3.02 (m, 2H, H22 and H26), 3.28 and 3.43 (both s, 3H each, OCH<sub>3</sub>), 3.79-4.10 (m, 12H, OCH<sub>2</sub>CH<sub>2</sub>OCH<sub>2</sub>CH<sub>2</sub>O, 2H23 and 2H25), 4.4 and 4.56 (both d, 1H each, H1 and H21, *J* = 7.3), 6.56 (s, 1H, C=CHCOO), 6.70-6.78 (m, 4H, H<sub>arom</sub>), 7.05 (d, 2H, H3 and H19, *J* = 7.6), 7.21 (m, 2H, H<sub>arom</sub>). Anal. Calcd for C<sub>31</sub>H<sub>34</sub> N<sub>2</sub>O<sub>9</sub>: C, 64.35; H, 5.92; N, 4.84. Found: C, 64.41; H, 6.07; N, 4.67.

# **S3. Refinement**

The hydrogen atoms were placed in calculated positions with C–H = 0.95-1.00Å and refined in the riding model with fixed isotropic displacement parameters:  $U_{iso}(H) = 1.5U_{eq}(C)$  for the methyl group and  $1.2U_{eq}(C)$  for the other groups.



# Figure 1

Michael addition of bis(benzo)-(bispidino)aza-14-crown-4 ether to dimethyl acetylenedicarboxylate.



# Figure 2

Molecular structure of I with the atom numbering scheme. Displacement ellipsoids are shown at the 50% probability level. H atoms are presented as small spheres of arbitrary radius.

Dimethyl 2-(24-acetyl-28-oxo-8,11,14-trioxa-24,27- diazapentacyclo[19.5.1.1<sup>22,26</sup>.0<sup>2,7</sup>.0<sup>15,20</sup>]octacosa-2,4,6,15(20),16,18-hexaen-27-yl)but-2-enedioate

Crystal data

 $C_{31}H_{34}N_2O_9$   $M_r = 578.60$ Monoclinic,  $P2_1/c$ Hall symbol: -P 2ybc a = 9.6634 (6) Å b = 26.3883 (18) Å c = 11.4375 (8) Å  $\beta = 99.614$  (1)° V = 2875.6 (3) Å<sup>3</sup> Z = 4

## Data collection

Bruker APEXII CCD diffractometer Radiation source: fine-focus sealed tube Graphite monochromator  $\varphi$  and  $\omega$  scans F(000) = 1224  $D_x = 1.337 \text{ Mg m}^{-3}$ Melting point = 522–524 K Mo Ka radiation,  $\lambda = 0.71073 \text{ Å}$ Cell parameters from 6686 reflections  $\theta = 2.3-30.4^{\circ}$   $\mu = 0.10 \text{ mm}^{-1}$  T = 100 KPrism, light yellow  $0.30 \times 0.20 \times 0.20 \text{ mm}$ 

Absorption correction: multi-scan (*SADABS*; Sheldrick, 2003)  $T_{min} = 0.971$ ,  $T_{max} = 0.981$ 36500 measured reflections 8396 independent reflections 6209 reflections with  $I > 2\sigma(I)$ 

$R_{\rm int} = 0.045$	$k = -37 \rightarrow 36$
$\theta_{\rm max} = 30.0^{\circ},  \theta_{\rm min} = 1.5^{\circ}$	$l = -16 \rightarrow 16$
$h = -13 \rightarrow 13$	

# Refinement

Refinement on $F^2$	Secondary atom site location: difference Fourier
Least-squares matrix: full	map
$R[F^2 > 2\sigma(F^2)] = 0.045$	Hydrogen site location: inferred from
$wR(F^2) = 0.111$	neighbouring sites
S = 1.00	H-atom parameters constrained
8396 reflections	$w = 1/[\sigma^2(F_o^2) + (0.046P)^2 + 1.09P]$
382 parameters	where $P = (F_o^2 + 2F_c^2)/3$
0 restraints	$(\Delta/\sigma)_{\rm max} < 0.001$
Primary atom site location: structure-invariant	$\Delta \rho_{\rm max} = 0.40 \text{ e } \text{\AA}^{-3}$
direct methods	$\Delta \rho_{\rm min} = -0.26 \text{ e } \text{\AA}^{-3}$

# Special details

**Geometry**. All s.u.'s (except the s.u. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell s.u.'s are taken into account individually in the estimation of s.u.'s in distances, angles and torsion angles; correlations between s.u.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell s.u.'s is used for estimating s.u.'s involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*-factors based on ALL data will be even larger.

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$
C1	0.11569 (13)	0.11896 (5)	0.20020 (11)	0.0157 (2)
H1	0.0768	0.1525	0.2195	0.019*
C2	0.09245 (13)	0.11385 (5)	0.06665 (11)	0.0179 (3)
C3	0.02840 (14)	0.15322 (6)	-0.00310 (12)	0.0216 (3)
Н3	0.0081	0.1840	0.0335	0.026*
C4	-0.00658 (16)	0.14824 (6)	-0.12602 (13)	0.0276 (3)
H4	-0.0504	0.1754	-0.1727	0.033*
C5	0.02316 (16)	0.10347 (6)	-0.17898 (13)	0.0287 (3)
Н5	-0.0025	0.0996	-0.2624	0.034*
C6	0.08995 (15)	0.06399 (6)	-0.11215 (12)	0.0250 (3)
H6	0.1117	0.0336	-0.1497	0.030*
C7	0.12495 (14)	0.06917 (5)	0.01056 (12)	0.0200 (3)
O8	0.18727 (11)	0.03213 (4)	0.08372 (8)	0.0225 (2)
C9	0.24451 (16)	-0.01130 (6)	0.03346 (13)	0.0250 (3)
H9A	0.3061	-0.0007	-0.0232	0.030*
H9B	0.1685	-0.0329	-0.0088	0.030*
C10	0.32707 (16)	-0.03936 (5)	0.13614 (13)	0.0250 (3)
H10A	0.2677	-0.0460	0.1972	0.030*
H10B	0.3595	-0.0723	0.1092	0.030*
O11	0.44422 (10)	-0.00887 (4)	0.18432 (8)	0.0223 (2)
C12	0.50802 (16)	-0.02495 (5)	0.29917 (13)	0.0250 (3)
H12A	0.5739	-0.0531	0.2926	0.030*

