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### Tris(1,10-phenanthroline- $\kappa^2 N, N'$ )iron(II) bis[(1,10-phenanthroline- $\kappa^2 N, N'$ )tetrakis(thiocyanato- $\kappa N$ )chromate(III)] acetonitrile trisolvate monohydrate

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Key indicators: single-crystal X-ray study; T = 173 K; mean  $\sigma$ (C–C) = 0.007 Å; R factor = 0.051; wR factor = 0.135; data-to-parameter ratio = 15.9.

Single crystals of the title heterometallic compound,  $[Fe(C_{12}H_8N_2)_3][Cr(NCS)_4(C_{12}H_8N_2)]_2 \cdot 3CH_3CN \cdot H_2O$  or  $[Fe(Cphen)_3][Cr(NCS)_4(phen)]_2 \cdot 3CH_3CN \cdot H_2O$ , were prepared using the one-pot open-air reaction of iron powder, Reineckes salt and 1,10-phenanthroline (phen) in acetonitrile. The asymetric unit consists of an  $[Fe(phen)_3]^{2+}$  cation, two  $[Cr(phen)(NCS)_4]^-$  anions, three acetonitrile solvent molecules and a water molecule. The Fe and Cr atoms both show a slightly distorted octahedral FeN<sub>6</sub> and CrN<sub>6</sub> coordination geometry with adjacent angles in the range 79.67 (12)– 95.21 (12)°. No classical hydrogen bonding involving the water molecule is observed.

### **Related literature**

For background to direct synthesis, see: Makhankova (2011). For background to the use of Reineckes salt as a source of building blocks or metalloligands, see: Zhang *et al.* (2001); Cucos *et al.* (2006); Cherkasova & Gorunova (2003); Nikitina *et al.* (2009); Kolotilov *et al.* (2010). For Fe—N bond lengths in iron-phen derivatives, see: Alonso *et al.* (2005). For a related structure, see: Semenaka *et al.* (2011).



### Experimental

#### Crystal data

 $[Fe(C_{12}H_8N_2)_3][Cr(NCS)_{4^-} (C_{12}H_8N_2)]_2 \cdot 3C_2H_3N \cdot H_2O$  $M_r = 1666.69$ Triclinic,*P*I*a*= 12.641 (2) Å*b*= 16.681 (3) Å*c*= 20.692 (4) Å*a*= 111.514 (5)°

#### Data collection

Bruker APEXII CCD diffractometer Absorption correction: multi-scan (SADABS; Bruker, 2005) T<sub>min</sub> = 0.847, T<sub>max</sub> = 0.916

### Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.051$   $wR(F^2) = 0.135$  S = 0.9915519 reflections 974 parameters 3 restraints 
$$\begin{split} \beta &= 107.291 \ (6)^{\circ} \\ \gamma &= 92.231 \ (5)^{\circ} \\ V &= 3821.5 \ (13) \ \text{\AA}^3 \\ Z &= 2 \\ \text{Mo } K\alpha \text{ radiation} \\ \mu &= 0.75 \ \text{mm}^{-1} \\ T &= 173 \ \text{K} \\ 0.23 \ \times \ 0.22 \ \times \ 0.12 \ \text{mm} \end{split}$$

48046 measured reflections 15519 independent reflections 8993 reflections with  $I > 2\sigma(I)$  $R_{\text{int}} = 0.078$ 

H atoms treated by a mixture of independent and constrained refinement  $\Delta \rho_{max} = 0.43 \text{ e} \text{ Å}^{-3}$  $\Delta \rho_{min} = -0.44 \text{ e} \text{ Å}^{-3}$ 

Data collection: *APEX2* (Bruker, 2005); cell refinement: *SAINT* (Bruker, 2005); data reduction: *SAINT*; program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXS97* (Sheldrick, 2008); molecular graphics: *PLATON* (Spek, 2009); software used to prepare material for publication: *publCIF* (Westrip, 2010).

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: RU2031).

### References

- Alonso, C., Ballster, L., Gutierrez, F., Rerpinaqn, M. F., Sanchez, A. E. & Azcondo, M. T. (2005). Eur. J. Inorg. Chem. pp. 486–495.
- Bruker (2005). APEX2, SAINT and SADABS.. Bruker AXS Inc., Madison, Wisconsin, USA.
- Cherkasova, T. G. & Gorunova, I. P. (2003). Zh. Neorg. Khim. 48, 611-615.
- Cucos, A., Avarvari, N., Andruh, M., Journaux, Y., Muller, A. & Schmidtmann, M. (2006). Eur. J. Inorg. Chem. pp. 903–907.
- Kolotilov, S. V., Cador, O., Gavrilenko, K. S., Golhen, S., Ouahab, L. & Pavlishchuk, V. V. (2010). *Eur. J. Inorg. Chem.* 8, 1255–1266.
- Makhankova, V. G. (2011). Glob. J. Inorg. Chem. 2, 265–285.
- Nikitina, V. M., Nesterova, O. V., Kokozay, V. N., Dyakonenko, V. V., Shishkin, O. V. & Jezierska, J. (2009). *Polyhedron*, 28, 1265–1272.

Semenaka, V. V., Nesterova, O. V., Kokozay, V. N., Zybatyuk, R. I. & Shishkin, O. V. (2011). Acta Cryst. E67, m1021-m1022. Sheldrick, G. M. (2008). Acta Cryst. A64, 112-122. Spek, A. L. (2009). Acta Cryst. D65, 148-155.

Westrip, S. P. (2010). J. Appl. Cryst. 43, 920–925.Zhang, K.-L., Chen, W., Xu, Y., Wang, Z., Zhong, Z. J. & You, X.-Z. (2001).Polyhedron, 20, 2033–2036.

# supporting information

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### Tris(1,10-phenanthroline- $\kappa^2 N, N'$ )iron(II) bis[(1,10-phenanthroline- $\kappa^2 N, N'$ )tetrakis(thiocyanato- $\kappa N$ )chromate(III)] acetonitrile trisolvate monohydrate

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### S1. Comment

Recently we have reported that the Reineckes salt, (NH)<sub>4</sub>[Cr(NCS)<sub>4</sub>(NH<sub>3</sub>)<sub>2</sub>]H<sub>2</sub>O, could be exploited as a source of building blocks or metalloligands in the direct synthesis of heterometallic Cu/Cr and Co/Cr compounds with amines and Schiff-base ligands (Nikitina *et al.*, 2009; Semenaka *et al.*, 2011). In the present work, we report that the reaction of iron powder, Reineckes salt and 1,10-phenanthroline (phen) in acetonitrile solution has afforded a single crystals of the novel heterometallic Fe/Cr compound. The asymetric unit of title compound consists of slightly distorted octahedral [Fe(phen)<sub>3</sub>]<sup>2+</sup> cation and two [Cr(phen)(NCS)<sub>4</sub>]<sup>-</sup> anion blocks as well as solvate acetonitrile and water molecules (Fig. 1). In complex cation iron centers are in elongated octahedral coordination environment with six nitrogen atoms phen ligands. The bond lengths of Fe–N vary in the range 1,959 (3) – 1,980 (3) Å which is in the range usually found in other iron-phen derivatives (Alonso *et al.*, 2005). The *cis* and *trans* N–Fe–N bond angles vary from 82,27 (12)° to 95.21 (12)° and from 172.90 (12)° to 174.04 (11)°, respectively. The Cr(III) ions have N6 donor set formed by two N atoms from phen, which are replaced NCS groups in initial anions of Reineckes salt, and two NCS-groups in the equatorial plane and by two another NCS-groups at the axial positions. The axial Cr–N bond lengths are vary from 1,962 (3) to 2,077 (3) Å. The *cis* and *trans* N–Cr–N bond angles vary from 170,61 (12)° to 174,77 (12)°, respectively. The thiocyanate groups are almost linear, bond angles N–C–S are in a narrow range: from 178.1 (3) ° to 179.3 (4)°.

