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Dicarbonyl(η^5 -cyclopentadienyl)(hexamethylenetetramine- κN^1)iron(II) tetrafluoridoborate

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Key indicators: single-crystal X-ray study; T = 173 K; mean σ (C–C) = 0.003 Å; disorder in solvent or counterion; *R* factor = 0.034; *wR* factor = 0.092; data-to-parameter ratio = 15.9.

In the structure of the title compound, $[Fe(C_5H_5)(C_6H_{12}N_4)-(CO)_2]BF_4$, the arrangement around the Fe^{II} atom corresponds to that of a three-legged piano stool. The cyclopentadienyl ligand occupies three coordination sites of the apical position in a η^5 fashion, while two CO ligands and one N atom of the hexamethylenetetramine ligand occupy the remaining coordination sites to complete a distorted octahedral geometry. The asymmetric unit consists of two sets of crystallographically independent cations and anions with the r.m.s. deviations of the overlay of non-H atoms of each pair being 0.081 and 0.120 Å, respectively. The Fe – N bond lengths are 2.0459 (15) and 2.0490 (14) Å, while the Fe – Cp(centroid) distances are 1.7257 (3) and 1.7246 (3) Å. One of the anions displays disorder, with the F atoms having occupancies of 0.58 (4) and 0.42 (4).

Related literature

For the synthesis of the title compound and structure of the dinuclear compound $[Fe_2(\eta^5-C_5H_5)_2(C_6H_{12}N_4)(CO)_4](BF_4)_2$, see: M'thiruaine, Friedrich, Changamu & Bala (2012). For other related compounds, see: Matos & Verkade (2003); M'thiruaine, Friedrich, Changamu & Fernandes (2012); M'thiruaine *et al.* (2011).



Experimental

Crystal data

 $[Fe(C_5H_5)(C_6H_{12}N_4)(CO)_2]BF_4$ $M_r = 403.97$ Monoclinic, $P2_1/c$ a = 15.1054 (6) Å b = 14.6407 (6) Å c = 14.2267 (6) Å $\beta = 96.997$ (2)°

Data collection

Bruker SMART APEXII CCD diffractometer Absorption correction: multi-scan (*SADABS*; Bruker, 2008) *T*_{min} = 0.673, *T*_{max} = 0.853

Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.034$ $wR(F^2) = 0.092$ S = 1.087768 reflections 488 parameters $V = 3122.9 \text{ (2) } \text{\AA}^3$ Z = 8 Mo K\alpha radiation \mu = 1.03 mm^{-1} T = 173 K 0.42 \times 0.16 mm

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62504 measured reflections
7768 independent reflections
6765 reflections with I > 2\sigma(I)
R_{\text{int}} = 0.033
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12 restraints H-atom parameters constrained
$$\begin{split} &\Delta\rho_{max}=0.63\ e\ {\mbox{\AA}}^{-3}\\ &\Delta\rho_{min}=-0.43\ e\ {\mbox{\AA}}^{-3} \end{split}$$

Data collection: *APEX2* (Bruker, 2008); cell refinement: *SAINT-Plus* (Bruker, 2008); data reduction: *SAINT-Plus* and *XPREP* (Bruker, 2008); program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *ORTEP-3* (Farrugia, 1997); software used to prepare material for publication: *WinGX* (Farrugia, 1999).

Our acknowledgement goes to the University of KwaZulu-Natal for resources and financial support.

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: KJ2206).

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supporting information

Acta Cryst. (2012). E68, m1077 [https://doi.org/10.1107/S1600536812031649] Dicarbonyl(η^5 -cyclopentadienyl)(hexamethylenetetramine- κN^1)iron(II) tetrafluoridoborate

Cyprian M. M'thiruaine, Holger B. Friedrich and Bernard Omondi

S1. Comment

The title compound was obtained as part of our ongoing investigation of the reactions of substitutionally unsaturated metal complexes with nitrogen donor ligands. The synthesis and characterization data was previously reported by us. (M'thiruaine *et al.*, 2011; M'thiruaine, Friedrich, Changamu & Fernandes, 2012). The asymmetric unit consists of two independent molecules of $[Fe(\eta^5-C_5H_5){N_4(CH_2)_6}(CO)_2]^+$ and two molecules of BF_4^- . The structure exhibits a typical three legged piano stool structure with Fe^{II} coordinated by one nitrogen atom of the hexamethylenetetramine ligand and two of the CO ligands. The coordination geometry around Fe is that of the distorted octahedral in which three sites are occupied by the η^5 -cyclopentadienyl ligand, two by the CO ligands and one by an N atom of the hexamethylenetetramine. Its structure is closely similar to that of recently reported pentamethylcyclopentadienyl analogue compound $[Fe{\eta^5-C_5(CH_3)_5}{N_4(CH_2)_6}(CO)_2]BF_4$ (M'thiruaine, Friedrich, Changamu & Fernandes, 2012). One of the anions displays disorder with the fluorine atoms having occupancies of 0.58 (4) for F1A, F2A, F3A and F4A, and 0.42 (4) for F1B, F2B, F3B and F4B.

The asymmetric unit consist of two sets of crystallographically independent molecules of the cations [r.m.s = 0.081 Å] and anions [r.m.s. = 0.120 Å]. The cations are related by a non-crystallographic translation across the *ac* diagonal. The Fe —N bonds distances are 2.0458 (15) and 2.0489 (14) Å, which are slightly shorter than the corresponding distances of the Cp* analogue (M'thiruaine, Friedrich, Changamu & Fernandes, 2012) (2.069 (2) Å) and of the dinuclear complex $[{Cp(CO)_2Fe}_2{N_4(CH_2)_6}]^{2+}$ (M'thiruaine, Friedrich, Changamu & Bala, 2012) (2.0817 (17) and 2.0858 (18) Å) as well as that of $[(CO)_4Fe{N_2(CH_2)_6}]$ (Matos and Verkade, 2003) (2.092 (4) Å).

S2. Experimental

The title compound was prepared according to a reported procedure (M'thiruaine, Friedrich, Changamu & Bala, 2012) and crystals were grown by layering a concentrated solution of the compound in acetone with Et_2O and the mixture kept undisturbed in the dark for four weeks.

S3. Refinement

Carbon-bound H-atoms were placed in calculated positions [C—H = 0.97 Å for for methylene H atoms and 0.98 for methine H atoms; $U_{iso}(H) = 1.2U_{eq}(C)$] and were included in the refinement in the riding model approximation. One of the tetrafluoroborate anions was refined with a disorder model. The total occupancy of each atom was constrained to 1; the occupancy for sites F1A, F2A, F3A and F4A was 0.58 (4) and 0.42 (4) for F1B, F2B, F3B and F4B. F4A and F4B were refined with restraints to prevent extreme anisotropy. One reflection (1 0 0) was omited from the *hkl* file.





Molecular structure of the title complex with the atom labeling scheme. Ellipsoids are drawn at 50% probability level.