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(\hat{A}^2)$ 

H12B	0.4353	-0.0373	0.3438	0.030*
C13	0.58570 (15)	0.01879 (5)	0.36341 (13)	0.0220 (3)
H13A	0.6447	0.0070	0.4376	0.026*
H13B	0.6472	0.0350	0.3131	0.026*
014	0.48284 (9)	0.05405 (3)	0.38952 (8)	0.01810 (19)
C15	0.52964 (13)	0.09761 (5)	0.44734 (11)	0.0154 (2)
C16	0.66552 (13)	0.10392 (5)	0.50956 (11)	0.0175(3)
H16	0.7331	0.0778	0.5094	0.021*
C17	0.70186 (14)	0.14851 (5)	0.57176 (12)	0.0202(3)
H17	0.7942	0.1525	0.6148	0.024*
C18	0.60535(14)	0 18708 (5)	0.57162(12)	0.0202(3)
H18	0.6306	0.2175	0.6143	0.0202 (3)
C19	0.0300 0.47031(14)	0.18075(5)	0.50794 (11)	0.021
H19	0.4042	0.2075	0.5071	0.022*
C20	0.42963(13)	0.13655 (5)	0.44570(11)	0.022 0.0147 (2)
C21	0.12903(13) 0.27882(13)	0.13019(5)	0.38529(11)	0.0144(2)
H21	0.2286	0.1629	0.3921	0.017*
C22	0.2230	$0.102^{\circ}$ 0.08817 (5)	0.3921 0.44644(11)	0.017 0.0158 (2)
U22 H22	0.20353 (15)	0.0704	0.5076	0.0198 (2)
C23	0.2720	0.11077 (5)	0.50463 (11)	0.019
H23A	0.0399	0.0836	0.5455	0.023*
H23R	0.1229	0.1364	0.5644	0.023*
N24	-0.02109(11)	0.13426 (5)	0.41473 (10)	0.023
C25	-0.08063(13)	0.10019 (6)	0.31856(12)	0.0192(2) 0.0207(3)
U25 H25A	-0.1472	0.10019 (0)	0.2501	0.0207 (3)
H25R	-0.1331	0.0727	0.2591	0.025
C26	0.1331 0.03642 (13)	0.0727	0.3500	0.025
U20	-0.0050	0.07711(5)	0.23840 (11)	0.0108(2) 0.020*
N27	0.0050	0.0320 0.11722(4)	0.1370	$0.020^{\circ}$
N27 C28	0.20343(11) 0.12448(12)	0.11722(4) 0.05052(5)	0.25731(9) 0.25580(11)	0.0140(2) 0.0172(3)
028	0.13440(13) 0.14211(11)	0.03032(3)	0.33369(11) 0.26862(0)	0.0175(3)
028 C20	0.14211(11)	0.00491(4)	0.30802(9)	0.0240(2)
029	-0.03451(14)	0.18412(6)	0.42329 (13)	0.0233(3)
029 C20	0.00129(12)	0.21020(4)	0.50702(10)	0.0323(3)
	-0.10320 (10)	0.20626 (6)	0.32078 (15)	0.0304 (3)
HOUA	-0.1//6	0.2421	0.3437	0.046*
H30B	-0.2519	0.1879	0.3236	0.046*
H30C	-0.1309	0.2032	0.2503	0.046*
C31	0.36237(13)	0.14313 (5)	0.19/59(11)	0.0149(2)
C32	0.44149 (13)	0.11639 (5)	0.13532 (11)	0.0162 (2)
H32	0.4245	0.0809	0.1296	0.019*
C33	0.55331 (14)	0.13640 (5)	0.07407 (11)	0.0170 (2)
033	0.67355 (10)	0.12234 (4)	0.09900 (9)	0.0259 (2)
034	0.50805 (10)	0.16863 (4)	-0.01385 (9)	0.0238 (2)
C34	0.61758 (16)	0.18984 (6)	-0.07172 (14)	0.0277 (3)
H34A	0.5771	0.2155	-0.1293	0.042*
H34B	0.6600	0.1628	-0.1127	0.042*
H34C	0.6896	0.2055	-0.0122	0.042*
C35	0.37909 (14)	0.19960 (5)	0.21065 (11)	0.0172 (2)

# supporting information

O35	0.48639 (11)	0.22224 (4)	0.20779 (10)	0.0258 (2)	
O36	0.25872 (10)	0.22096 (4)	0.22817 (9)	0.0209 (2)	
C36	0.25952 (17)	0.27511 (5)	0.24882 (14)	0.0266 (3)	
H36A	0.1657	0.2889	0.2206	0.040*	
H36B	0.3274	0.2913	0.2059	0.040*	
H36C	0.2859	0.2818	0.3339	0.040*	