### S2. Experimental

Iron powder (0.07 g, 1.25 mmol), NH<sub>4</sub>[Cr(NCS)<sub>4</sub>(NH<sub>3</sub>)<sub>2</sub>]·H<sub>2</sub>O (0.443 g, 1.25 mmol), NH<sub>4</sub>NCS (0.190 g, 2.5 mmol), phen H<sub>2</sub>O (0.496 g, 2.5 mmol) and acetonitrile (15 ml) were heated to 50–60° and stirred magnetically until total dissolution of the iron was observed (4,5 h). The resulting red solution was slowly evaporated at room temperature until dark-red crystals suitable for crystallographic study were formed. The crystals were filtered off, washed with dry Pr<sup>i</sup>OH and finally dried *in vacuo* at room temperature. Yield: 0.25 g. IR (KBr, cm<sup>-1</sup>): 3048(sh), 3044(sh), 2314(w), 2066(*vs*), 1996(sh), 1645(sh), 1638(sh), 1635(*m*), 1599(*m*), 1578(*m*), 1554(sh), 1536(w), 1521(*m*), 1494(sh), 1472(sh), 1455(sh), 1424(*s*), 1409(sh), 1373(w), 1307(w), 1271(w), 1256(sh), 1223(sh), 1207(w), 1144(*m*), 1102(*m*), 1057(sh), 1039(sh), 990(*m*), 960(w), 942(sh), 915(sh), 876(w), 870(sh), 843(*s*), 798(*m*), 771(w), 737(sh), 719(*s*), 668(sh), 656(w), 620(w), 581(sh), 557(w), 626(w), 568(sh), 481(*m*), 451(sh), 433(w), 427(sh). The compound is sparingly soluble in dmso and dmf, insoluble in water and it is indefinitely stable in air.

### **S3. Refinement**

All non-hydrogen atoms were located from the initial solution and refined with anisotropic thermal parameters. The hydrogen atoms were positioned geometrically and included into refinement using riding model approximation with  $U_{iso}$ 



=  $nU_{eq}$  of non-hydrogen carrier atom (n = 1.5 for CH<sub>3</sub> groups and n = 1.2 for remaining H-atoms)

### Figure 1

Crystal structure of the complex, showing the atom numbering, with 50% probability displacement ellipsoids. Solvent molecules are omitted for clarity.

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Crystal data	
$[Fe(C_{12}H_8N_2)_3]$ $[Cr(NCS)_4(C_{12}H_8N_2)]_2 \cdot 3C_2H_3N \cdot H_2O$ $M_r = 1666.69$ Triclinic, $P\overline{1}$ $a = 12.641 (2) \text{ Å}$ $b = 16.681 (3) \text{ Å}$ $c = 20.692 (4) \text{ Å}$ $a = 111.514 (5)^{\circ}$ $\beta = 107.291 (6)^{\circ}$ $\gamma = 92.231 (5)^{\circ}$ $V = 3821.5 (13) \text{ Å}^3$	Z = 2 F(000) = 1704 $D_x = 1.448 \text{ Mg m}^{-3}$ Mo K $\alpha$ radiation, $\lambda = 0.71073 \text{ Å}$ Cell parameters from 4485 reflections $\theta = 2.3-21.7^{\circ}$ $\mu = 0.75 \text{ mm}^{-1}$ T = 173  K Block, red $0.23 \times 0.22 \times 0.12 \text{ mm}$
Data collection	
Bruker APEXII CCD diffractometer Radiation source: fine-focus sealed tube Graphite monochromator $\varphi$ and $\omega$ scans	Absorption correction: multi-scan (SADABS; Bruker, 2005) $T_{min} = 0.847$ , $T_{max} = 0.916$ 48046 measured reflections 15519 independent reflections 8993 reflections with $I > 2\sigma(I)$

$R_{\rm int} = 0.078$	$k = -20 \rightarrow 20$
$\theta_{\rm max} = 26.4^{\circ},  \theta_{\rm min} = 1.1^{\circ}$	$l = -25 \rightarrow 25$
$h = -15 \rightarrow 15$	

Refinement	
Refinement on $F^2$	Secondary atom site location: difference Fourier
Least-squares matrix: full	map
$R[F^2 > 2\sigma(F^2)] = 0.051$	Hydrogen site location: inferred from
$wR(F^2) = 0.135$	neighbouring sites
<i>S</i> = 0.99	H atoms treated by a mixture of independent
15519 reflections	and constrained refinement
974 parameters	$w = 1/[\sigma^2(F_o^2) + (0.0572P)^2 + 0.0054P]$
3 restraints	where $P = (F_o^2 + 2F_c^2)/3$
Primary atom site location: structure-invariant	$(\Delta/\sigma)_{\rm max} < 0.001$
direct methods	$\Delta \rho_{\rm max} = 0.43 \text{ e } \text{\AA}^{-3}$
	$\Delta \rho_{\rm min} = -0.44 \text{ e } \text{\AA}^{-3}$

### Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

	x	у	Z	$U_{ m iso}$ */ $U_{ m eq}$	
Crl	0.27228 (5)	0.11974 (4)	0.24479 (4)	0.03091 (17)	
Cr2	0.65438 (5)	0.31815 (4)	0.08754 (3)	0.02873 (16)	
Fe1	0.21655 (4)	0.67016 (4)	0.34300 (3)	0.02632 (14)	
<b>S</b> 1	0.27329 (12)	0.22111 (9)	0.49075 (7)	0.0579 (4)	
S2	0.09452 (10)	-0.17085 (8)	0.16961 (8)	0.0536 (3)	
S3	0.62676 (10)	0.06152 (8)	0.35925 (7)	0.0531 (3)	
S4	0.37743 (12)	0.41344 (8)	0.28415 (7)	0.0530 (3)	
S5	0.77068 (12)	0.50790 (9)	0.33991 (7)	0.0604 (4)	
S6	0.65109 (9)	0.07691 (8)	0.15795 (7)	0.0441 (3)	
S7	0.62707 (10)	0.59283 (8)	0.07321 (7)	0.0491 (3)	
<b>S</b> 8	1.02840 (9)	0.36578 (8)	0.08940 (7)	0.0451 (3)	
N1	0.2488 (3)	0.1575 (2)	0.3417 (2)	0.0376 (9)	
N2	0.2035 (3)	-0.0022 (2)	0.21591 (19)	0.0371 (9)	
N3	0.4240 (3)	0.0943 (2)	0.28350 (18)	0.0356 (8)	
N4	0.3298 (3)	0.2410 (2)	0.26495 (18)	0.0358 (8)	
N5	0.6900 (3)	0.3873 (2)	0.1943 (2)	0.0371 (9)	
N6	0.6551 (3)	0.2076 (2)	0.10439 (18)	0.0346 (8)	
N7	0.6422 (3)	0.4265 (2)	0.07093 (18)	0.0341 (8)	
N8	0.8136 (3)	0.3295 (2)	0.09225 (18)	0.0354 (8)	
N9	0.2783 (3)	0.0844 (2)	0.13939 (18)	0.0309 (8)	
N10	0.1155 (3)	0.1396 (2)	0.19199 (17)	0.0285 (7)	