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Crystal data

```
[Fe(C_{5}H_{5})(C_{6}H_{12}N_{4})(CO)_{2}]BF_{4}

M_{r} = 403.97

Monoclinic, P2_{1}/c

Hall symbol: -P 2ybc

a = 15.1054 (6) Å

b = 14.6407 (6) Å

c = 14.2267 (6) Å

\beta = 96.997 (2)°

V = 3122.9 (2) Å<sup>3</sup>

Z = 8
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Data collection

Bruker SMART APEXII CCD diffractometer Graphite monochromator φ and ω scans Absorption correction: multi-scan (*SADABS*; Bruker, 2008) $T_{\min} = 0.673$, $T_{\max} = 0.853$ 62504 measured reflections

Refinement

Refinement on F^2 Least-squares matrix: full $R[F^2 > 2\sigma(F^2)] = 0.034$ $wR(F^2) = 0.092$ S = 1.087768 reflections 488 parameters 12 restraints F(000) = 1648 $D_x = 1.718 \text{ Mg m}^{-3}$ Mo K\alpha radiation, $\lambda = 0.71073 \text{ Å}$ Cell parameters from 63978 reflections $\theta = 1.9-28.3^{\circ}$ $\mu = 1.03 \text{ mm}^{-1}$ T = 173 KBlock, yellow $0.42 \times 0.19 \times 0.16 \text{ mm}$

7768 independent reflections 6765 reflections with $I > 2\sigma(I)$ $R_{int} = 0.033$ $\theta_{max} = 28.3^\circ, \ \theta_{min} = 1.9^\circ$ $h = -20 \rightarrow 20$ $k = -19 \rightarrow 19$ $l = -18 \rightarrow 18$

Primary atom site location: structure-invariant direct methods
Secondary atom site location: difference Fourier map
Hydrogen site location: inferred from neighbouring sites
H-atom parameters constrained

 $w = 1/[\sigma^{2}(F_{o}^{2}) + (0.0391P)^{2} + 2.9672P] \qquad \Delta \rho_{max} = 0.63 \text{ e } \text{\AA}^{-3}$ where $P = (F_{o}^{2} + 2F_{c}^{2})/3 \qquad \Delta \rho_{min} = -0.43 \text{ e } \text{\AA}^{-3}$ $(\Delta / \sigma)_{max} = 0.026$

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates an	<i>id isotropic or</i>	equivalent isotrop	oic displacement	parameters	$(Å^2)$)
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	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	Occ. (<1)
C1	0.86930 (13)	-0.03952 (15)	0.80821 (16)	0.0275 (4)	
H1	0.8674	-0.1007	0.8393	0.033*	
C2	0.87149 (14)	0.04629 (15)	0.85391 (15)	0.0292 (4)	
H2	0.8723	0.0563	0.9235	0.035*	
C3	0.87061 (14)	0.11633 (15)	0.78406 (17)	0.0323 (5)	
H3	0.8709	0.1837	0.7957	0.039*	
C4	0.86568 (13)	0.07273 (17)	0.69515 (16)	0.0339 (5)	
H4	0.8639	0.1044	0.6327	0.041*	
C5	0.86628 (13)	-0.02251 (17)	0.70865 (16)	0.0320 (5)	
Н5	0.863	-0.0699	0.6577	0.038*	
C6	1.04710 (15)	0.07326 (13)	0.88830 (14)	0.0270 (4)	
C7	1.04138 (12)	-0.07593 (12)	0.78590 (13)	0.0204 (4)	
C8	1.16153 (11)	0.07250 (12)	0.72516 (14)	0.0199 (4)	
H8A	1.1768	0.0981	0.7895	0.024*	
H8B	1.1723	0.0058	0.7289	0.024*	
C9	1.19672 (12)	0.07558 (13)	0.56646 (14)	0.0235 (4)	
H9A	1.2072	0.0088	0.5678	0.028*	
H9B	1.2362	0.1032	0.5235	0.028*	
C10	1.08860 (12)	0.19357 (13)	0.52845 (13)	0.0214 (4)	
H10A	1.1265	0.2222	0.4846	0.026*	
H10B	1.0256	0.2068	0.5047	0.026*	
C11	1.05207 (13)	0.19222 (12)	0.68625 (13)	0.0200 (4)	
H11A	0.9892	0.2066	0.6627	0.024*	
H11B	1.0654	0.219	0.7503	0.024*	
C12	1.04575 (12)	0.05226 (12)	0.59314 (12)	0.0189 (3)	
H12A	1.0556	-0.0146	0.5947	0.023*	
H12B	0.9826	0.0634	0.5683	0.023*	
C13	1.20368 (13)	0.21211 (12)	0.65816 (15)	0.0241 (4)	
H13A	1.2431	0.2405	0.6156	0.029*	
H13B	1.219	0.2384	0.7222	0.029*	
C14	0.35418 (12)	0.09213 (13)	0.27619 (14)	0.0213 (4)	
H14	0.3491	0.1598	0.2835	0.026*	

C15	0.35489 (12)	0.02563 (13)	0.34992 (14)	0.0219 (4)	
H15	0.3497	0.0387	0.418	0.026*	
C16	0.36150 (12)	-0.06169(13)	0.30960 (14)	0.0226 (4)	
H16	0.3617	-0.1213	0.344	0.027*	
C17	0.36425 (12)	-0.05030(14)	0.21025 (14)	0.0237 (4)	
H17	0.3679	-0.1003	0.163	0.028*	
C18	0.35832 (12)	0.04445 (14)	0.19039 (14)	0.0224 (4)	
H18	0.3588	0.073	0.1266	0.027*	
C19	0.52488 (12)	0.07220 (13)	0.39393 (13)	0.0210 (4)	
C20	0.53847 (12)	-0.08684(12)	0.31050 (13)	0.0192 (3)	