Atomic displacement parameters  $(Å^2)$ 

	$U^{11}$	$U^{22}$	$U^{33}$	$U^{12}$	$U^{13}$	$U^{23}$
C1	0.0137 (6)	0.0194 (6)	0.0137 (6)	-0.0016 (5)	0.0010 (4)	-0.0006 (5)
C2	0.0145 (6)	0.0247 (7)	0.0141 (6)	-0.0040 (5)	0.0011 (4)	-0.0005 (5)
C3	0.0203 (6)	0.0263 (7)	0.0179 (6)	-0.0004(5)	0.0025 (5)	0.0014 (5)
C4	0.0263 (7)	0.0376 (9)	0.0184 (7)	0.0024 (6)	0.0023 (6)	0.0072 (6)
C5	0.0285 (7)	0.0429 (9)	0.0142 (6)	-0.0008 (7)	0.0026 (5)	0.0000 (6)
C6	0.0265 (7)	0.0325 (8)	0.0160 (6)	-0.0032 (6)	0.0039 (5)	-0.0050 (6)
C7	0.0178 (6)	0.0250 (7)	0.0171 (6)	-0.0034 (5)	0.0023 (5)	-0.0011 (5)
08	0.0290 (5)	0.0207 (5)	0.0175 (5)	0.0017 (4)	0.0031 (4)	-0.0036 (4)
С9	0.0301 (7)	0.0218 (7)	0.0223 (7)	-0.0007 (6)	0.0019 (6)	-0.0092 (6)
C10	0.0309 (7)	0.0165 (7)	0.0270 (7)	-0.0033 (6)	0.0027 (6)	-0.0063 (5)
O11	0.0263 (5)	0.0194 (5)	0.0201 (5)	-0.0024 (4)	0.0011 (4)	-0.0001 (4)
C12	0.0335 (8)	0.0162 (7)	0.0237 (7)	0.0036 (6)	-0.0001 (6)	-0.0005 (5)
C13	0.0219 (6)	0.0188 (7)	0.0245 (7)	0.0055 (5)	0.0012 (5)	-0.0030 (5)
O14	0.0171 (4)	0.0143 (4)	0.0229 (5)	-0.0004 (3)	0.0035 (4)	-0.0024 (4)
C15	0.0180 (6)	0.0154 (6)	0.0132 (6)	-0.0016 (5)	0.0039 (5)	0.0008 (5)
C16	0.0163 (6)	0.0194 (6)	0.0171 (6)	0.0021 (5)	0.0037 (5)	0.0020 (5)
C17	0.0158 (6)	0.0269 (7)	0.0168 (6)	-0.0025 (5)	-0.0003 (5)	-0.0002 (5)
C18	0.0215 (6)	0.0210 (7)	0.0172 (6)	-0.0032 (5)	0.0006 (5)	-0.0045 (5)
C19	0.0204 (6)	0.0176 (6)	0.0166 (6)	0.0010 (5)	0.0029 (5)	-0.0008 (5)
C20	0.0157 (6)	0.0165 (6)	0.0117 (5)	-0.0003 (5)	0.0020 (4)	0.0018 (5)
C21	0.0145 (5)	0.0168 (6)	0.0116 (5)	-0.0002 (4)	0.0015 (4)	-0.0003 (4)
C22	0.0156 (6)	0.0185 (6)	0.0135 (6)	-0.0008 (5)	0.0032 (4)	0.0010 (5)
C23	0.0178 (6)	0.0250 (7)	0.0148 (6)	-0.0015 (5)	0.0041 (5)	-0.0014 (5)
N24	0.0140 (5)	0.0260 (6)	0.0178 (5)	-0.0004 (4)	0.0031 (4)	-0.0040 (5)
C25	0.0143 (6)	0.0285 (7)	0.0195 (6)	-0.0041 (5)	0.0034 (5)	-0.0038 (5)
C26	0.0158 (6)	0.0196 (6)	0.0150 (6)	-0.0041 (5)	0.0028 (5)	-0.0025 (5)
N27	0.0133 (5)	0.0186 (5)	0.0119 (5)	-0.0020 (4)	0.0018 (4)	-0.0004 (4)
C28	0.0166 (6)	0.0202 (6)	0.0165 (6)	-0.0022 (5)	0.0070 (5)	0.0002 (5)
O28	0.0298 (5)	0.0182 (5)	0.0266 (5)	-0.0019 (4)	0.0068 (4)	0.0005 (4)
C29	0.0180 (6)	0.0265 (7)	0.0263 (7)	-0.0004 (5)	0.0067 (5)	-0.0024 (6)
O29	0.0315 (6)	0.0279 (6)	0.0356 (6)	-0.0008 (5)	0.0003 (5)	-0.0092 (5)
C30	0.0249 (7)	0.0306 (8)	0.0349 (8)	0.0064 (6)	0.0029 (6)	-0.0010 (7)
C31	0.0155 (6)	0.0165 (6)	0.0121 (5)	-0.0008 (5)	0.0006 (4)	0.0014 (4)
C32	0.0166 (6)	0.0171 (6)	0.0147 (6)	0.0005 (5)	0.0016 (5)	0.0000 (5)
C33	0.0192 (6)	0.0182 (6)	0.0137 (6)	0.0004 (5)	0.0034 (5)	-0.0027 (5)
O33	0.0178 (5)	0.0355 (6)	0.0245 (5)	0.0042 (4)	0.0042 (4)	0.0056 (4)
O34	0.0209 (5)	0.0289 (5)	0.0231 (5)	0.0031 (4)	0.0082 (4)	0.0099 (4)
C34	0.0299 (8)	0.0269 (8)	0.0300 (8)	0.0000 (6)	0.0156 (6)	0.0087 (6)

# supporting information

C35	0.0192 (6)	0.0186 (6)	0.0137 (6)	0.0010 (5)	0.0028 (5)	0.0007 (5)
O35	0.0238 (5)	0.0200 (5)	0.0355 (6)	-0.0045 (4)	0.0105 (4)	-0.0014 (4)
O36	0.0199 (5)	0.0163 (5)	0.0266 (5)	0.0025 (4)	0.0044 (4)	-0.0001 (4)
C36	0.0338 (8)	0.0174 (7)	0.0292 (8)	0.0052 (6)	0.0069 (6)	-0.0006 (6)

Geometric parameters (Å, °)

C1—N27	1.4862 (16)	C20—C21	1.5143 (17)
C1—C2	1.5124 (17)	C21—N27	1.4854 (16)
C1-C26	1.5560 (18)	C21—C22	1.5548 (17)
C1—H1	1.0000	C21—H21	1.0000
C2—C3	1.3907 (19)	C22—C28	1.5081 (18)
C2—C7	1.4025 (19)	C22—C23	1.5456 (18)
C3—C4	1.3962 (19)	C22—H22	1.0000
С3—Н3	0.9500	C23—N24	1.4576 (17)
C4—C5	1.380 (2)	C23—H23A	0.9900
C4—H4	0.9500	C23—H23B	0.9900
C5—C6	1.386 (2)	N24—C29	1.3623 (19)
С5—Н5	0.9500	N24—C25	1.4621 (17)
С6—С7	1.3944 (19)	C25—C26	1.5435 (18)
С6—Н6	0.9500	C25—H25A	0.9900
С7—О8	1.3603 (17)	C25—H25B	0.9900
O8—C9	1.4338 (17)	C26—C28	1.5097 (18)
C9—C10	1.500 (2)	C26—H26	1.0000
С9—Н9А	0.9900	N27—C31	1.4245 (16)
С9—Н9В	0.9900	C28—O28	1.2130 (16)
C10—O11	1.4228 (17)	C29—O29	1.2283 (18)
C10—H10A	0.9900	C29—C30	1.509 (2)
C10—H10B	0.9900	C30—H30A	0.9800
O11—C12	1.4196 (17)	C30—H30B	0.9800
C12—C13	1.500 (2)	C30—H30C	0.9800
C12—H12A	0.9900	C31—C32	1.3311 (18)
C12—H12B	0.9900	C31—C35	1.5036 (18)
C13—O14	1.4292 (16)	C32—C33	1.4799 (18)
C13—H13A	0.9900	C32—H32	0.9500
C13—H13B	0.9900	C33—O33	1.2076 (16)
O14—C15	1.3650 (15)	C33—O34	1.3337 (16)
C15—C16	1.3950 (18)	O34—C34	1.4512 (16)
C15—C20	1.4086 (18)	C34—H34A	0.9800
C16—C17	1.3894 (19)	C34—H34B	0.9800
C16—H16	0.9500	C34—H34C	0.9800
C17—C18	1.3804 (19)	C35—O35	1.2019 (16)
С17—Н17	0.9500	C35—O36	1.3373 (16)
C18—C19	1.3942 (18)	O36—C36	1.4481 (17)
C18—H18	0.9500	С36—Н36А	0.9800
C19—C20	1.3885 (18)	C36—H36B	0.9800
C19—H19	0.9500	C36—H36C	0.9800