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(Å^2)$ 

N11	0.6017 (3)	0.2448 (2)	-0.02542(17)	0.0300 (8)
N12	0.4819 (3)	0.2997 (2)	0.06400 (17)	0.0277 (7)
N13	0.3234 (3)	0.6688 (2)	0.43423 (17)	0.0318 (8)
N14	0.1557 (3)	0.5523 (2)	0.33057 (17)	0.0277 (7)
N15	0.3167 (3)	0.6249 (2)	0.28571 (18)	0.0304 (8)
N16	0.1125 (3)	0.6567(2)	0.24675 (18)	0.0303 (8)
N17	0 2766 (3)	0.7928(2)	0.36711(18)	0.0318 (8)
N18	0.1187(3)	0.7270(2)	0.39894(17)	0.0294 (8)
C1	0.2574(3)	0.1240(2) 0.1841(3)	0.39091(17) 0.4040(3)	0.0291(0)
C2	0.2574(3) 0.1576(3)	-0.0722(3)	0.1971 (2)	0.0305(10)
C2	0.1970(3)	0.0722(3)	0.1971(2) 0.3150(2)	0.0353(10)
C4	0.3093(3)	0.0004(3)	0.3130(2) 0.2722(2)	0.0304(0)
C4 C5	0.3402(3) 0.7241(3)	0.3134(3) 0.4291(3)	0.2722(2) 0.2550(3)	0.0304(9)
C5 C6	0.7241(3) 0.6516(3)	0.4381(3) 0.1528(3)	0.2330(3)	0.0339(10)
C0 C7	0.0310(3)	0.1328(3)	0.1204(2)	0.0298(9)
C/	0.0301(3)	0.4903(3)	0.0724(2)	0.0294(9)
C8	0.9035 (3)	0.3456 (3)	0.0913 (2)	0.0323 (10)
C9	0.3598 (3)	0.0550 (3)	0.1145 (2)	0.0423 (11)
H9	0.4260	0.0487	0.1478	0.051*
C10	0.3528 (4)	0.0328 (3)	0.0414 (3)	0.0476 (12)
H10	0.4130	0.0112	0.0254	0.057*
C11	0.2582 (4)	0.0423 (3)	-0.0073(2)	0.0411 (11)
H11	0.2530	0.0281	-0.0572	0.049*
C12	0.1700 (3)	0.0730 (3)	0.0169 (2)	0.0346 (10)
C13	0.1840 (3)	0.0932 (2)	0.0913 (2)	0.0301 (9)
C14	0.0672 (4)	0.0842 (3)	-0.0288 (2)	0.0390 (11)
H14	0.0572	0.0716	-0.0792	0.047*
C15	-0.0159 (3)	0.1123 (3)	-0.0024 (2)	0.0382 (11)
H15	-0.0832	0.1192	-0.0343	0.046*
C16	-0.0044 (3)	0.1321 (2)	0.0735 (2)	0.0315 (10)
C17	0.0967 (3)	0.1231 (2)	0.1195 (2)	0.0279 (9)
C18	-0.0874 (3)	0.1580 (3)	0.1043 (2)	0.0362 (10)
H18	-0.1578	0.1636	0.0746	0.043*
C19	-0.0685 (3)	0.1754 (3)	0.1769 (2)	0.0379 (10)
H19	-0.1248	0.1944	0.1982	0.045*
C20	0.0349 (3)	0.1652 (2)	0.2197 (2)	0.0344 (10)
H20	0.0475	0.1769	0.2702	0.041*
C21	0.6622 (4)	0.2196 (3)	-0.0695(2)	0.0428 (11)
H21	0 7415	0.2367	-0.0487	0.051*
C22	0.6150 (4)	0.1688(3)	-0.1451(3)	0.0525(13)
H22	0.6616	0.1519	-0.1747	0.063*
C23	0.5010(4)	0.1319 0.1438(3)	-0.1760(3)	0.003 0.0482(12)
U23 H23	0.3010 (4)	0.1438 (3)	-0.2271	0.058*
C24	0.4079 0.4338(A)	0.1079 0.1714 (3)	-0.1322(2)	0.0360 (10)
C25	0.4875(2)	0.1717(3)	-0.0566(2)	0.0300 (10)
C25	0.7073(3)	0.2212(2) 0.1526(2)	-0.1504(2)	0.0200(9)
U20 U26	0.3133 (4)	0.1520 (5)	-0.2102	0.0413 (11)
п20 С27	0.2737	0.11/0	-0.2102	$0.030^{*}$
U27	0.2326 (4)	0.1829 (3)	-0.1146(2)	0.0392 (11)
H2/	0.1729	0.1705	-0.134/	0.04/*

C28	0.3064 (3)	0.2338 (2)	-0.0370(2)	0.0311 (9)
C29	0.4245 (3)	0.2515 (2)	-0.0088(2)	0.0263 (9)
C30	0.2486 (3)	0.2690 (3)	0.0123 (2)	0.0359 (10)
H30	0.1688	0.2601	-0.0049	0.043*
C31	0.3074 (3)	0.3161 (3)	0.0850(2)	0.0388 (11)
H31	0.2687	0.3394	0.1190	0.047*
C32	0.4244 (3)	0.3298 (3)	0.1094 (2)	0.0343 (10)
H32	0.4643	0.3619	0.1604	0.041*
C33	0.4073 (3)	0.7303 (3)	0.4874 (2)	0.0407 (11)
H33	0.4205	0.7846	0.4835	0.049*
C34	0.4762 (4)	0.7181 (3)	0.5483(2)	0.0498 (13)
H34	0.5352	0.7634	0.5849	0.060*
C35	0.4589 (4)	0.6411 (4)	0.5554 (2)	0.0526 (13)
H35	0.5064	0.6325	0.5966	0.063*
C36	0.3710 (4)	0.5746 (3)	0.5017(2)	0.0428 (11)
C37	0.3056(3)	0.5923(3)	0.4424(2)	0.0316(9)
C38	0.3420(4)	0.4927(3)	0.1121(2) 0.5040(3)	0.0510(3)
H38	0.3865	0.4796	0.5436	0.062*
C39	0.2537(5)	0.4335(3)	0.4520(3)	0.0540(13)
H39	0.2361	0 3799	0.4558	0.065*
C40	0.1863 (4)	0.4501(3)	0.3911 (2)	0.0407 (11)
C41	0.2133(3)	0.5289(3)	0.3860(2)	0.0304 (9)
C42	0.0900 (4)	0.3932(3)	0.3352(3)	0.0492(13)
H42	0.0659	0.3392	0.3362	0.059*
C43	0.0321 (4)	0.4165 (3)	0.2800 (2)	0.0456 (12)
H43	-0.0332	0.3787	0.2424	0.055*
C44	0.0675 (4)	0.4948 (3)	0.2780(2)	0.0372 (10)
H44	0.0272	0.5081	0.2376	0.045*
C45	0.4222 (3)	0.6122 (3)	0.3077 (3)	0.0388 (11)
H45	0.4587	0.6254	0.3585	0.047*
C46	0.4818 (4)	0.5801 (3)	0.2591 (3)	0.0531 (14)
H46	0.5564	0.5702	0.2768	0.064*
C47	0.4325 (5)	0.5629 (3)	0.1860 (3)	0.0582 (15)
H47	0.4731	0.5422	0.1528	0.070*
C48	0.3220 (4)	0.5761 (3)	0.1604 (3)	0.0462 (12)
C49	0.2676 (4)	0.6073 (2)	0.2123 (2)	0.0326 (10)
C50	0.2600 (6)	0.5605 (3)	0.0852 (3)	0.0634 (16)
H50	0.2954	0.5399	0.0489	0.076*
C51	0.1544 (6)	0.5741 (3)	0.0648 (3)	0.0615 (16)
H51	0.1162	0.5625	0.0145	0.074*
C52	0.0969 (5)	0.6058 (3)	0.1170 (2)	0.0466 (12)
C53	0.1562 (4)	0.6232 (2)	0.1911 (2)	0.0347 (10)
C54	-0.0145 (5)	0.6198 (3)	0.1000 (3)	0.0519 (14)
H54	-0.0592	0.6069	0.0504	0.062*
C55	-0.0581 (4)	0.6523 (3)	0.1554 (3)	0.0479 (12)
Н55	-0.1337	0.6622	0.1444	0.057*
C56	0.0075 (3)	0.6712 (3)	0.2281 (2)	0.0383 (11)
Н56	-0.0243	0.6954	0.2659	0.046*