C21	0.54333(12)	0.17549 (11)	0.19492 (13)	0.0170(3)	
H21A	0.4811	0.1876	0.1672	0.02*	
H21B	0 5522	0 2034	0 2588	0.02*	
C22	0.69695(12)	0 19948 (12)	0.17685 (14)	0.0212 (4)	
H22A	0 7383	0 2289	0.1371	0.0212 (1)	
H22R H22B	0.7076	0.2269	0.241	0.025*	
C23	0.69925 (12)	0.06230 (13)	0.08670 (14)	0.025	
H23A	0.7117	-0.0041	0.0894	0.0210 (1)	
H23R	0.7405	0.000	0.0463	0.026*	
C24	0.7403 0 54675 (12)	0.03453(12)	0.10393 (12)	0.020	
H24A	0.5587	-0.032	0.107	0.021*	
H24R	0.4843	0.032	0.0751	0.021	
C25	0.4645	0.0494 (12)	0.0751 0.24201(13)	0.021 0.0182 (3)	
H25A	0.659	0.085	0.3066	0.0102 (5)	
H25R	0.6671	-0.0074	0.2467	0.022	
C26	0.58916 (13)	0.0074 0.17684 (12)	0.2407 0.04086 (13)	0.022 0.0210 (4)	
H26A	0.6289	0.2065	-0.0004	0.0210 (4)	
H26R	0.5268	0.1879	0.0131	0.025*	
R1	0.32781 (15)	0.1079 0.21448 (14)	0.93390(14)	0.023 (4)	
B1 B2	1 18854 (14)	-0.20775(13)	0.55550(11) 0.54535(13)	0.0209(1) 0.0169(4)	
N1	1.06343 (9)	0.08967 (10)	0.69277 (10)	0.0103(1)	
N2	1.00313(9)	0.00007(10) 0.23350(10)	0.69277(10)	0.0191(3) 0.0209(3)	
N3	1.11000(11) 1.21930(10)	0.23330(10) 0.11287(11)	0.62302(11) 0.66204(12)	0.0203(3) 0.0222(3)	
N4	1.10294 (10)	0.09386 (11)	0.52956 (11)	0.0222(3) 0.0201(3)	
N5	0 55772 (9)	0.07343 (9)	0.20366 (10)	0.0201(3) 0.0145(3)	
N6	0.55772(5) 0.60404(10)	0.07315(9) 0.21776(10)	0.20500(10) 0.13595(11)	0.0189(3)	
N7	0.71550 (10)	0.10091 (10)	0.18284 (11)	0.0107(3)	
N8	0.60659 (10)	0.07755(10)	0.04412(11)	0.0193(3)	
01	1.08297(13)	0.09476(12)	0.01112(11) 0.95985(11)	0.0135(5) 0.0436(4)	
02	1.00257 (15)	-0.14597(9)	0.79173(12)	0.0130(1) 0.0314(3)	
03	0.55295(10)	0.14397(9) 0.10444(11)	0.79175(12) 0.46397(10)	0.0314(3)	
04	0.57492 (9)	-0.15342(9)	0.32834(11)	0.0265(3)	
F1A	0.37192(0) 0.2452(6)	0.2217(16)	0.8959 (7)	0.0205(3)	0.58(4)
F2A	0.3595 (6)	0.3019 (6)	0.0999(7) 0.9694(4)	0.071(5)	0.50(1) 0.58(4)
F3A	0 313 (2)	0.1541(5)	0 9998 (6)	0 073 (4)	0.53(1) 0.58(4)
F4A	0.3667(12)	0 1825 (12)	0 8619 (12)	0.056(3)	0.53(4)
F1B	0 2404 (8)	0 2517 (10)	0.8923 (7)	0.045(2)	0.33(4) 0.42(4)
F2B	0 3690 (8)	0 2897 (11)	0.0723(7)	0.065(2)	0.12(-7) 0.42(4)
1 2 1	0.5070 (0)	0.2077 (11)		0.000 (0)	U.72 (T)

supporting information

F3B	0.3532 (9)	0.1541 (7)	1.0064 (8)	0.0482 (19)	0.42 (4)	
F4B	0.3880 (12)	0.1945 (13)	0.8637 (15)	0.040 (2)	0.42 (4)	
F5	1.23942 (12)	-0.14457 (10)	0.50207 (12)	0.0563 (4)		
F6	1.13743 (11)	-0.16773 (11)	0.60532 (11)	0.0495 (4)		
F7	1.24900 (10)	-0.26959 (10)	0.59476 (9)	0.0434 (4)		
F8	1.13740 (10)	-0.25675 (15)	0.47543 (13)	0.0673 (6)		
Fe1	0.983683 (17)	0.031636 (17)	0.782706 (18)	0.01738 (7)		
Fe2	0.473433 (16)	0.015894 (16)	0.289440 (17)	0.01452 (7)		

Atomic displacement parameters $(Å^2)$

	U^{11}	U ²²	U^{33}	U^{12}	U^{13}	U^{23}
C1	0.0159 (9)	0.0308 (10)	0.0367 (11)	0.0006 (7)	0.0069 (8)	0.0042 (8)
C2	0.0257 (10)	0.0341 (11)	0.0306 (11)	0.0085 (8)	0.0141 (8)	0.0059 (8)
C3	0.0240 (10)	0.0317 (11)	0.0442 (12)	0.0125 (8)	0.0162 (9)	0.0123 (9)
C4	0.0137 (9)	0.0554 (14)	0.0330 (11)	0.0105 (9)	0.0052 (8)	0.0164 (10)
C5	0.0116 (8)	0.0503 (13)	0.0339 (11)	-0.0003 (8)	0.0016 (8)	-0.0037 (10)
C6	0.0370 (11)	0.0218 (9)	0.0228 (10)	-0.0029 (8)	0.0054 (8)	0.0008 (7)
C7	0.0140 (8)	0.0209 (9)	0.0266 (9)	-0.0040 (7)	0.0033 (7)	0.0007 (7)
C8	0.0122 (8)	0.0188 (8)	0.0273 (9)	-0.0004 (6)	-0.0028 (7)	0.0041 (7)
C9	0.0171 (9)	0.0209 (9)	0.0341 (10)	0.0003 (7)	0.0094 (8)	-0.0011 (7)
C10	0.0193 (9)	0.0230 (9)	0.0215 (9)	0.0006 (7)	0.0009 (7)	0.0033 (7)
C11	0.0255 (9)	0.0126 (8)	0.0221 (9)	0.0045 (7)	0.0036 (7)	0.0003 (6)
C12	0.0169 (8)	0.0205 (8)	0.0194 (8)	-0.0031 (7)	0.0028 (7)	-0.0050(7)
C13	0.0223 (9)	0.0172 (8)	0.0312 (10)	-0.0060 (7)	-0.0027 (8)	0.0019 (7)
C14	0.0136 (8)	0.0208 (9)	0.0298 (10)	0.0041 (7)	0.0032 (7)	0.0024 (7)