N27—C1—C2	114.34 (10)	N27—C21—H21	108.1
N27—C1—C26	107.57 (10)	C20—C21—H21	108.1
C2—C1—C26	111.62 (10)	C22—C21—H21	108.1
N27—C1—H1	107.7	C28—C22—C23	105.85 (10)
C2—C1—H1	107.7	C28—C22—C21	110.33 (10)
$C_{26} - C_{1} - H_{1}$	107.7	$C_{23}$ $C_{22}$ $C_{21}$	110.96 (11)
$C_{3}-C_{2}-C_{7}$	118 54 (12)	C28—C22—H22	109.9
$C_{3}$ $-C_{2}$ $-C_{1}$	119 31 (12)	$C^{23}$ $C^{22}$ $H^{22}$	109.9
C7-C2-C1	122 01 (12)	$C_{21}$ $C_{22}$ $H_{22}$	109.9
$C_{2} - C_{3} - C_{4}$	122.01(12) 121.13(14)	N24-C23-C22	110.07(10)
C2C3H3	110.4	N24_C23_H23A	109.6
$C_{4}$ $C_{3}$ $H_{3}$	110.4	$C_{22}$ $C_{23}$ $H_{23}$ $H_{23}$	109.6
$C_{4} = C_{3} = 113$	119.7	N24 C23 H23R	109.0
$C_5 = C_4 = C_5$	119.31 (14)	1124 - C23 - 1123B	109.0
$C_3 = C_4 = 114$	120.3	122 - 123 - 1123 D	109.0
$C_3 = C_4 = H_4$	120.5	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	108.2
C4 - C5 - C6	120.89 (15)	$C_{29} = N_{24} = C_{23}$	120.37(11)
C4—C5—H5	119.6	$C_{29} = N_{24} = C_{25}$	125.43 (12)
C6—C5—H5	119.6	C23—N24—C25	114.19 (11)
C5-C6-C7	119.59 (14)	N24—C25—C26	110.62 (10)
С5—С6—Н6	120.2	N24—C25—H25A	109.5
С7—С6—Н6	120.2	C26—C25—H25A	109.5
O8—C7—C6	123.83 (13)	N24—C25—H25B	109.5
O8—C7—C2	115.64 (11)	С26—С25—Н25В	109.5
C6—C7—C2	120.50 (13)	H25A—C25—H25B	108.1
С7—О8—С9	119.25 (11)	C28—C26—C25	105.72 (10)
O8—C9—C10	105.72 (11)	C28—C26—C1	110.66 (10)
O8—C9—H9A	110.6	C25—C26—C1	111.13 (11)
С10—С9—Н9А	110.6	C28—C26—H26	109.8
O8—C9—H9B	110.6	C25—C26—H26	109.8
С10—С9—Н9В	110.6	C1—C26—H26	109.8
Н9А—С9—Н9В	108.7	C31—N27—C21	113.99 (10)
O11—C10—C9	107.99 (12)	C31—N27—C1	116.30 (10)
O11—C10—H10A	110.1	C21—N27—C1	110.20 (9)
C9—C10—H10A	110.1	O28—C28—C22	124.07 (12)
O11—C10—H10B	110.1	O28—C28—C26	124.59 (12)
C9—C10—H10B	110.1	$C_{22} - C_{28} - C_{26}$	110.61 (11)
H10A—C10—H10B	108.4	029 - 029 - 020	121.24(13)
$C_{12} = 011 = C_{10}$	112 57 (11)	029 - 029 - 030	120.99(14)
011 - C12 - C13	109 13 (12)	N24-C29-C30	117 76 (13)
011 - C12 - H12A	109.13 (12)	$C_{29}$ $C_{30}$ $H_{30A}$	109 5
$C_{12}$ $C_{12}$ $H_{12A}$	100.0	$C_{29}$ $C_{30}$ $H_{30R}$	109.5
011 C12 H12R	109.9	$H_{30A} = C_{30} = H_{30B}$	109.5
$C_{12}$ $C_{12}$ $H_{12}$ $H_{12}$	109.9	$C_{20}$ $C_{30}$ $H_{30C}$	109.5
$\begin{array}{c} 13 \\ 13 \\ 12 \\ 11$	109.9	$\begin{array}{c} 123 \\$	109.5
$\Pi 12A - C 12 - \Pi 12D$	100.3	$H_{20} P = C_{20} = H_{20} C$	107.3
014 - 013 - 012	107.14 (11)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	109.3
$C_{12} = C_{12} = U_{12} A$	110.5	$C_{22} = C_{21} = C_{25}$	119.03(12)
$C12 \rightarrow C13 \rightarrow H13A$	110.3	132 - 131 - 133	121.12 (12)
U14-U13-H13B	110.5	INZ/	119./3(11)