C57	0.3560 (4)	0.8248 (3)	0.3485 (3)	0.0436 (11)	
H57	0.3877	0.7853	0.3159	0.052*	
C58	0.3943 (4)	0.9148 (3)	0.3754 (3)	0.0540 (13)	
H58	0.4510	0.9353	0.3610	0.065*	
C59	0.3506 (4)	0.9725 (3)	0.4218 (3)	0.0509 (13)	
H59	0.3770	1.0334	0.4402	0.061*	
C60	0.2657 (3)	0.9420 (3)	0.4428 (2)	0.0377 (10)	
C61	0.2327 (3)	0.8515 (3)	0.4135 (2)	0.0310 (9)	
C62	0.2158 (4)	0.9964 (3)	0.4924 (2)	0.0450 (12)	
H62	0.2395	1.0579	0.5135	0.054*	
C63	0.1353 (4)	0.9622 (3)	0.5098 (2)	0.0428 (11)	
H63	0.1036	0.9999	0.5434	0.051*	
C64	0.0968 (3)	0.8696 (3)	0.4785 (2)	0.0350 (10)	
C65	0.1474 (3)	0.8161 (3)	0.4315 (2)	0.0304 (9)	
C66	0.0108 (4)	0.8297 (3)	0.4916 (2)	0.0458 (12)	
H66	-0.0265	0.8639	0.5230	0.055*	
C67	-0.0190 (4)	0.7413 (3)	0.4589 (2)	0.0450 (12)	
H67	-0.0775	0.7135	0.4673	0.054*	
C68	0.0361 (3)	0.6915 (3)	0.4129 (2)	0.0379 (10)	
H68	0.0141	0.6298	0.3907	0.045*	
N21	0.9342 (4)	0.8805 (3)	0.3236 (3)	0.0737 (14)	
C70	0.6627 (4)	0.7663 (3)	0.3096 (3)	0.0519 (13)	
N20	0.6003 (4)	0.8084 (3)	0.3261 (3)	0.0895 (17)	
N19	0.9140 (5)	0.2258 (4)	0.3444 (3)	0.0921 (18)	
C69	0.7423 (4)	0.7123 (3)	0.2876 (3)	0.0703 (16)	
H69A	0.7475	0.6677	0.3082	0.106*	
H69B	0.8162	0.7487	0.3059	0.106*	
H69C	0.7175	0.6839	0.2336	0.106*	
C74	0.8294 (6)	0.2449 (4)	0.3437 (3)	0.078 (2)	
C75	0.7198 (6)	0.2697 (4)	0.3412 (4)	0.105 (3)	
H75A	0.6719	0.2521	0.2898	0.158*	
H75B	0.7285	0.3332	0.3672	0.158*	
H75C	0.6851	0.2405	0.3651	0.158*	
C78	0.9856 (6)	1.0175 (4)	0.3033 (3)	0.105 (3)	
H78A	1.0594	1.0493	0.3388	0.158*	
H78B	0.9288	1.0552	0.3099	0.158*	
H78C	0.9876	1.0002	0.2530	0.158*	
C77	0.9574 (4)	0.9401 (4)	0.3151 (3)	0.0577 (15)	
01	0.0464 (10)	0.5593 (6)	0.5096 (4)	0.250 (5)	
H1O	0.065 (13)	0.589 (9)	0.5548 (17)	0.376*	
H2O	-0.001 (11)	0.585 (10)	0.490 (7)	0.376*	

Atomic displacement parameters  $(Å^2)$ 

	$U^{11}$	$U^{22}$	$U^{33}$	$U^{12}$	$U^{13}$	$U^{23}$
Crl	0.0235 (3)	0.0264 (4)	0.0375 (4)	0.0009 (3)	0.0060 (3)	0.0105 (3)
Cr2	0.0239 (3)	0.0303 (4)	0.0328 (4)	0.0069 (3)	0.0082 (3)	0.0142 (3)
Fe1	0.0257 (3)	0.0230 (3)	0.0286 (3)	0.0021 (2)	0.0103 (3)	0.0076 (3)

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S1	0.0837 (10)	0.0521 (9)	0.0546 (8)	0.0133 (7)	0.0436 (8)	0.0232 (7)
S2	0.0506 (8)	0.0322 (7)	0.0728 (9)	-0.0058 (6)	0.0107 (7)	0.0243 (7)
S3	0.0345 (7)	0.0514 (8)	0.0649 (9)	0.0073 (6)	-0.0027 (6)	0.0289 (7)
S4	0.0887 (10)	0.0291 (7)	0.0478 (8)	0.0071 (6)	0.0297 (7)	0.0174 (6)
S5	0.0675 (9)	0.0559 (9)	0.0355 (7)	0.0033 (7)	0.0024 (6)	0.0060 (7)
S6	0.0362 (6)	0.0504 (8)	0.0618 (8)	0.0098 (5)	0.0209 (6)	0.0363 (7)
S7	0.0433 (7)	0.0339 (7)	0.0687 (9)	0.0040 (5)	0.0086 (6)	0.0272 (7)
S8	0.0311 (6)	0.0551 (8)	0.0519 (7)	0.0036 (5)	0.0177 (6)	0.0217 (6)
N1	0.033 (2)	0.036 (2)	0.037 (2)	0.0016 (16)	0.0077 (18)	0.0109 (19)
N2	0.031 (2)	0.030 (2)	0.046 (2)	0.0031 (16)	0.0094 (17)	0.0133 (19)
N3	0.029 (2)	0.034 (2)	0.035 (2)	0.0020 (16)	0.0022 (17)	0.0109 (18)
N4	0.0296 (19)	0.031 (2)	0.039 (2)	-0.0029 (16)	0.0026 (16)	0.0126 (18)
N5	0.036 (2)	0.038 (2)	0.034 (2)	0.0043 (17)	0.0089 (18)	0.0132 (19)
N6	0.0309 (19)	0.034 (2)	0.043 (2)	0.0087 (16)	0.0124 (17)	0.0190 (19)
N7	0.0314 (19)	0.036 (2)	0.034 (2)	0.0055 (16)	0.0067 (16)	0.0164 (18)
N8	0.0265 (19)	0.035 (2)	0.043 (2)	0.0063 (16)	0.0072 (17)	0.0175 (18)
N9	0.0203 (17)	0.030 (2)	0.038 (2)	0.0013 (15)	0.0074 (16)	0.0109 (17)
N10	0.0224 (17)	0.0243 (19)	0.034 (2)	0.0016 (14)	0.0069 (15)	0.0082 (16)
N11	0.0310 (19)	0.030 (2)	0.034 (2)	0.0117 (15)	0.0126 (16)	0.0151 (17)
N12	0.0289 (18)	0.0254 (19)	0.031 (2)	0.0070 (15)	0.0108 (16)	0.0124 (16)
N13	0.0271 (18)	0.030 (2)	0.032 (2)	0.0050 (15)	0.0102 (16)	0.0053 (17)
N14	0.0282 (18)	0.0273 (19)	0.0263 (18)	0.0027 (15)	0.0106 (15)	0.0081 (16)
N15	0.035 (2)	0.0222 (19)	0.039 (2)	0.0055 (15)	0.0183 (17)	0.0126 (17)
N16	0.035 (2)	0.0231 (19)	0.036 (2)	0.0023 (15)	0.0148 (17)	0.0134 (16)
N17	0.0312 (19)	0.0223 (19)	0.039 (2)	0.0005 (15)	0.0130 (17)	0.0078 (17)
N18	0.0296 (18)	0.033 (2)	0.0282 (19)	0.0064 (15)	0.0106 (15)	0.0138 (17)
C1	0.030 (2)	0.028 (2)	0.053 (3)	0.0021 (19)	0.017 (2)	0.016 (2)
C2	0.029 (2)	0.032 (3)	0.040 (3)	0.0062 (19)	0.009 (2)	0.017 (2)
C3	0.032 (2)	0.034 (3)	0.036 (3)	-0.003 (2)	0.005 (2)	0.013 (2)
C4	0.033 (2)	0.031 (3)	0.025 (2)	0.0026 (19)	0.0085 (18)	0.010 (2)
C5	0.031 (2)	0.036 (3)	0.044 (3)	0.008 (2)	0.010(2)	0.021 (2)
C6	0.020 (2)	0.035 (3)	0.030 (2)	0.0070 (18)	0.0094 (18)	0.007 (2)
C7	0.020 (2)	0.038 (3)	0.029 (2)	0.0034 (18)	0.0046 (18)	0.016 (2)
C8	0.031 (2)	0.030 (2)	0.032 (2)	0.0085 (19)	0.0026 (19)	0.014 (2)
C9	0.026 (2)	0.048 (3)	0.047 (3)	0.006 (2)	0.010(2)	0.014 (2)
C10	0.037 (3)	0.054 (3)	0.050 (3)	0.009 (2)	0.020 (2)	0.014 (3)
C11	0.041 (3)	0.037 (3)	0.042 (3)	0.000 (2)	0.016 (2)	0.010(2)
C12	0.035 (2)	0.024 (2)	0.038 (3)	-0.0030 (19)	0.011 (2)	0.007 (2)
C13	0.024 (2)	0.022 (2)	0.037 (2)	-0.0023 (17)	0.0084 (19)	0.007 (2)
C14	0.042 (3)	0.033 (3)	0.038 (3)	-0.001 (2)	0.008 (2)	0.015 (2)
C15	0.033 (2)	0.034 (3)	0.047 (3)	0.004 (2)	0.004 (2)	0.023 (2)
C16	0.027 (2)	0.021 (2)	0.041 (3)	-0.0006 (17)	0.0040 (19)	0.012 (2)
C17	0.023 (2)	0.019 (2)	0.037 (2)	0.0018 (16)	0.0060 (18)	0.0090 (19)
C18	0.023 (2)	0.030 (3)	0.052 (3)	0.0047 (18)	0.005 (2)	0.018 (2)
C19	0.026 (2)	0.033 (3)	0.051 (3)	0.0045 (19)	0.014 (2)	0.011 (2)
C20	0.031 (2)	0.027 (2)	0.042 (3)	0.0032 (18)	0.013 (2)	0.008 (2)
C21	0.037 (3)	0.052 (3)	0.044 (3)	0.018 (2)	0.019 (2)	0.018 (3)
C22	0.053 (3)	0.069 (4)	0.040 (3)	0.027 (3)	0.026 (3)	0.017 (3)