C15	0.0153 (8)	0.0264 (9)	0.0251 (9)	0.0025 (7)	0.0062 (7)	0.0012 (7)
C16	0.0131 (8)	0.0205 (9)	0.0344 (10)	-0.0022 (7)	0.0035 (7)	0.0038 (7)
C17	0.0136 (8)	0.0263 (9)	0.0305 (10)	-0.0030 (7)	0.0001 (7)	-0.0068 (8)
C18	0.0122 (8)	0.0312 (10)	0.0233 (9)	-0.0005 (7)	0.0002 (7)	0.0038 (7)
C19	0.0187 (9)	0.0212 (9)	0.0235 (9)	-0.0013 (7)	0.0037 (7)	0.0003 (7)
C20	0.0156 (8)	0.0183 (8)	0.0241 (9)	-0.0049 (7)	0.0043 (7)	0.0010 (7)
C21	0.0184 (8)	0.0106 (7)	0.0221 (9)	0.0006 (6)	0.0022 (7)	0.0001 (6)
C22	0.0180 (9)	0.0172 (8)	0.0278 (9)	-0.0060 (7)	0.0002 (7)	0.0013 (7)
C23	0.0161 (8)	0.0208 (9)	0.0290 (10)	-0.0001 (7)	0.0064 (7)	0.0004 (7)
C24	0.0170 (8)	0.0172 (8)	0.0193 (8)	-0.0036 (6)	0.0035 (7)	-0.0049 (6)
C25	0.0123 (8)	0.0177 (8)	0.0239 (9)	-0.0005 (6)	-0.0004 (7)	0.0043 (7)
C26	0.0208 (9)	0.0207 (9)	0.0215 (9)	-0.0014 (7)	0.0023 (7)	0.0043 (7)
B1	0.0285 (11)	0.0201 (10)	0.0119 (9)	0.0064 (8)	0.0009 (8)	-0.0050(7)
B2	0.0206 (10)	0.0182 (9)	0.0112 (8)	0.0048 (7)	-0.0012 (7)	-0.0018 (7)
N1	0.0135 (7)	0.0133 (6)	0.0181 (7)	0.0017 (5)	0.0003 (5)	-0.0015 (5)
N2	0.0240 (8)	0.0148 (7)	0.0235 (8)	0.0009 (6)	0.0010 (6)	0.0012 (6)
N3	0.0146 (7)	0.0182 (7)	0.0331 (9)	-0.0017 (6)	0.0004 (6)	0.0046 (6)
N4	0.0180 (7)	0.0211 (7)	0.0220 (8)	-0.0030 (6)	0.0054 (6)	-0.0028 (6)
N5	0.0130 (7)	0.0109 (6)	0.0191 (7)	-0.0001 (5)	0.0000 (5)	-0.0006 (5)
N6	0.0186 (7)	0.0141 (7)	0.0238 (8)	-0.0017 (5)	0.0018 (6)	0.0025 (6)
N7	0.0138 (7)	0.0178 (7)	0.0274 (8)	-0.0021 (6)	0.0015 (6)	0.0040 (6)
N8	0.0167 (7)	0.0201 (7)	0.0216 (8)	-0.0026 (6)	0.0040 (6)	-0.0012 (6)

supporting information

01	0.0653 (12)	0.0411 (9)	0.0227 (8)	-0.0158 (8)	-0.0016 (8)	-0.0032 (7)
O2	0.0222 (7)	0.0177 (7)	0.0560 (10)	0.0011 (5)	0.0115 (7)	0.0059 (6)
O3	0.0325 (8)	0.0376 (8)	0.0243 (7)	-0.0066 (7)	-0.0001 (6)	-0.0066 (6)
O4	0.0189 (7)	0.0173 (6)	0.0435 (8)	0.0020 (5)	0.0049 (6)	0.0076 (6)
F1A	0.035 (2)	0.126 (9)	0.051 (3)	-0.004 (4)	-0.005 (2)	-0.042 (4)
F2A	0.074 (4)	0.0210 (19)	0.035 (2)	-0.0067 (18)	0.028 (3)	-0.0028 (14)
F3A	0.154 (12)	0.0319 (18)	0.038 (2)	0.012 (4)	0.026 (5)	0.0130 (15)
F4A	0.069 (6)	0.059 (5)	0.040 (3)	0.034 (4)	0.010 (4)	-0.005 (3)
F1B	0.039 (3)	0.074 (5)	0.024 (3)	0.009 (3)	0.015 (2)	0.008 (4)
F2B	0.055 (4)	0.049 (5)	0.081 (6)	-0.009 (3)	-0.031 (5)	-0.014 (3)
F3B	0.066 (5)	0.038 (2)	0.042 (3)	0.016 (3)	0.012 (3)	0.022 (2)
F4B	0.050 (5)	0.040 (3)	0.034 (4)	0.021 (3)	0.023 (4)	0.001 (3)
F5	0.0730 (12)	0.0375 (8)	0.0622 (10)	0.0071 (8)	0.0233 (9)	0.0146 (7)
F6	0.0527 (9)	0.0541 (9)	0.0432 (8)	0.0255 (7)	0.0116 (7)	-0.0125 (7)
F7	0.0462 (8)	0.0527 (9)	0.0333 (7)	0.0256 (7)	0.0121 (6)	0.0164 (6)
F8	0.0338 (8)	0.1018 (15)	0.0636 (11)	0.0017 (9)	-0.0049 (7)	-0.0475 (10)
Fe1	0.01647 (13)	0.01728 (13)	0.01851 (13)	0.00332 (9)	0.00265 (10)	0.00090 (9)
Fe2	0.01275 (12)	0.01259 (12)	0.01814 (13)	0.00006 (8)	0.00148 (9)	-0.00002 (9)

Geometric parameters (Å, °)

C1—C2	1.413 (3)	C16—C17	1.429 (3)
C1—C5	1.433 (3)	C16—Fe2	2.0855 (18)
C1—Fe1	2.087 (2)	C16—H16	1
C1—H1	1	C17—C18	1.416 (3)
C2—C3	1.427 (3)	C17—Fe2	2.1157 (18)
C2—Fe1	2.0887 (19)	C17—H17	1
С2—Н2	1	C18—Fe2	2.1418 (18)
C3—C4	1.411 (3)	C18—H18	1
C3—Fe1	2.113 (2)	C19—O3	1.137 (2)
С3—Н3	1	C19—Fe2	1.7921 (19)
C4—C5	1.408 (3)	C20—O4	1.133 (2)
C4—Fe1	2.133 (2)	C20—Fe2	1.8016 (18)
C4—H4	1	C21—N6	1.454 (2)
C5—Fe1	2.104 (2)	C21—N5	1.513 (2)
С5—Н5	1	C21—H21A	0.99
C6—O1	1.138 (3)	C21—H21B	0.99
C6—Fe1	1.788 (2)	C22—N7	1.471 (2)
C7—O2	1.134 (2)	C22—N6	1.477 (2)
C7—Fe1	1.7978 (19)	C22—H22A	0.99
C8—N3	1.452 (2)	C22—H22B	0.99
C8—N1	1.518 (2)	C23—N7	1.473 (2)
C8—H8A	0.99	C23—N8	1.473 (2)
C8—H8B	0.99	C23—H23A	0.99
C9—N3	1.466 (3)	C23—H23B	0.99
C9—N4	1.474 (2)	C24—N8	1.458 (2)
С9—Н9А	0.99	C24—N5	1.519 (2)
С9—Н9В	0.99	C24—H24A	0.99

C10—N2	1.474 (2)	C24—H24B	0.99