C12—C13—H13B	110.3	C31—C32—C33	126.45 (12)
H13A—C13—H13B	108.5	С31—С32—Н32	116.8
C15—O14—C13	117.64 (10)	С33—С32—Н32	116.8
O14—C15—C16	123.71 (12)	O33—C33—O34	123.74 (12)
O14—C15—C20	115.90 (11)	O33—C33—C32	121.90 (12)
C16—C15—C20	120.33 (12)	O34—C33—C32	114.26 (11)
C17—C16—C15	119.87 (12)	C33—O34—C34	114.68 (11)
C17—C16—H16	120.1	O34—C34—H34A	109.5
C15—C16—H16	120.1	O34—C34—H34B	109.5
C18—C17—C16	120.73 (12)	H34A—C34—H34B	109.5
C18—C17—H17	119.6	O34—C34—H34C	109.5
С16—С17—Н17	119.6	H34A—C34—H34C	109.5
C17—C18—C19	119.04 (12)	H34B—C34—H34C	109.5
C17—C18—H18	120.5	O35—C35—O36	124.79 (12)
C19—C18—H18	120.5	O35—C35—C31	124.67 (12)
C20-C19-C18	121.91 (12)	O36—C35—C31	110.53 (11)
С20—С19—Н19	119.0	C35—O36—C36	117.33 (11)
C18—C19—H19	119.0	O36—C36—H36A	109.5
C19—C20—C15	118.10 (11)	O36—C36—H36B	109.5
C19—C20—C21	119.71 (11)	H36A—C36—H36B	109.5
C15—C20—C21	122.07 (11)	O36—C36—H36C	109.5
N27—C21—C20	113.17 (10)	H36A—C36—H36C	109.5
N27—C21—C22	107.93 (10)	H36B—C36—H36C	109.5
C20—C21—C22	111.15 (10)		
N27—C1—C2—C3	-118.70 (13)	C22—C23—N24—C29	-122.32 (13)
C26—C1—C2—C3	118.90 (13)	C22—C23—N24—C25	56.46 (14)
N27—C1—C2—C7	65.64 (16)	C29—N24—C25—C26	122.45 (14)
C26—C1—C2—C7	-56.75 (16)	C23—N24—C25—C26	-56.26 (15)
C7 $C2$ $C2$ $C4$			
$C/-C_2-C_3-C_4$	1.7 (2)	N24—C25—C26—C28	57.46 (14)
$C_{1} = C_{2} = C_{3} = C_{4}$ $C_{1} = C_{2} = C_{3} = C_{4}$	1.7 (2) -174.11 (12)	N24—C25—C26—C28 N24—C25—C26—C1	57.46 (14) -62.65 (14)
C1C2C3C4 C1C2C3C4 C2C3C4C5	1.7 (2) -174.11 (12) -0.1 (2)	N24—C25—C26—C28 N24—C25—C26—C1 N27—C1—C26—C28	57.46 (14) -62.65 (14) 2.43 (14)
C1C2C3C4 C1C2C3C4 C2C3C4C5 C3C4C5C6	1.7 (2) -174.11 (12) -0.1 (2) -1.5 (2)	N24—C25—C26—C28 N24—C25—C26—C1 N27—C1—C26—C28 C2—C1—C26—C28	57.46 (14) -62.65 (14) 2.43 (14) 128.63 (11)
$C_{1} = C_{2} = C_{3} = C_{4}$ $C_{1} = C_{2} = C_{3} = C_{4}$ $C_{2} = C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5} = C_{6}$ $C_{4} = C_{5} = C_{6} = C_{7}$	1.7 (2) -174.11 (12) -0.1 (2) -1.5 (2) 1.3 (2)	N24—C25—C26—C28 N24—C25—C26—C1 N27—C1—C26—C28 C2—C1—C26—C28 N27—C1—C26—C25	57.46 (14) -62.65 (14) 2.43 (14) 128.63 (11) 119.57 (11)
$\begin{array}{c} C_{1} = C_{2} = C_{3} = C_{4} \\ C_{1} = C_{2} = C_{3} = C_{4} \\ C_{2} = C_{3} = C_{4} = C_{5} \\ C_{3} = C_{4} = C_{5} = C_{6} \\ C_{4} = C_{5} = C_{6} = C_{7} \\ C_{5} = C_{6} = C_{7} = C_{8} \end{array}$	1.7 (2) -174.11 (12) -0.1 (2) -1.5 (2) 1.3 (2) 178.27 (13)	N24—C25—C26—C28 N24—C25—C26—C1 N27—C1—C26—C28 C2—C1—C26—C28 N27—C1—C26—C25 C2—C1—C26—C25	57.46 (14) -62.65 (14) 2.43 (14) 128.63 (11) 119.57 (11) -114.23 (12)
$C_{1} = C_{2} = C_{3} = C_{4}$ $C_{1} = C_{2} = C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5} = C_{6}$ $C_{4} = C_{5} = C_{6} = C_{7} = C_{6}$ $C_{5} = C_{6} = C_{7} = C_{2}$	1.7 (2) -174.11 (12) -0.1 (2) -1.5 (2) 1.3 (2) 178.27 (13) 0.3 (2)	N24—C25—C26—C28 N24—C25—C26—C1 N27—C1—C26—C28 C2—C1—C26—C28 N27—C1—C26—C25 C2—C1—C26—C25 C20—C21—N27—C31	57.46 (14) -62.65 (14) 2.43 (14) 128.63 (11) 119.57 (11) -114.23 (12) -38.88 (14)
$C_{1} = C_{2} = C_{3} = C_{4}$ $C_{1} = C_{2} = C_{3} = C_{4}$ $C_{2} = C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5} = C_{6}$ $C_{4} = C_{5} = C_{6} = C_{7}$ $C_{5} = C_{6} = C_{7} = C_{2}$ $C_{3} = C_{2} = C_{7} = C_{8}$	1.7 (2) -174.11 (12) -0.1 (2) -1.5 (2) 1.3 (2) 178.27 (13) 0.3 (2) -179.92 (12)	N24—C25—C26—C28 N24—C25—C26—C1 N27—C1—C26—C28 C2—C1—C26—C28 N27—C1—C26—C25 C2—C1—C26—C25 C20—C21—N27—C31 C22—C21—N27—C31	57.46 (14) -62.65 (14) 2.43 (14) 128.63 (11) 119.57 (11) -114.23 (12) -38.88 (14) -162.31 (10)
$C_{1} = C_{2} = C_{3} = C_{4}$ $C_{1} = C_{2} = C_{3} = C_{4}$ $C_{2} = C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5} = C_{6}$ $C_{4} = C_{5} = C_{6} = C_{7}$ $C_{5} = C_{6} = C_{7} = C_{8}$ $C_{5} = C_{6} = C_{7} = C_{8}$ $C_{3} = C_{2} = C_{7} = C_{8}$ $C_{1} = C_{2} = C_{7} = C_{8}$	1.7 (2) -174.11 (12) -0.1 (2) -1.5 (2) 1.3 (2) 178.27 (13) 0.3 (2) -179.92 (12) -4.24 (18)	N24—C25—C26—C28 N24—C25—C26—C1 N27—C1—C26—C28 C2—C1—C26—C28 N27—C1—C26—C25 C2—C1—C26—C25 C20—C21—N27—C31 C22—C21—N27—C31 C20—C21—N27—C1	57.46 (14) -62.65 (14) 2.43 (14) 128.63 (11) 119.57 (11) -114.23 (12) -38.88 (14) -162.31 (10) -171.75 (10)
$C_{1} = C_{2} = C_{3} = C_{4}$ $C_{1} = C_{2} = C_{3} = C_{4}$ $C_{2} = C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5} = C_{6}$ $C_{4} = C_{5} = C_{6} = C_{7}$ $C_{5} = C_{6} = C_{7} = C_{8}$ $C_{5} = C_{6} = C_{7} = C_{8}$ $C_{3} = C_{2} = C_{7} = C_{8}$ $C_{3} = C_{2} = C_{7} = C_{6}$	1.7 (2) -174.11 (12) -0.1 (2) -1.5 (2) 1.3 (2) 178.27 (13) 0.3 (2) -179.92 (12) -4.24 (18) -1.8 (2)	N24—C25—C26—C28 N24—C25—C26—C1 N27—C1—C26—C28 C2—C1—C26—C28 N27—C1—C26—C25 C2—C1—C26—C25 C20—C21—N27—C31 C22—C21—N27—C31 C20—C21—N27—C1 C22—C21—N27—C1	57.46 (14) -62.65 (14) 2.43 (14) 128.63 (11) 119.57 (11) -114.23 (12) -38.88 (14) -162.31 (10) -171.75 (10) 64.81 (12)