C23	0.059 (3)	0.044 (3)	0.033 (3)	0.015 (2)	0.015 (2)	0.006 (2)
C24	0.042 (3)	0.031 (3)	0.032 (3)	0.007 (2)	0.009 (2)	0.012 (2)
C25	0.031 (2)	0.023 (2)	0.033 (2)	0.0071 (18)	0.0100 (19)	0.012 (2)
C26	0.045 (3)	0.028 (3)	0.035 (3)	0.002 (2)	0.000 (2)	0.007 (2)
C27	0.031 (2)	0.031 (3)	0.046 (3)	-0.0037 (19)	0.001 (2)	0.015 (2)
C28	0.029 (2)	0.023 (2)	0.040 (3)	0.0028 (18)	0.008 (2)	0.015 (2)
C29	0.029 (2)	0.020 (2)	0.030 (2)	0.0035 (17)	0.0094 (19)	0.0111 (19)
C30	0.023 (2)	0.033 (3)	0.049 (3)	0.0005 (19)	0.009 (2)	0.017 (2)
C31	0.032 (2)	0.042 (3)	0.052 (3)	0.012 (2)	0.024 (2)	0.022(2)
C32	0.032 (2)	0.036 (3)	0.033 (2)	0.0055 (19)	0.013 (2)	0.011 (2)
C33	0.027(2)	0.039 (3)	0.041 (3)	-0.003(2)	0.007 (2)	0.003 (2)
C34	0.029(3)	0.063 (4)	0.032(3)	0.001 (2)	0.001(2)	-0.001(3)
C35	0.039(3)	0.082(4)	0.030(3)	0.022(3)	0.009(2)	0.016(3)
C36	0.039(3)	0.002(1) 0.055(3)	0.033(3)	0.022(3)	0.003(2)	0.010(3)
C37	0.031(2)	0.033(3)	0.033(3)	0.019(2)	0.012(2)	0.011(2)
C38	0.051(2) 0.061(3)	0.055(3)	0.031(2) 0.045(3)	0.033(3)	0.020(3)	0.035(3)
C39	0.001(3) 0.072(4)	0.001(1)	0.019(3) 0.054(3)	0.025(3)	0.020(3)	0.032(3)
C40	0.072(4) 0.059(3)	0.031(3)	0.034(3)	0.020(3)	0.027(3)	0.032(3)
C40	0.039(3)	0.030(3)	0.030(3)	0.013(2) 0.0047(19)	0.023(2)	0.017(2)
C42	0.034(2)	0.030(2)	0.027(2)	-0.003(2)	0.015 + (17)	0.012(2)
C43	0.070(3)	0.031(3) 0.034(3)	0.047(3) 0.033(3)	-0.011(2)	0.023(3)	0.012(2)
C44	0.038(3)	0.034(3)	0.033(3)	-0.005(2)	0.000(2)	0.003(2)
C45	0.036(3)	0.029(3)	0.052(2)	0.000(2)	0.009(2)	0.007(2)
C46	0.050(3)	0.020(2)	0.001(3)	0.0009(19)	0.027(2) 0.048(3)	0.010(2)
C40	0.031(3)	0.031(3)	0.094(4)	0.015(2)	0.048(3) 0.067(4)	0.023(3)
C48	0.060(4)	0.023(3)	0.000(4)	0.011(3)	0.007(4)	0.017(3)
C40	0.000(3)	0.027(3)	0.039(3)	0.004(2)	0.041(3)	0.012(2)
C50	0.049(5)	0.013(2)	0.055(3)	0.0052(1))	0.020(2)	0.0004(1))
C51	0.100(5)	0.043(3)	0.035(4)	0.011(3)	0.033(4)	0.017(3)
C52	0.110(3)	0.032(3)	0.035(3)	-0.002(3)	0.032(3)	0.007(2)
C52	0.075(4)	0.021(2)	0.031(3)	0.003(2)	0.012(3)	0.007(2)
C54	0.031(3) 0.076(4)	0.020(2) 0.027(3)	0.035(3)	-0.011(2)	-0.009(2)	0.009(2)
C55	0.070(4)	0.027(3)	0.051(3)	-0.001(2)	-0.009(3)	0.011(2)
C56	0.030(3)	0.038(3)	0.030(3)	0.001(2)	0.001(3)	0.020(3)
C50	0.033(3)	0.038(3)	0.041(3)	0.004(2)	0.008(2)	0.018(2)
C58	0.043(3)	0.030(3)	0.004(3)	0.000(2)	0.030(2)	0.010(2)
C50	0.052(3)	0.039(3)	0.078(4)	0.000(2)	0.030(3)	0.025(3)
C59	0.031(3)	0.024(3)	0.073(4)	0.003(2)	0.020(3)	0.013(3)
C00	0.030(2)	0.027(3)	0.043(3)	0.007(2)	0.009(2)	0.010(2)
C61	0.031(2)	0.020(2)	0.035(2)	0.0090(18)	0.0009(19)	0.011(2)
C62	0.040(3)	0.024(3)	0.043(3)	0.011(2)	0.004(2)	0.001(2)
C05	0.040(3)	0.039(3)	0.033(3)	0.019(2)	0.011(2)	0.003(2)
C04	0.034(2)	0.039(3)	0.031(2)	0.010(2)	0.012(2)	0.012(2)
C03	0.050(2)	0.028(2)	0.031(2)	0.0009 (18)	0.0005(19)	0.012(2)
C00	0.051(3)	0.051(3)	0.039(3)	0.022(2)	0.025(2)	0.014(3)
	0.045(3)	0.055(3)	0.051(3)	0.015(2)	0.031(2)	0.024(3)
C68	0.039 (3)	0.03/(3)	0.041(3)	0.007(2)	0.020(2)	0.015(2)
INZ I	0.066(3)	0.083(4)	0.068(3)	-0.011(3)	0.011(3)	0.030(3)
C/0	0.042 (3)	0.050 (3)	0.065 (4)	0.000 (3)	0.014 (3)	0.030(3)