C10—N4	1.476 (2)	C25—N7	1.455 (2)
C10—H10A	0.99	C25—N5	1.516 (2)
C10—H10B	0.99	С25—Н25А	0.99
C11—N2	1.454 (2)	С25—Н25В	0.99
C11—N1	1.513 (2)	C26—N6	1.471 (2)
C11—H11A	0.99	C26—N8	1.477 (2)
С11—Н11В	0.99	C26—H26A	0.99
C12—N4	1.458 (2)	C26—H26B	0.99
C12—N1	1.513 (2)	B1—F1A	1.303 (11)
C12—H12A	0.99	B1—F3A	1 328 (8)
C12—H12B	0.99	B1—F4A	1.326(0) 1.326(16)
C13—N3	1472(2)	B1—F2B	1.320(10) 1.357(11)
C13—N2	1.172(2) 1 474(2)	B1—F3B	1.327(10)
C13—H13A	0.99	B1—F2A	1.377(10) 1 436 (7)
C13—H13B	0.99	B1—F4B	1.460(17)
C14— $C18$	1414(3)	B1—F1B	1.483(12)
C_{14} C_{15}	1.430(3)	B2F6	1.403(12) 1.352(2)
C14—Fe2	2 1079 (18)	B2—F8	1.332(2) 1 383(2)
C14—H14	1	B2F5	1.303(2) 1 393(3)
C_{15}	1 410(3)	B2—F7	1.373(3)
C15 - E10	2.0838(18)	N1_Fe1	2.0459(15)
C15 H15	2.0030 (10)	N5 Fe2	2.0439(13) 2.0490(14)
015-1115	1	113-102	2.0490 (14)
C2-C1-C5	107 24 (19)	N5-C25-H25A	109.1
$C_2 = C_1 = F_{e_1}$	70.29(12)	N7-C25-H25B	109.1
C_{2} C_{1} E_{1}	70.66 (12)	N5-C25-H25B	109.1
$C_2 - C_1 - H_1$	126.4	$H_{25}^{-} = C_{25}^{-} = H_{25}^{-} B$	107.8
C5-C1-H1	126.4	N6_C26_N8	107.0 111 42 (14)
E_{2} C_{1} H_{1}	120.4	$N_{0} = C_{20} = N_{0}$	100 3
$C_1 = C_2 = C_3$	120.4	N8 C26 H26A	109.3
$C_1 = C_2 = C_3$	100.7(2)	N6 C26 H26P	109.3
$C_1 = C_2 = Fe_1$	70.13 (11)	NG-C26-H26B	109.3
$C_3 = C_2 = H_2$	125.6	$H_{20} = 120B$	109.5
$C_1 = C_2 = H_2$	125.6	$F_{1} \wedge P_{1} = F_{2} \wedge$	108
$C_3 = C_2 = H_2$	125.6	$\Gamma I A D I F A A$	90(2)
FeI = C2 = H2	123.0 107.1(2)	$ \begin{array}{ccc} \Gamma I A & \\ \hline \Gamma I A & $	101.0(9)
C4 = C3 = C2	107.1(2)	$\Gamma J A \longrightarrow D I \longrightarrow D D$	110.1(7)
C4 - C3 - Fel	(1.38(12))	FIA BI F2B	118.5(8)
$C_2 = C_3 = Fel$	09.24 (11) 126 4	$\Gamma J A = D I = \Gamma 2 D$	110.3(10)
C4 - C3 - H3	120.4	F4A - B1 - F2B	112.9 (11)
$C_2 - C_3 - H_3$	126.4	FIA BI F3B	121.9 (14)
FeI-C3-H3	126.4	F4A - B1 - F3B	104.0 (8)
	109.10(19)	$F_2B \longrightarrow B_1 \longrightarrow F_3B$	97.0 (10)
$C_2 = C_4 = F_{e1}$		FIA	109.0(8)
	69.50 (12) (0.81 (12)		1150(0)
	69.80 (12) 69.81 (12)	F3A—B1—F2A	115.0 (6)
C5-C4-H4	69.50 (12) 69.81 (12) 125.4	F3A—B1—F2A F4A—B1—F2A F2A	115.0 (6) 115.2 (10)
C5—C4—Fei C5—C4—H4 C3—C4—H4	69.50 (12) 69.81 (12) 125.4 125.4	F3A—B1—F2A F4A—B1—F2A F3B—B1—F2A	115.0 (6) 115.2 (10) 105.0 (7)

C4—C5—C1	107.8 (2)	F3A—B1—F4B	121.6 (11)
C4—C5—Fe1	71.71 (13)	F2B—B1—F4B	99.2 (10)
C1—C5—Fe1	69.35 (12)	F3B—B1—F4B	104.1 (10)
C4—C5—H5	126.1	F2A—B1—F4B	102.2 (8)
C1—C5—H5	126.1	F3A—B1—F1B	107.8 (14)
Fe1—C5—H5	126.1	F4A—B1—F1B	106.2 (9)
O1—C6—Fe1	173.88 (19)	F2B—B1—F1B	102.2 (7)
O2—C7—Fe1	175.25 (17)	F3B—B1—F1B	133.4 (8)
N3—C8—N1	112.50 (14)	F2A—B1—F1B	93.2 (6)
N3—C8—H8A	109.1	F4B—B1—F1B	113.5(10)
N1—C8—H8A	109.1	F6—B2—F8	111 51 (17)
N3—C8—H8B	109.1	F6-B2-F5	112.30(17)
N1—C8—H8B	109.1	F8—B2—F5	10844(17)
H8A - C8 - H8B	107.8	F6 = B2 = F7	110.39(15)
N3_C9_N4	111 56 (14)	F8—B2—F7	107 23 (17)
N3—C9—H9A	109.3	F5F7	106 73 (16)
N4 - C9 - H9A	109.3	C_{12} N1_C11	107.23(13)
N3_C9_H9B	109.3	C12 N1 $C8$	106.19(13)
N4_C9_H9B	109.3	C_{11} N_{1} C_{8}	106.19(13) 106.39(13)
$H_{0}A = C_{0} = H_{0}B$	109.5	$C12$ _N1_Fe1	112.67(10)
N2 - C10 - N4	111 52 (15)	C11 N1 Fe1	112.07(10) 112.30(10)
$N_2 - C_{10} - H_{10A}$	109.3	C8—N1—Fe1	112.50(10) 111.63(10)
N4-C10-H10A	109.3	C_11 N2 C_13	109.43(15)
$N_2 C_{10} H_{10}B$	109.3	$C_{11} = N_2 = C_{10}$	109.43(13) 108.47(14)
N/ C10 H10B	109.3	$C_{11} = N_2 = C_{10}$	108.47(14) 108.45(15)
$H_{10A} = C_{10} = H_{10B}$	109.5	C_{13} C_{23} C_{10} C_{23} C	108.43(13) 109.42(14)
$N_2 C_{11} N_1$	112 18 (14)	$C_8 = N_3 = C_7$	109.42(14) 108.63(15)
$N_2 = C_{11} = N_1$	112.18 (14)	$C_0 = N_3 = C_{13}$	108.03(15) 108.34(15)
N1 C11 H11A	109.2	$C_{12} N_{4} C_{9}$	108.54(15) 108.63(15)
$N_{1} = C_{11} = M_{11}R$	109.2	C_{12} N_4 C_{10}	108.03(13) 108.82(14)