$C_{1} = C_{2} = C_{3} = C_{4}$ $C_{1} = C_{2} = C_{3} = C_{4}$ $C_{2} = C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5} = C_{6}$ $C_{4} = C_{5} = C_{6} = C_{7}$ $C_{5} = C_{6} = C_{7} = C_{8}$ $C_{5} = C_{6} = C_{7} = C_{8}$ $C_{3} = C_{2} = C_{7} = C_{8}$ $C_{3} = C_{2} = C_{7} = C_{6}$ $C_{1} = C_{2} = C_{7} = C_{6}$	1.7 (2) -174.11 (12) -0.1 (2) -1.5 (2) 1.3 (2) 178.27 (13) 0.3 (2) -179.92 (12) -4.24 (18) -1.8 (2) 173.87 (12)	N24—C25—C26—C28 N24—C25—C26—C1 N27—C1—C26—C28 C2—C1—C26—C28 N27—C1—C26—C25 C2—C1—C26—C25 C20—C21—N27—C31 C22—C21—N27—C31 C20—C21—N27—C1 C22—C21—N27—C1 C2—C1—N27—C31	57.46(14) - $62.65(14)$ 2.43(14) 128.63(11) 119.57(11) - $114.23(12)$ - $38.88(14)$ - $162.31(10)$ - $171.75(10)$ 64.81(12) 39.86(16)
$C_{1} = C_{2} = C_{3} = C_{4}$ $C_{1} = C_{2} = C_{3} = C_{4}$ $C_{2} = C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5} = C_{6}$ $C_{4} = C_{5} = C_{6} = C_{7}$ $C_{5} = C_{6} = C_{7} = C_{8}$ $C_{5} = C_{6} = C_{7} = C_{8}$ $C_{3} = C_{2} = C_{7} = C_{8}$ $C_{3} = C_{2} = C_{7} = C_{6}$ $C_{1} = C_{2} = C_{7} = C_{6}$ $C_{6} = C_{7} = C_{9}$	1.7 (2) -174.11 (12) -0.1 (2) -1.5 (2) 1.3 (2) 178.27 (13) 0.3 (2) -179.92 (12) -4.24 (18) -1.8 (2) 173.87 (12) 12.0 (2)	$\begin{array}{c} N24 - C25 - C26 - C28 \\ N24 - C25 - C26 - C1 \\ N27 - C1 - C26 - C28 \\ C2 - C1 - C26 - C28 \\ N27 - C1 - C26 - C25 \\ C2 - C1 - C26 - C25 \\ C20 - C21 - N27 - C31 \\ C22 - C21 - N27 - C31 \\ C20 - C21 - N27 - C1 \\ C22 - C21 - N27 - C1 \\ C22 - C1 - N27 - C31 \\ C26 - C1 - N27 - C31 \\ \end{array}$	57.46(14) - $62.65(14)$ 2.43(14) 128.63(11) 119.57(11) - $114.23(12)$ - $38.88(14)$ - $162.31(10)$ - $171.75(10)$ 64.81(12) 39.86(16) 164.43(10)
$C_{1}-C_{2}-C_{3}-C_{4}$ $C_{2}-C_{3}-C_{4}-C_{5}$ $C_{3}-C_{4}-C_{5}-C_{6}$ $C_{4}-C_{5}-C_{6}-C_{7}$ $C_{5}-C_{6}-C_{7}-C_{2}$ $C_{3}-C_{2}-C_{7}-C_{8}$ $C_{1}-C_{2}-C_{7}-C_{8}$ $C_{3}-C_{2}-C_{7}-C_{6}$ $C_{1}-C_{2}-C_{7}-C_{6}$ $C_{1}-C_{2}-C_{7}-C_{6}$ $C_{6}-C_{7}-C_{8}-C_{9}$ $C_{2}-C_{7}-C_{8}-C_{9}$	1.7 (2) -174.11 (12) -0.1 (2) -1.5 (2) 1.3 (2) 178.27 (13) 0.3 (2) -179.92 (12) -4.24 (18) -1.8 (2) 173.87 (12) 12.0 (2) -169.97 (12)	$\begin{array}{c} N24 & -C25 & -C26 & -C28 \\ N24 & -C25 & -C26 & -C1 \\ N27 & -C1 & -C26 & -C28 \\ C2 & -C1 & -C26 & -C25 \\ C2 & -C1 & -C26 & -C25 \\ C20 & -C21 & -N27 & -C31 \\ C22 & -C21 & -N27 & -C31 \\ C20 & -C21 & -N27 & -C1 \\ C22 & -C21 & -N27 & -C1 \\ C22 & -C21 & -N27 & -C31 \\ C26 & -C1 & -N27 & -C31 \\ C26 & -C1 & -N27 & -C31 \\ C26 & -C1 & -N27 & -C21 \\ \end{array}$	57.46(14) - $62.65(14)$ 2.43(14) 128.63(11) 119.57(11) - $114.23(12)$ - $38.88(14)$ - $162.31(10)$ - $171.75(10)$ 64.81(12) 39.86(16) 164.43(10) 171.54(11)
$C_{1} = C_{2} = C_{3} = C_{4}$ $C_{1} = C_{2} = C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5} = C_{6}$ $C_{4} = C_{5} = C_{6} = C_{7}$ $C_{5} = C_{6} = C_{7} = C_{8}$ $C_{5} = C_{6} = C_{7} = C_{8}$ $C_{3} = C_{2} = C_{7} = C_{8}$ $C_{3} = C_{2} = C_{7} = C_{6}$ $C_{1} = C_{2} = C_{7} = C_{6}$ $C_{6} = C_{7} = C_{9}$ $C_{2} = C_{7} = C_{8} = C_{9}$ $C_{7} = C_{8} = C_{9} = C_{10}$	$\begin{array}{c} 1.7 (2) \\ -174.11 (12) \\ -0.1 (2) \\ -1.5 (2) \\ 1.3 (2) \\ 178.27 (13) \\ 0.3 (2) \\ -179.92 (12) \\ -4.24 (18) \\ -1.8 (2) \\ 173.87 (12) \\ 12.0 (2) \\ -169.97 (12) \\ 169.85 (11) \end{array}$	$\begin{array}{c} N24 - C25 - C26 - C28 \\ N24 - C25 - C26 - C1 \\ N27 - C1 - C26 - C28 \\ C2 - C1 - C26 - C28 \\ N27 - C1 - C26 - C25 \\ C2 - C1 - C26 - C25 \\ C20 - C21 - N27 - C31 \\ C22 - C21 - N27 - C31 \\ C22 - C21 - N27 - C1 \\ C22 - C21 - N27 - C1 \\ C22 - C1 - N27 - C31 \\ C26 - C1 - N27 - C31 \\ C26 - C1 - N27 - C21 \\ C26 - C1 - N27 - C21 \\ C26 - C1 - N27 - C21 \\ \end{array}$	57.46(14) - $62.65(14)$ 2.43(14) 128.63(11) 119.57(11) - $114.23(12)$ - $38.88(14)$ - $162.31(10)$ - $171.75(10)$ 64.81(12) 39.86(16) 164.43(10) 171.54(11) - $63.88(13)$
$C_{1} = C_{2} = C_{3} = C_{4}$ $C_{1} = C_{2} = C_{3} = C_{4} = C_{5}$ $C_{3} = C_{4} = C_{5} = C_{6}$ $C_{4} = C_{5} = C_{6} = C_{7} = C_{6}$ $C_{5} = C_{6} = C_{7} = C_{2}$ $C_{3} = C_{2} = C_{7} = C_{8}$ $C_{1} = C_{2} = C_{7} = C_{6}$ $C_{1} = C_{2} = C_{7} = C_{6}$ $C_{1} = C_{2} = C_{7} = C_{6}$ $C_{6} = C_{7} = C_{8} = C_{9}$ $C_{2} = C_{7} = C_{8} = C_{9}$ $C_{7} = C_{8} = C_{9} = C_{10}$ $O_{8} = C_{9} = C_{10} = O_{11}$	$\begin{array}{c} 1.7 (2) \\ -174.11 (12) \\ -0.1 (2) \\ -1.5 (2) \\ 1.3 (2) \\ 178.27 (13) \\ 0.3 (2) \\ -179.92 (12) \\ -4.24 (18) \\ -1.8 (2) \\ 173.87 (12) \\ 12.0 (2) \\ -169.97 (12) \\ 169.85 (11) \\ -67.15 (14) \end{array}$	$\begin{array}{l} N24 \\ -C25 \\ -C26 \\ -C1 \\ -C1 \\ -C26 \\ -C28 \\ -C1 \\ -C26 \\ -C28 \\ -C1 \\ -C26 \\ -C25 \\ -C2 \\ -C1 \\ -C26 \\ -C25 \\ -C20 \\ -C21 \\ -N27 \\ -C31 \\ -C20 \\ -C21 \\ -N27 \\ -C1 \\ -C22 \\ -C21 \\ -N27 \\ -C1 \\ -C22 \\ -C1 \\ -N27 \\ -C1 \\ -N27 \\ -C31 \\ -C26 \\ -C1 \\ -N27 \\ -C21 \\ -N27 \\ $	57.46(14) - $62.65(14)$ 2.43(14) 128.63(11) 119.57(11) - $114.23(12)$ - $38.88(14)$ - $162.31(10)$ - $171.75(10)$ 64.81(12) 39.86(16) 164.43(10) 171.54(11) - $63.88(13)$ - $105.51(14)$