## supporting information

0.083 (4)	0.079 (4)	0.135 (5)	0.030 (3)	0.064 (4)	0.050 (4)
0.100 (5)	0.093 (4)	0.077 (4)	0.000 (4)	0.052 (4)	0.011 (3)
0.049 (3)	0.068 (4)	0.098 (5)	0.004 (3)	0.023 (3)	0.039 (4)
0.106 (6)	0.053 (4)	0.079 (4)	-0.007 (4)	0.065 (5)	0.006 (3)
0.132 (6)	0.056 (4)	0.161 (7)	0.021 (4)	0.109 (6)	0.032 (4)
0.165 (7)	0.057 (4)	0.101 (5)	-0.020 (4)	0.084 (5)	0.011 (4)
0.053 (3)	0.069 (4)	0.034 (3)	-0.014 (3)	0.013 (2)	0.005 (3)
0.305 (13)	0.339 (13)	0.093 (5)	0.207 (11)	0.040 (7)	0.076 (9)
	0.083 (4) 0.100 (5) 0.049 (3) 0.106 (6) 0.132 (6) 0.165 (7) 0.053 (3) 0.305 (13)	0.083 (4)0.079 (4)0.100 (5)0.093 (4)0.049 (3)0.068 (4)0.106 (6)0.053 (4)0.132 (6)0.056 (4)0.165 (7)0.057 (4)0.053 (3)0.069 (4)0.305 (13)0.339 (13)	0.083 (4)0.079 (4)0.135 (5)0.100 (5)0.093 (4)0.077 (4)0.049 (3)0.068 (4)0.098 (5)0.106 (6)0.053 (4)0.079 (4)0.132 (6)0.056 (4)0.161 (7)0.165 (7)0.057 (4)0.101 (5)0.053 (3)0.069 (4)0.034 (3)0.305 (13)0.339 (13)0.093 (5)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

Geometric parameters (Å, °)

Cr1—N4	1.969 (3)	C27—H27	0.9500
Cr1—N3	1.975 (3)	C28—C30	1.398 (5)
Cr1—N2	1.978 (4)	C28—C29	1.407 (5)
Cr1—N1	1.986 (4)	C30—C31	1.363 (6)
Cr1—N10	2.064 (3)	C30—H30	0.9500
Cr1—N9	2.066 (3)	C31—C32	1.393 (5)
Cr2—N7	1.963 (3)	C31—H31	0.9500
Cr2—N5	1.977 (4)	C32—H32	0.9500
Cr2—N8	1.984 (3)	C33—C34	1.392 (6)
Cr2—N6	1.999 (3)	С33—Н33	0.9500
Cr2—N12	2.071 (3)	C34—C35	1.361 (6)
Cr2—N11	2.078 (3)	C34—H34	0.9500
Fel—N16	1.959 (3)	C35—C36	1.402 (6)
Fel—N15	1.972 (3)	C35—H35	0.9500
Fe1—N13	1.976 (3)	C36—C37	1.399 (5)
Fel—N18	1.977 (3)	C36—C38	1.423 (6)
Fe1—N17	1.978 (3)	C37—C41	1.425 (5)
Fel—N14	1.978 (3)	C38—C39	1.342 (6)
S1—C1	1.615 (5)	C38—H38	0.9500
S2—C2	1.616 (4)	C39—C40	1.424 (6)
S3—C3	1.608 (4)	С39—Н39	0.9500
S4—C4	1.606 (4)	C40—C41	1.395 (5)
S5—C5	1.619 (5)	C40—C42	1.410 (6)
S6—C6	1.623 (4)	C42—C43	1.357 (6)
S7—C7	1.612 (4)	C42—H42	0.9500
S8—C8	1.616 (4)	C43—C44	1.382 (5)
N1—C1	1.168 (5)	C43—H43	0.9500
N2—C2	1.153 (5)	C44—H44	0.9500
N3—C3	1.163 (5)	C45—C46	1.397 (6)
N4—C4	1.166 (5)	C45—H45	0.9500
N5—C5	1.163 (5)	C46—C47	1.366 (7)
N6—C6	1.166 (5)	C46—H46	0.9500
N7—C7	1.160 (5)	C47—C48	1.396 (7)
N8—C8	1.166 (5)	C47—H47	0.9500
N9—C9	1.318 (5)	C48—C49	1.398 (6)
N9—C13	1.359 (5)	C48—C50	1.437 (7)
N10-C20	1.324 (5)	C49—C53	1.412 (6)

N10—C17	1.364 (5)	C50—C51	1.330(7)
N11—C21	1.324 (5)	С50—Н50	0.9500
N11—C25	1.368 (5)	C51—C52	1.432 (7)
N12—C32	1.324 (5)	C51—H51	0.9500
N12—C29	1.364 (5)	C52—C54	1.397 (7)
N13—C33	1.335 (5)	C52—C53	1.403 (6)
N13—C37	1.366 (5)	C54—C55	1.362 (6)
N14—C44	1.334 (5)	C54—H54	0.9500
N14—C41	1 361 (5)	C55—C56	1 394 (6)
N15-C45	1.301(5) 1.327(5)	C55—H55	0.9500
N15-C49	1.370(5)	С56—Н56	0.9500
N16-C56	1.370(5)	C57 - C58	1 403 (6)
N16-C53	1.327(5)	C57—H57	0.9500
N17-C57	1.370(5) 1.334(5)	$C_{58}$ $C_{59}$	1 354 (6)
N17-C61	1.363 (5)	C58—H58	0.9500
N18-C68	1.305(5) 1.335(5)	$C_{50}$ $C_{60}$	1 412 (6)
N18 C65	1.355(5)	C59 H59	0.9500
$C_{0}$ $C_{10}$	1.308 (5)	$C_{59} = 1159$	1 396 (5)
С9—С10 С9—Н0	0.0500	$C_{60}$ $C_{62}$	1.390(3) 1.421(6)
$C_{9}$	0.9300	$C_{00} = C_{02}$	1.421(0)
C10_U10	0.0500	$C_{01} = C_{03}$	1.413(3) 1.348(6)
$C_{11}$ $C_{12}$	1 305 (6)	$C_{02} = C_{03}$	0.0500
C11_H11	0.0500	$C_{02}$ $C_{62}$ $C_{64}$	1.425(6)
	0.9300	$C_{03} = C_{04}$	1.433 (0)
C12-C13	1.403(3)	C03-H03	0.9300
C12 - C14	1.427(0) 1.422(5)	C64 - C65	1.390 (3)
C13 - C17	1.422(3)	C04-C00	1.390 (0)
	1.347 (0)		1.358 (6)
C14—H14	0.9500		0.9500
	1.442 (5)	$C_0/-C_{08}$	1.393 (6)
	0.9500		0.9500
	1.386 (5)	C68—H68	0.9500
	1.399 (5)	N21-C//	1.114 (6)
C18—C19	1.364 (6)	C70—N20	1.123 (6)
	0.9500	C/0—C69	1.440 (7)
C19—C20	1.400 (5)	N19—C/4	1.125 (8)
С19—Н19	0.9500	С69—Н69А	0.9800
C20—H20	0.9500	С69—Н69В	0.9800
C21—C22	1.398 (6)	С69—Н69С	0.9800
C21—H21	0.9500	C74—C75	1.453 (9)
C22—C23	1.367 (6)	C/5—H/5A	0.9800
C22—H22	0.9500	C75—H75B	0.9800
C23—C24	1.392 (6)	C/5—H75C	0.9800
С23—Н23	0.9500	C/8—C//	1.449 (7)
C24—C25	1.403 (5)	C/8—H78A	0.9800
C24—C26	1.433 (6)	C78—H78B	0.9800
C25—C29	1.414 (5)	C78—H78C	0.9800
C26—C27	1.348 (6)	OI—HIO	0.84 (2)
C26—H26	0.9500	01—H2O	0.85 (2)