N1 C11 H11P	109.2	C_{12} N_{4} C_{10}	108.82(14)
	109.2	$C_{21} N_{5} C_{25}$	106.48(14) 106.01(13)
M = C12 = N1	107.9 112 32 (14)	$C_{21} = N_{5} = C_{23}$	100.91(13) 107.17(13)
N4 = C12 = M1	112.32 (14)	$C_{21} = N_{3} = C_{24}$	107.17(13) 105.03(13)
N4 - C12 - H12A $N1 - C12 - H12A$	109.1	$C_{23} = N_{3} = C_{24}$	103.93(13)
NI-C12-III2A N4 C12 H12B	109.1	C_{21} N_{3} P_{22} C_{25} N_{5} E_{22}	111.19(10) 111.84(10)
N4 - C12 - H12B $N1 - C12 - H12B$	109.1	C_{23} N_{3} P_{22} C_{24} N_{5} E_{22}	111.64(10) 113.40(10)
H12A C12 H12B	107.0	$C_2 = N_3 = \Gamma_{C_2}$	113.40(10) 108 70(14)
$\frac{1112}{112} = \frac{112}{112} = \frac{1112}{112} = \frac{112}{112} $	107.9	$C_{21} = N_{0} = C_{20}$	108.70(14) 100.35(14)
$N_{2} = C_{13} = N_{2}$	100.3	$C_{21} = N_{0} = C_{22}$	109.55(14)
N2 C12 H12A	109.3	C_{20} NO C_{22}	108.03(14)
$N_2 = C_{13} = H_{13} P_{13}$	109.3	C_{23} $N/-C_{22}$	108.39(14) 100.26(14)
N2 C12 H12D	109.3	$C_{23} = N/ - C_{23}$	109.20(14) 108.20(14)
H12A C12 H12D	109.5	$C_{22} = 107 = C_{23}$	100.29(14) 108.68(14)
C18 C14 C15	107 45 (17)	C_{27} N8 C26	108.00(14)
$C_{10} = C_{14} = C_{13}$	71.86 (10)	$C_{24} = 100 - C_{20}$	100.02(14) 108.60(14)
$C_{10} - C_{14} - C_{2}$	60 15 (10)	$C_{23} = 10 = C_{20}$	03 05 (0)
C13 - C14 - 162	126.3	$C_{0} = C_{1} = C_{1}$	95.95 (9) 95.95 (9)
010-014-1114	120.3	UU-1'U1-INI	7J.UJ (0)

C15—C14—H14	126.3	C7—Fe1—N1	93.38 (7)
Fe2—C14—H14	126.3	C6—Fe1—C1	113.22 (9)
C16—C15—C14	108.27 (17)	C7—Fe1—C1	88.13 (8)
C16—C15—Fe2	70.30 (10)	N1—Fe1—C1	151.53 (7)
C14—C15—Fe2	70.96 (10)	C6—Fe1—C2	86.60 (9)
С16—С15—Н15	125.9	C7—Fe1—C2	119.82 (8)
C14—C15—H15	125.9	N1—Fe1—C2	146.62 (7)
Fe2—C15—H15	125.9	C1—Fe1—C2	39.56 (8)
C15—C16—C17	107.98 (17)	C6—Fe1—C5	151.87 (9)
C15—C16—Fe2	70.17 (10)	C7—Fe1—C5	93.38 (9)
C17—C16—Fe2	71.26 (10)	N1—Fe1—C5	111.58 (7)
C15—C16—H16	126	C1—Fe1—C5	39.99 (8)
C17—C16—H16	126	C2—Fe1—C5	66.26 (9)
Fe2—C16—H16	126	C6—Fe1—C3	98.24 (10)
C18 - C17 - C16	107.63 (17)	C7—Fe1—C3	154.68 (8)
C18—C17—Fe2	71.57 (11)	N1—Fe1—C3	107.47 (7)
$C16-C17-Fe^{2}$	68 98 (10)	C1—Fe1—C3	66 67 (8)
C18 - C17 - H17	126.2	C^2 —Fe1—C3	39 71 (8)
C16—C17—H17	126.2	C5—Fe1—C3	65 97 (9)
Fe2—C17—H17	126.2	C6—Fe1—C4	135.95(10)
C14-C18-C17	108.64 (17)	C7—Fe1—C4	129.04 (9)
$C14$ — $C18$ — Fe^2	69 27 (10)	N1—Fe1—C4	91 81 (7)
C17—C18—Fe2	69.57 (11)	C1—Fe1—C4	65.90 (8)
C14—C18—H18	125.7	C2—Fe1—C4	65.45 (8)
C17—C18—H18	125.7	C5—Fe1—C4	38.79 (9)
Fe2—C18—H18	125.7	C3—Fe1—C4	38.81 (9)
03-C19-Fe2	174.69 (17)	C19—Fe2—C20	94.22 (8)
04—C20—Fe2	174.77 (16)	C19—Fe2—N5	93.83 (7)
N6—C21—N5	111.92 (14)	C20—Fe2—N5	94.39 (7)
N6—C21—H21A	109.2	C19—Fe2—C15	86.20 (8)
N5—C21—H21A	109.2	C20—Fe2—C15	117.84 (8)
N6—C21—H21B	109.2	N5—Fe2—C15	147.71 (7)
N5—C21—H21B	109.2	C19—Fe2—C16	114.42 (8)
H21A—C21—H21B	107.9	C20—Fe2—C16	87.55 (8)
N7—C22—N6	111.47 (14)	N5—Fe2—C16	151.50(7)
N7—C22—H22A	109.3	C15—Fe2—C16	39.53 (7)
N6—C22—H22A	109.3	C19—Fe2—C14	96.32 (8)
N7—C22—H22B	109.3	C20—Fe2—C14	154.12 (8)
N6—C22—H22B	109.3	N5—Fe2—C14	108.38 (6)
H22A—C22—H22B	108	C15—Fe2—C14	39.89 (7)
N7—C23—N8	111.49 (14)	C16—Fe2—C14	66.57 (7)
N7—C23—H23A	109.3	C19—Fe2—C17	152.07 (8)
N8—C23—H23A	109.3	C20—Fe2—C17	94.59 (8)
N7—C23—H23B	109.3	N5—Fe2—C17	111.83 (7)
N8—C23—H23B	109.3	C15—Fe2—C17	66.29 (8)
H23A—C23—H23B	108	C16—Fe2—C17	39.76 (8)
N8—C24—N5	112.23 (13)	C14—Fe2—C17	65.96 (7)
N8—C24—H24A	109.2	C19—Fe2—C18	133.73 (8)
			× /

N5—C24—H24A	109.2	C20—Fe2—C18	130.92 (8)
N8—C24—H24B	109.2	N5—Fe2—C18	92.38 (6)
N5—C24—H24B	109.2	C15—Fe2—C18	65.71 (7)
H24A—C24—H24B	107.9	C16—Fe2—C18	65.79 (7)
N7—C25—N5	112.53 (14)	C14—Fe2—C18	38.86 (7)
N7—C25—H25A	109.1	C17—Fe2—C18	38.86 (7)
C5—C1—C2—C3	-0.5 (2)	C3-C2-Fe1-C1	-119.0 (2)
Fe1—C1—C2—C3	60.88 (14)	C1—C2—Fe1—C5	38.58 (13)