$C_{1} - C_{2} - C_{3} - C_{4}$ $C_{2} - C_{3} - C_{4} - C_{5}$ $C_{3} - C_{4} - C_{5} - C_{6}$ $C_{4} - C_{5} - C_{6} - C_{7}$ $C_{5} - C_{6} - C_{7} - C_{8}$ $C_{5} - C_{6} - C_{7} - C_{2}$ $C_{3} - C_{2} - C_{7} - C_{8}$ $C_{1} - C_{2} - C_{7} - C_{8}$ $C_{3} - C_{2} - C_{7} - C_{6}$ $C_{1} - C_{2} - C_{7} - C_{6}$ $C_{1} - C_{2} - C_{7} - C_{6}$ $C_{6} - C_{7} - 0_{8} - C_{9}$ $C_{2} - C_{7} - 0_{8} - C_{9}$ $C_{7} - 0_{8} - C_{9} - C_{10}$ $0_{8} - C_{9} - C_{10} - 0_{11}$ $C_{9} - C_{10} - 0_{11} - C_{12}$	$\begin{array}{c} 1.7 (2) \\ -174.11 (12) \\ -0.1 (2) \\ -1.5 (2) \\ 1.3 (2) \\ 178.27 (13) \\ 0.3 (2) \\ -179.92 (12) \\ -4.24 (18) \\ -1.8 (2) \\ 173.87 (12) \\ 12.0 (2) \\ -169.97 (12) \\ 169.85 (11) \\ -67.15 (14) \\ 164.25 (12) \end{array}$	$\begin{array}{c} N24 - C25 - C26 - C28 \\ N24 - C25 - C26 - C1 \\ N27 - C1 - C26 - C28 \\ C2 - C1 - C26 - C28 \\ N27 - C1 - C26 - C25 \\ C2 - C1 - C26 - C25 \\ C20 - C21 - N27 - C31 \\ C22 - C21 - N27 - C31 \\ C20 - C21 - N27 - C1 \\ C22 - C21 - N27 - C1 \\ C22 - C1 - N27 - C31 \\ C26 - C1 - N27 - C31 \\ C26 - C1 - N27 - C21 \\ C26 - C1 - N27 - C21 \\ C23 - C22 - C28 - O28 \\ C21 - C22 - C28 - O28 \\ C21 - C22 - C28 - O28 \\ \end{array}$	57.46(14) - $62.65(14)$ 2.43(14) 128.63(11) 119.57(11) - $114.23(12)$ - $38.88(14)$ - $162.31(10)$ - $171.75(10)$ 64.81(12) 39.86(16) 164.43(10) 171.54(11) - $63.88(13)$ - $105.51(14)$ 134.37(13)
$C_{1} - C_{2} - C_{3} - C_{4}$ $C_{1} - C_{2} - C_{3} - C_{4} - C_{5}$ $C_{3} - C_{4} - C_{5} - C_{6}$ $C_{4} - C_{5} - C_{6} - C_{7} - C_{7}$ $C_{5} - C_{6} - C_{7} - C_{2}$ $C_{3} - C_{2} - C_{7} - C_{8}$ $C_{1} - C_{2} - C_{7} - C_{8}$ $C_{3} - C_{2} - C_{7} - C_{6}$ $C_{1} - C_{2} - C_{7} - C_{6}$ $C_{6} - C_{7} - O_{8} - C_{9}$ $C_{2} - C_{7} - O_{8} - C_{9}$ $C_{7} - O_{8} - C_{9} - C_{10}$ $O_{8} - C_{9} - C_{10} - O_{11}$ $C_{9} - C_{10} - O_{11} - C_{12}$ $C_{10} - O_{11} - C_{12} - C_{13}$	$\begin{array}{c} 1.7 (2) \\ -174.11 (12) \\ -0.1 (2) \\ -1.5 (2) \\ 1.3 (2) \\ 178.27 (13) \\ 0.3 (2) \\ -179.92 (12) \\ -4.24 (18) \\ -1.8 (2) \\ 173.87 (12) \\ 12.0 (2) \\ -169.97 (12) \\ 169.85 (11) \\ -67.15 (14) \\ 164.25 (12) \\ -156.42 (12) \end{array}$	$\begin{array}{c} N24 - C25 - C26 - C28 \\ N24 - C25 - C26 - C1 \\ N27 - C1 - C26 - C28 \\ C2 - C1 - C26 - C28 \\ N27 - C1 - C26 - C25 \\ C2 - C1 - C26 - C25 \\ C20 - C21 - N27 - C31 \\ C22 - C21 - N27 - C31 \\ C20 - C21 - N27 - C1 \\ C22 - C21 - N27 - C1 \\ C22 - C21 - N27 - C1 \\ C22 - C1 - N27 - C31 \\ C26 - C1 - N27 - C31 \\ C26 - C1 - N27 - C21 \\ C23 - C22 - C28 - O28 \\ C21 - C22 - C28 - O28 \\ C23 - C22 - C28 - C26 \\ \end{array}$	57.46(14) - $62.65(14)$ 2.43(14) 128.63(11) 119.57(11) - $114.23(12)$ - $38.88(14)$ - $162.31(10)$ - $171.75(10)$ 64.81(12) 39.86(16) 164.43(10) 171.54(11) - $63.88(13)$ - $105.51(14)$ 134.37(13) 65.06(13)
$C_{1}-C_{2}-C_{3}-C_{4}$ $C_{1}-C_{2}-C_{3}-C_{4}-C_{5}$ $C_{3}-C_{4}-C_{5}-C_{6}$ $C_{4}-C_{5}-C_{6}-C_{7}$ $C_{5}-C_{6}-C_{7}-C_{2}$ $C_{3}-C_{2}-C_{7}-O_{8}$ $C_{1}-C_{2}-C_{7}-O_{8}$ $C_{3}-C_{2}-C_{7}-C_{6}$ $C_{1}-C_{2}-C_{7}-C_{6}$ $C_{6}-C_{7}-O_{8}-C_{9}$ $C_{2}-C_{7}-O_{8}-C_{9}$ $C_{2}-C_{7}-O_{8}-C_{9}$ $C_{7}-O_{8}-C_{9}-C_{10}$ $O_{8}-C_{9}-C_{10}-O_{11}$ $C_{9}-C_{10}-O_{11}-C_{12}$ $C_{10}-O_{11}-C_{12}-C_{13}$ $O_{11}-C_{12}-C_{13}-O_{14}$	$\begin{array}{c} 1.7 (2) \\ -174.11 (12) \\ -0.1 (2) \\ -1.5 (2) \\ 1.3 (2) \\ 178.27 (13) \\ 0.3 (2) \\ -179.92 (12) \\ -4.24 (18) \\ -1.8 (2) \\ 173.87 (12) \\ 12.0 (2) \\ -169.97 (12) \\ 169.85 (11) \\ -67.15 (14) \\ 164.25 (12) \\ -156.42 (12) \\ 70.09 (14) \end{array}$	$\begin{array}{c} N24 - C25 - C26 - C28\\ N24 - C25 - C26 - C1\\ N27 - C1 - C26 - C28\\ C2 - C1 - C26 - C28\\ N27 - C1 - C26 - C25\\ C2 - C1 - C26 - C25\\ C20 - C21 - N27 - C31\\ C22 - C21 - N27 - C31\\ C20 - C21 - N27 - C1\\ C22 - C21 - N27 - C1\\ C22 - C1 - N27 - C31\\ C26 - C1 - N27 - C31\\ C26 - C1 - N27 - C21\\ C23 - C22 - C28 - O28\\ C21 - C22 - C28 - O28\\ C23 - C22 - C28 - C26\\ C21 - C22 - C28 - C26\\ \end{array}$	57.46(14) -62.65(14) 2.43(14) 128.63(11) 119.57(11) -114.23(12) -38.88(14) -162.31(10) -171.75(10) 64.81(12) 39.86(16) 164.43(10) 171.54(11) -63.88(13) -105.51(14) 134.37(13) 65.06(13) -55.06(13)