C27—C28	1.439 (6)		
N4—Cr1—N3	93.08 (13)	С28—С27—Н27	119.5
N4—Cr1—N2	174.49 (14)	C30—C28—C29	117.6 (4)
N3—Cr1—N2	91.37 (14)	C30—C28—C27	124.1 (4)
N4—Cr1—N1	91.16 (14)	C29—C28—C27	118.3 (4)
N3—Cr1—N1	93.32 (14)	N12—C29—C28	121.9 (4)
N2—Cr1—N1	91.82 (14)	N12—C29—C25	117.9 (3)
N4—Cr1—N10	87.71 (13)	C28—C29—C25	120.2 (4)
N3—Cr1—N10	173.14 (14)	C31—C30—C28	119.6 (4)
N2—Cr1—N10	87.50 (13)	С31—С30—Н30	120.2
N1—Cr1—N10	93.48 (14)	С28—С30—Н30	120.2
N4—Cr1—N9	88.10 (13)	C30—C31—C32	119.7 (4)
N3—Cr1—N9	93.48 (13)	С30—С31—Н31	120.2
N2—Cr1—N9	88.38 (13)	С32—С31—Н31	120.2
N1—Cr1—N9	173.20 (13)	N12—C32—C31	122.3 (4)
N10-Cr1-N9	79.73 (13)	N12—C32—H32	118.8
N7—Cr2—N5	89.11 (14)	С31—С32—Н32	118.8
N7—Cr2—N8	89.61 (13)	N13—C33—C34	122.6 (4)
N5—Cr2—N8	94.14 (14)	N13—C33—H33	118.7
N7—Cr2—N6	175.77 (13)	С34—С33—Н33	118.7
N5—Cr2—N6	90.40 (14)	C35—C34—C33	119.9 (4)
N8—Cr2—N6	94.62 (13)	С35—С34—Н34	120.0
N7—Cr2—N12	88.04 (12)	С33—С34—Н34	120.0
N5—Cr2—N12	95.01 (13)	C34—C35—C36	119.9 (4)
N8—Cr2—N12	170.52 (13)	С34—С35—Н35	120.0
N6—Cr2—N12	87.81 (12)	С36—С35—Н35	120.0
N7—Cr2—N11	90.64 (13)	C37—C36—C35	116.5 (4)
N5—Cr2—N11	174.81 (13)	C37—C36—C38	118.2 (4)
N8—Cr2—N11	91.05 (13)	C35—C36—C38	125.3 (4)
N6—Cr2—N11	89.46 (13)	N13—C37—C36	124.0 (4)
N12—Cr2—N11	79.80 (12)	N13—C37—C41	115.8 (4)
N16—Fe1—N15	82.94 (14)	C36—C37—C41	120.2 (4)
N16—Fe1—N13	173.04 (13)	C39—C38—C36	121.9 (4)
N15—Fe1—N13	92.81 (13)	С39—С38—Н38	119.0
N16—Fe1—N18	95.12 (13)	C36—C38—H38	119.0
N15—Fe1—N18	173.96 (13)	C38—C39—C40	120.7 (5)
N13—Fe1—N18	89.65 (13)	С38—С39—Н39	119.7
N16—Fe1—N17	92.39 (13)	С40—С39—Н39	119.7
N15—Fe1—N17	92.11 (13)	C41—C40—C42	116.1 (4)
N13—Fe1—N17	93.27 (13)	C41—C40—C39	119.1 (4)
N18—Fe1—N17	82.24 (13)	C42—C40—C39	124.7 (4)
N16—Fe1—N14	92.28 (13)	N14—C41—C40	124.7 (4)
N15—Fe1—N14	93.11 (12)	N14—C41—C37	115.5 (3)
N13—Fe1—N14	82.42 (13)	C40—C41—C37	119.8 (4)
N18—Fe1—N14	92.68 (13)	C43—C42—C40	119.3 (4)
N17—Fe1—N14	173.38 (13)	C43—C42—H42	120.3
C1—N1—Cr1	166.9 (3)	C40—C42—H42	120.3

C2—N2—Cr1	176.1 (3)	C42—C43—C44	120.5 (4)
C3—N3—Cr1	170.3 (3)	C42—C43—H43	119.7
C4—N4—Cr1	170.4 (3)	C44—C43—H43	119.7
C5—N5—Cr2	167.4 (3)	N14—C44—C43	122.8 (4)
C6—N6—Cr2	166.9 (3)	N14—C44—H44	118.6
C7—N7—Cr2	169.4 (3)	C43—C44—H44	118.6
C8-N8-Cr2	170.1 (3)	N15-C45-C46	122.7(5)
C9-N9-C13	118 1 (3)	N15-C45-H45	118.6
C9-N9-Cr1	128 4 (3)	C46-C45-H45	118.6
C13 - N9 - Cr1	1135(3)	C47 - C46 - C45	119.9(5)
$C_{20}$ N10 $C_{17}$	118.6 (3)	C47 - C46 - H46	120.1
$C_{20}$ N10 $C_{r1}$	128.2(3)	C45 C46 H46	120.1
$C_{17}$ N10 $C_{r1}$	120.2(3) 113.2(2)	$C_{45} = C_{40} = 1140$	120.1
$C_{1}$ $N_{10}$ $C_{25}$	113.2(2) 117.5(4)	$C_{40} = C_{47} = C_{48}$	119.3 (4)
$C_{21}$ N11 $C_{23}$	117.3(4) 120.2(2)	$C_{40} = C_{47} = H_{47}$	120.3
$C_2 I = N I I = C I 2$	129.5 (3)	C48 - C47 - F147	120.5
$C_{23}$ N12 $C_{23}$	113.1 (3)	C47 - C48 - C49	117.2 (5)
$C_{32}$ —N12—C29	118.8 (3)	C47 - C48 - C50	125.3 (5)
C32—N12— $Cr2$	128.5 (3)	C49—C48—C50	117.5 (5)
C29—N12—Cr2	112.7 (2)	N15—C49—C48	123.6 (4)
C33—N13—C37	117.0 (4)	N15—C49—C53	115.7 (4)
C33—N13—Fe1	130.0 (3)	C48—C49—C53	120.8 (4)
C37—N13—Fe1	113.0 (3)	C51—C50—C48	121.9 (5)
C44—N14—C41	116.5 (3)	С51—С50—Н50	119.1
C44—N14—Fe1	130.2 (3)	C48—C50—H50	119.1
C41—N14—Fe1	113.3 (2)	C50—C51—C52	121.6 (5)
C45—N15—C49	117.1 (4)	C50—C51—H51	119.2
C45—N15—Fe1	130.3 (3)	C52—C51—H51	119.2
C49—N15—Fe1	112.6 (3)	C54—C52—C53	117.1 (4)
C56—N16—C53	117.1 (4)	C54—C52—C51	125.2 (5)
C56—N16—Fe1	129.9 (3)	C53—C52—C51	117.7 (5)
C53—N16—Fe1	112.9 (3)	N16—C53—C52	123.6 (4)
C57—N17—C61	117.1 (4)	N16—C53—C49	115.9 (4)
C57—N17—Fe1	130.0 (3)	C52—C53—C49	120.6 (4)
C61—N17—Fe1	112.7 (3)	C55—C54—C52	119.2 (4)
C68—N18—C65	117.0 (3)	С55—С54—Н54	120.4
C68—N18—Fe1	129.8 (3)	С52—С54—Н54	120.4
C65—N18—Fe1	113.0 (2)	C54—C55—C56	120.4 (5)
N1-C1-S1	178 2 (4)	C54—C55—H55	119.8
$N_2 - C_2 - S_2$	178.8 (4)	C56-C55-H55	119.8
N3-C3-S3	179.4 (4)	N16-C56-C55	122.6 (4)
N4-C4-S4	178.2 (4)	N16-C56-H56	118 7
N5_C5_\$5	170.2(1) 179.2(4)	C55_C56_H56	118.7
N6-C6-86	178.1 (3)	N17-C57-C58	122 1 (4)
N7	179.2 (4)	N17_C57_H57	122.1 (7)
$\frac{1}{10} = \frac{1}{10} = \frac{1}{10}$	179.2 (T) 178.8 (A)	$C_{58}$ $C_{57}$ $H_{57}$	118.0
$N_0 = C_0 = S_0$	122 6 (4)	$C_{50} = C_{57} = C_{57}$	110.7 120.2(4)
NO CO HO	122.0 (4)	$C_{59} = C_{50} = C_{57}$	120.2 (4)
119 - 0.7 - 117	110./	$C_{57} = C_{50} = H_{50}$	117.7
U10-U7-U7	110./	Сэ/—Сэо—пэо	117.7