C5-C1-C2-Fe1	-61.34 (13)	C3—C2—Fe1—C5	-80.39 (15)
C1—C2—C3—C4	1.4 (2)	C1—C2—Fe1—C3	119.0 (2)
Fe1—C2—C3—C4	61.71 (14)	C1-C2-Fe1-C4	81.25 (14)
C1-C2-C3-Fe1	-60.31 (14)	C3—C2—Fe1—C4	-37.72 (14)
C2—C3—C4—C5	-1.8 (2)	C4—C5—Fe1—C6	96.1 (2)
Fe1—C3—C4—C5	58.52 (14)	C1C5Fe1C6	-21.8 (3)
C2-C3-C4-Fe1	-60.33 (14)	C4—C5—Fe1—C7	-159.01 (13)
C3—C4—C5—C1	1.5 (2)	C1—C5—Fe1—C7	83.04 (13)
Fe1—C4—C5—C1	60.24 (14)	C4—C5—Fe1—N1	-64.02 (13)
C3—C4—C5—Fe1	-58.71 (15)	C1C5Fe1N1	178.02 (11)
C2—C1—C5—C4	-0.6 (2)	C4C5Fe1C1	117.95 (18)
Fe1—C1—C5—C4	-61.75 (14)	C4C5Fe1C2	79.79 (13)
C2-C1-C5-Fe1	61.10 (14)	C1	-38.17 (12)
C18—C14—C15—C16	1.3 (2)	C4—C5—Fe1—C3	36.18 (12)
Fe2-C14-C15-C16	-60.70 (13)	C1—C5—Fe1—C3	-81.77 (13)
C18—C14—C15—Fe2	62.03 (12)	C1C5Fe1C4	-117.95 (18)
C14—C15—C16—C17	-0.5 (2)	C4—C3—Fe1—C6	168.18 (14)
Fe2-C15-C16-C17	-61.57 (13)	C2—C3—Fe1—C6	-74.45 (15)
C14-C15-C16-Fe2	61.11 (13)	C4—C3—Fe1—C7	-73.9 (2)
C15—C16—C17—C18	-0.6 (2)	C2-C3-Fe1-C7	43.5 (3)
Fe2-C16-C17-C18	-61.48 (13)	C4—C3—Fe1—N1	70.21 (14)
C15-C16-C17-Fe2	60.88 (13)	C2—C3—Fe1—N1	-172.42 (13)
C15—C14—C18—C17	-1.7 (2)	C4—C3—Fe1—C1	-80.01 (14)
Fe2-C14-C18-C17	58.57 (13)	C2-C3-Fe1-C1	37.36 (14)
C15-C14-C18-Fe2	-60.29 (12)	C4—C3—Fe1—C2	-117.4 (2)
C16—C17—C18—C14	1.4 (2)	C4—C3—Fe1—C5	-36.17 (13)
Fe2-C17-C18-C14	-58.39 (13)	C2-C3-Fe1-C5	81.21 (15)
C16—C17—C18—Fe2	59.83 (13)	C2—C3—Fe1—C4	117.4 (2)
N4—C12—N1—C11	56.03 (18)	C5-C4-Fe1-C6	-137.60 (15)
N4—C12—N1—C8	-57.41 (18)	C3—C4—Fe1—C6	-16.95 (19)
N4-C12-N1-Fe1	-179.91 (11)	C5-C4-Fe1-C7	27.41 (17)
N2-C11-N1-C12	-56.77 (18)	C3—C4—Fe1—C7	148.06 (13)
N2-C11-N1-C8	56.53 (18)	C5—C4—Fe1—N1	123.24 (13)
N2-C11-N1-Fe1	178.94 (11)	C3—C4—Fe1—N1	-116.11 (13)
N3—C8—N1—C12	56.63 (18)	C5-C4-Fe1-C1	-38.46 (13)
N3—C8—N1—C11	-57.39 (18)	C3-C4-Fe1-C1	82.19 (14)
N3—C8—N1—Fe1	179.78 (12)	C5-C4-Fe1-C2	-82.06 (14)
N1-C11-N2-C13	-58.67 (19)	C3-C4-Fe1-C2	38.59 (13)
N1-C11-N2-C10	59.46 (19)	C3—C4—Fe1—C5	120.65 (18)

N3—C13—N2—C11	59.3 (2)	C5-C4-Fe1-C3	-120.65 (18)
N3—C13—N2—C10	-58.9 (2)	C21—N5—Fe2—C19	-66.78 (12)
N4—C10—N2—C11	-60.45 (19)	C25—N5—Fe2—C19	52.66 (12)
N4—C10—N2—C13	58.31 (19)	C24—N5—Fe2—C19	172.37 (12)
N1—C8—N3—C9	-58.50 (19)	C21—N5—Fe2—C20	-161.31 (12)
N1—C8—N3—C13	59.60 (19)	C25—N5—Fe2—C20	-41.87 (12)
N4—C9—N3—C8	58.99 (19)	C24—N5—Fe2—C20	77.84 (12)
N4—C9—N3—C13	-59.29 (19)	C21—N5—Fe2—C15	22.16 (18)
N2-C13-N3-C8	-59.4 (2)	C25—N5—Fe2—C15	141.60 (14)
N2—C13—N3—C9	59.4 (2)	C24—N5—Fe2—C15	-98.69(15)
N1—C12—N4—C9	59.75 (18)	C_{21} —N5—Fe2—C16	105.75 (16)
N1-C12-N4-C10	-58.17(19)	C_{25} N5—Fe2—C16	-134.81(15)
N_{3} C9 N_{4} C12	-59.39(19)	C_{24} N5—Fe2—C16	-151(2)
N_{3} C9 N_{4} C10	58 75 (19)	$C_{21} = N_{5} = F_{62} = C_{14}$	31.19(13)
N_{2} C_{10} N_{4} C_{12}	59.85 (19)	C_{25} N5 Fe2 C14	150.62(11)
$N_2 = C_{10} = N_4 = C_{12}$	-58.16(19)	$C_{23} = 103 = 102 = C_{14}$	-89.67(12)
$N_{6} = C_{21} = N_{5} = C_{25}$	56 37 (18)	$C_{24} = N_{5} = F_{62} = C_{14}$	101.96(12)
N6-C21-N5-C24	-56.85(17)	C_{25} N5 F_{e2} C_{17}	-13860(11)
$N6-C21-N5-Ee^2$	$178\ 70\ (11)$	$C_{23} = N_{3} = 162 = C_{17}$	-18.89(13)
N7 C25 N5 C21	-56.07(18)	$C_{24} = N_{5} = 162 = C_{17}$	67.34(12)
N7 - C25 - N5 - C24	57.09(17)	$C_{21} = N_{5} = 162 = C_{18}$	-173 22 (12)
N7 - C25 - N5 - Ee2	-17890(11)	$C_{23} = N_{3} = 162 = C_{18}$	-5351(12)
$N_{22} = N_{22} = N_{2} = N_{2} = N_{2}$	56 10 (18)	C_{16} C_{15} $E_{e^{2}}$ C_{18}	-137.02(13)
N8 C24 N5 C25	-57.77(17)	$C_{10} = C_{15} = 102 = C_{10}$	10457(12)
$N8 C24 N5 E_{2}2$	170.20(11)	$C_{14} = C_{15} = C_{2} = C_{19}$	-44.25(14)
N5 C21 N6 C26	50.81 (18)	C_{10} C_{15} C_{20} C	-162.66(11)
$N_{5} = C_{21} = N_{6} = C_{20}$	-59.66(19)	$C_{14} = C_{15} = C_{20} = C_{20}$	102.00(11) 121.82(12)
NS = C26 = N6 = C21	-50.00(18)	C10 - C15 - Fe2 - N5	131.03(13) 13.42(10)