C13-014-C15-C16	-17.86(18)	C1 - C26 - C28 - O28	-133.57(13)
C13—O14—C15—C20	164.85 (11)	C25—C26—C28—C22	-64.49 (13)
O14—C15—C16—C17	-176.19 (12)	C1—C26—C28—C22	55.92 (13)
C20-C15-C16-C17	0.99 (19)	C23—N24—C29—O29	-0.9 (2)
C15—C16—C17—C18	-0.8 (2)	C25—N24—C29—O29	-179.56 (13)
C16—C17—C18—C19	0.0 (2)	C23—N24—C29—C30	179.47 (12)
C17—C18—C19—C20	0.7 (2)	C25—N24—C29—C30	0.8 (2)
C18—C19—C20—C15	-0.51 (19)	C21—N27—C31—C32	127.63 (12)
C18—C19—C20—C21	175.64 (12)	C1—N27—C31—C32	-102.47 (14)
O14—C15—C20—C19	177.05 (11)	C21—N27—C31—C35	-49.22 (15)
C16—C15—C20—C19	-0.34 (18)	C1—N27—C31—C35	80.68 (14)
O14—C15—C20—C21	0.99 (17)	N27—C31—C32—C33	-175.87 (11)
C16—C15—C20—C21	-176.40 (11)	C35—C31—C32—C33	0.9 (2)
C19—C20—C21—N27	126.37 (12)	C31—C32—C33—O33	119.73 (16)
C15—C20—C21—N27	-57.63 (15)	C31—C32—C33—O34	-63.77 (18)
C19—C20—C21—C22	-111.98 (13)	O33—C33—O34—C34	-5.65 (19)
C15—C20—C21—C22	64.01 (15)	C32—C33—O34—C34	177.93 (12)
N27—C21—C22—C28	-3.72 (14)	C32—C31—C35—O35	-28.2 (2)
C20—C21—C22—C28	-128.38 (11)	N27—C31—C35—O35	148.54 (13)
N27—C21—C22—C23	-120.71 (11)	C32—C31—C35—O36	152.95 (12)
C20—C21—C22—C23	114.63 (11)	N27—C31—C35—O36	-30.27 (15)
C28—C22—C23—N24	-58.32 (14)	O35—C35—O36—C36	-2.02 (19)
C21—C22—C23—N24	61.39 (13)	C31—C35—O36—C36	176.78 (11)

*Hydrogen-bond geometry (Å, °)* 

D—H···A	D—H	H···A	D··· $A$	D—H···A
C18—H18…O35 <sup>i</sup>	0.95	2.47	3.1735 (17)	131
С25—Н25А…О33іі	0.99	2.30	3.2091 (17)	152
C34—H34A····O35 <sup>iii</sup>	0.98	2.53	3.5045 (19)	174

Symmetry codes: (i) *x*, -*y*+1/2, *z*+1/2; (ii) *x*-1, *y*, *z*; (iii) *x*, -*y*+1/2, *z*-1/2.