$N_{0} = C_{20} = N_{0} = C_{21}$	-00.71(10)	C14 - C15 - Fe2 - N5	13.42(19)
$N_{0} = C_{20} = N_{0} = C_{22}$	50.60 (10)	C14 - C15 - Fe2 - C10	-118.41(17)
N = C22 = N6 = C21	59.09 (19)	C16 - C15 - Fe2 - C14	110.41(17)
N = C22 = N0 = C20	-58.81(19)	C16-C15-Fe2-C17	38.09 (12)
$N_{5} = C_{25} = N_{7} = C_{22}$	59.10 (19)	C14-C15-Fe2-C17	-80.32(12)
$N_{2} = C_{2} = N_{2} = C_{2}$	-58.82(18)	C16-C15-Fe2-C18	80.80 (12)
N6-C22-N/-C25	-59.46 (19)	C14-C15-Fe2-C18	-3/.61(11)
N6-C22-N/-C23	59.07 (18)	C15-C16-Fe2-C19	48.34 (14)
N8-C23-N/-C25	58.91 (19)	C17—C16—Fe2—C19	166.30 (11)
N8—C23—N/—C22	-59.20 (18)	C15—C16—Fe2—C20	141.86 (12)
N5—C24—N8—C23	59.99 (18)	C17—C16—Fe2—C20	-100.18 (12)
N5—C24—N8—C26	-58.10 (18)	C15—C16—Fe2—N5	-123.47 (15)
N7—C23—N8—C24	-59.41 (18)	C17—C16—Fe2—N5	-5.5 (2)
N7—C23—N8—C26	58.82 (18)	C17—C16—Fe2—C15	117.96 (16)
N6—C26—N8—C24	59.87 (18)	C15—C16—Fe2—C14	-37.94 (11)
N6-C26-N8-C23	-58.28 (19)	C17—C16—Fe2—C14	80.02 (12)
C12—N1—Fe1—C6	166.15 (12)	C15—C16—Fe2—C17	-117.96 (16)
C11—N1—Fe1—C6	-72.64 (13)	C15—C16—Fe2—C18	-80.58 (12)
C8—N1—Fe1—C6	46.76 (13)	C17—C16—Fe2—C18	37.38 (11)
C12—N1—Fe1—C7	71.87 (12)	C18—C14—Fe2—C19	166.14 (12)
C11—N1—Fe1—C7	-166.91 (12)	C15-C14-Fe2-C19	-76.31 (12)

C8—N1—Fe1—C7	-4752(12)	C18—C14—Fe2—C20	-804(2)
C12—N1—Fe1—C1	-204(2)	C_{15} C_{14} F_{e2} C_{20}	371(2)
C_{11} N1—Fe1—C1	100.77(17)	$C18 - C14 - Fe^2 - N5$	69.96(12)
C8—N1—Fe1—C1	-139.84(15)	C_{15} C_{14} F_{e2} N5	-17249(11)
C12 N1 Fe1 C2	$-102\ 37\ (16)$	$C18 - C14 - Fe^2 - C15$	-11755(16)
$C11 _ N1 _ Fe1 _ C2$	188(2)	$C18 - C14 - Fe^2 - C16$	-79.95(12)
C8 N1 $Ee1$ $C2$	138.24(15)	C_{15} C_{14} F_{e2} C_{16}	37 59 (11)
C12 N1 Fe1 C5	-23 11 (14)	$C18 - C14 - Fe^2 - C17$	-3635(11)
$C_{11} = N_1 = F_{c_1} = C_5$	98 10 (13)	$C_{15} - C_{14} - F_{e2} - C_{17}$	81 20 (12)
C8—N1—Fe1—C5	-14250(12)	$C_{15} = C_{14} = F_{e2} = C_{18}$	117.55(16)
C_1^2 N1 Eq. C_3^2	-93.56(13)	$C_{13} = C_{14} = 162 = C_{10}$	90.6(2)
C_{12} N_{1} E_{e1} C_{3}	95.50 (15) 27.65 (14)	$C_{16} - C_{17} - F_{e2} - C_{19}$	-274(2)
C_8 N1 Fe1 C3	147.05(12)	$C_{10} = C_{17} = 102 = C_{17}$	-161.38(12)
$C_{12} = N_1 = P_1 = C_2$	-57.41(13)	$C_{16} = C_{17} = C_{20} = C_{20}$	101.38(12) 80.58(12)
$C_{12} = N_1 = 1 C_1$	63 80 (13)	$C_{10} = C_{17} = 102 = 020$	-64.79(12)
$C_{1} = N_{1} = C_{1} = C_{4}$	-176.80(13)	$C_{16} = C_{17} = C_{2} = N_{5}$	177 17 (10)
C_{2} C_{1} E_{2} C_{4}	51.64.(15)	$C_{10} = C_{17} = C_{2} = C_{15}$	177.17(10) 80.16(12)
$C_2 - C_1 - F_{c1} - C_0$	168.00(13)	$C_{16} = C_{17} = C_{12} = C_{15}$	-37.88(11)
C_{2} C_{1} F_{e1} C_{7}	106.99(13) 145.14(13)	C18 C17 Fe2 C15	-37.88(11)
$C_2 = C_1 = P_1 = C_7$	-07.51(13)	$C_{10} = C_{17} = F_{22} = C_{10}$	110.04(10)
$C_{2} = C_{1} = C_{1} = C_{1}$	-97.51(15) -12121(16)	$C_{16} = C_{17} = F_{22} = C_{14}$	-81.68(11)
$C_2 = C_1 = F_{e_1} = N_1$	-121.21(10) -2.0(2)	C16 - C17 - Fe2 - C14	-81.08(12) -118.04(16)
$C_5 = C_1 = F_{e_1} = C_2$	-3.9(2)	C14 - C19 = Fe2 - C18	-118.04(10)
$C_3 = C_1 = F_{e_1} = C_2$	117.33(18) 117.25(18)	C17 - C18 - Fe2 - C19	-19.24(10)
C_2 — C_1 — F_{e1} — C_3	-117.33(18)	C17 - C18 - Fe2 - C19	-139.00(13)
C_2 — C_1 — F_{e_1} — C_3	-3/.49(13)	C14 - C18 - Fe2 - C20	145.27(12)
$C_3 = C_1 = F_1 = C_3$	/9.86 (14)	C17 - C18 - Fe2 - C20	24.91 (15)
C_2 — C_1 — F_{e1} — C_4	-80.03(14)	C14— $C18$ — $Fe2$ — $N5$	-116.84 (11)
C_{2} C_{1} C_{2} C_{1} C_{4}	37.32 (13)	C1/-C18-Fe2-N5	122.80 (11)
C1 - C2 - Fe1 - C6	-133.79 (14)	C14— $C18$ — $Fe2$ — $C15$	38.60 (11)
C3—C2—Fel—C6	107.23 (15)	C17—C18—Fe2—C15	-81.77 (12)
C1-C2-Fe1-C7	-41.18 (16)	C14—C18—Fe2—C16	82.13 (12)
C3—C2—Fe1—C7	-160.16 (14)	C17—C18—Fe2—C16	-38.23 (11)
C1—C2—Fe1—N1	132.19 (14)	C17—C18—Fe2—C14	-120.37 (16)
C3—C2—Fe1—N1	13.2 (2)	C14—C18—Fe2—C17	120.37 (16)