C11—C10—C9	119.5 (4)	C58—C59—C60	119.9 (4)
C11—C10—H10	120.2	С58—С59—Н59	120.1
C9—C10—H10	120.2	С60—С59—Н59	120.1
C10-C11-C12	119.5 (4)	C61—C60—C59	116.1 (4)
C10-C11-H11	120.2	C61—C60—C62	119.2 (4)
C12—C11—H11	120.2	C59—C60—C62	124.6 (4)
C11—C12—C13	117.0 (4)	N17—C61—C60	124.5 (4)
C11—C12—C14	124.5 (4)	N17—C61—C65	116.1 (4)
$C_{13}$ $C_{12}$ $C_{14}$	1184(4)	C60 - C61 - C65	110.1(1) 119.4(4)
N9-C13-C12	123.2(4)	C63 - C62 - C60	119.1(1) 121.1(4)
N9-C13-C17	125.2(1) 116.6(3)	C63 - C62 - H62	119.5
$C_{12}$ $C_{13}$ $C_{17}$	120.2(4)	C60 - C62 - H62	119.5
$C_{12} = C_{13} = C_{17}$	120.2(4)	C62 - C63 - C64	117.5 121.0(4)
C15 - C14 - C12	121.0 (4)	C62 - C63 - C64	121.0 (4)
C13 - C14 - H14	119.2	C64 C63 H63	119.5
C12-C14-H14	119.2		119.3
C14 - C15 - C16	121.1 (4)	C65 - C64 - C66	117.0(4)
C14—C15—H15	119.5	C65 - C64 - C63	118.1 (4)
C16—C15—H15	119.5	C66-C64-C63	124.3 (4)
	117.2 (4)	N18—C65—C64	123.4 (4)
C18—C16—C15	124.6 (4)	N18—C65—C61	115.4 (3)
C17—C16—C15	118.1 (4)	C64—C65—C61	121.2 (4)
N10—C17—C16	122.6 (4)	C67—C66—C64	119.3 (4)
N10—C17—C13	116.9 (3)	С67—С66—Н66	120.3
C16—C17—C13	120.6 (4)	C64—C66—H66	120.3
C19—C18—C16	120.4 (4)	C66—C67—C68	120.1 (4)
C19—C18—H18	119.8	С66—С67—Н67	119.9
C16—C18—H18	119.8	С68—С67—Н67	119.9
C18—C19—C20	119.3 (4)	N18—C68—C67	122.5 (4)
C18—C19—H19	120.4	N18—C68—H68	118.7
С20—С19—Н19	120.4	C67—C68—H68	118.7
N10-C20-C19	122.0 (4)	N20—C70—C69	179.3 (6)
N10-C20-H20	119.0	С70—С69—Н69А	109.5
С19—С20—Н20	119.0	С70—С69—Н69В	109.5
N11—C21—C22	123.1 (4)	H69A—C69—H69B	109.5
N11—C21—H21	118.5	С70—С69—Н69С	109.5
C22—C21—H21	118.5	H69A—C69—H69C	109.5
C23—C22—C21	119.4 (4)	H69B—C69—H69C	109.5
C23—C22—H22	120.3	N19—C74—C75	178.8 (8)
C21—C22—H22	120.3	С74—С75—Н75А	109.5
$C_{22} - C_{23} - C_{24}$	119.5 (4)	C74—C75—H75B	109.5
C22—C23—H23	120.3	H75A—C75—H75B	109.5
$C_{24}$ $C_{23}$ $H_{23}$	120.3	C74 - C75 - H75C	109.5
$C_{23}$ $C_{24}$ $C_{25}$ $C_{25}$ $C_{25}$	117 8 (4)	H75A - C75 - H75C	109.5
$C_{23} = C_{24} = C_{25}$	177.0(7) 174 2 (4)	H75B_C75_H75C	109.5
$C_{25} = C_{24} = C_{26}$	127.2 (T) 117 Q (A)	C77_C78_H78A	109.5
123 - 024 - 020	117.7(4)	C77 C78 H78P	109.5
N11 $C25 C29$	122.7(4)	H78A C78 H78D	109.5
$C_{24} C_{25} C_{29}$	110.4 (4)	$\frac{11}{0A} - \frac{1}{0} - \frac{1}{0} \frac{1}{0$	109.5
U24-U2J-U2Y	120.7(4)	$U/1 - U/0 - \pi/0U$	109.3

C27—C26—C24	121.7 (4)	H78A—C78—H78C	109.5
С27—С26—Н26	119.2	H78B—C78—H78C	109.5
С24—С26—Н26	119.2	N21—C77—C78	179.0 (7)
C26—C27—C28	121.0 (4)	H10-01-H20	105 (5)
С26—С27—Н27	119.5		
N4—Cr1—N1—C1	-65.0 (15)	C20-N10-C17-C16	0.0 (5)
N3—Cr1—N1—C1	28.2 (15)	Cr1—N10—C17—C16	179.7 (3)
N2—Cr1—N1—C1	119.7 (15)	C20-N10-C17-C13	-178.1 (3)
N10-Cr1-N1-C1	-152.7 (15)	Cr1—N10—C17—C13	1.6 (4)
N9—Cr1—N1—C1	-148.7 (13)	C18-C16-C17-N10	-0.7 (5)
N4—Cr1—N2—C2	-30 (6)	C15-C16-C17-N10	-179.6 (3)
N3—Cr1—N2—C2	-173 (5)	C18—C16—C17—C13	177.3 (3)
N1—Cr1—N2—C2	93 (5)	C15—C16—C17—C13	-1.6 (5)
N10—Cr1—N2—C2	0 (5)	N9—C13—C17—N10	-0.4(5)
N9—Cr1—N2—C2	-80 (5)	C12-C13-C17-N10	178.7 (3)
N4—Cr1—N3—C3	104 (2)	N9—C13—C17—C16	-178.5(3)
N2—Cr1—N3—C3	-79 (2)	C12—C13—C17—C16	0.6 (5)
N1—Cr1—N3—C3	13 (2)	C17—C16—C18—C19	1.4 (6)
N10—Cr1—N3—C3	-159.7 (17)	C15—C16—C18—C19	-179.9 (4)
N9—Cr1—N3—C3	-168(2)	C16—C18—C19—C20	-1.3 (6)
N3—Cr1—N4—C4	177 (2)	C17—N10—C20—C19	0.1 (5)
N2—Cr1—N4—C4	33 (3)	Cr1—N10—C20—C19	-179.5(3)
N1—Cr1—N4—C4	-90(2)	$C_{18}$ $C_{19}$ $C_{20}$ $N_{10}$	0.5 (6)
N10-Cr1-N4-C4	4 (2)	C25—N11—C21—C22	-1.5(6)
N9—Cr1—N4—C4	83 (2)	Cr2—N11—C21—C22	179.1 (3)
N7—Cr2—N5—C5	-45.6(16)	N11-C21-C22-C23	0.3(7)
N8—Cr2—N5—C5	43.9 (16)	$C_{21}$ $-C_{22}$ $-C_{23}$ $-C_{24}$	1.9 (7)
N6—Cr2—N5—C5	138.6 (16)	C22—C23—C24—C25	-2.6(6)
N12—Cr2—N5—C5	-133.6(16)	C22—C23—C24—C26	177.0 (4)
N11—Cr2—N5—C5	-132.9(16)	$C_{21}$ N11 $-C_{25}$ $-C_{24}$	0.7 (5)
N7—Cr2—N6—C6	-61 (3)	Cr2-N11-C25-C24	-179.9(3)
N5— $Cr2$ — $N6$ — $C6$	22.6 (14)	$C_{21}$ N11 $-C_{25}$ $-C_{29}$	-177.9(3)
N8— $Cr2$ — $N6$ — $C6$	116.8 (14)	Cr2-N11-C25-C29	1.6 (4)
N12— $Cr2$ — $N6$ — $C6$	-72.4(14)	$C_{23}$ — $C_{24}$ — $C_{25}$ —N11	1.4 (6)
N11— $Cr2$ — $N6$ — $C6$	-152.2(14)	$C_{26}$ $C_{24}$ $C_{25}$ $N_{11}$	-178.2(3)
N5— $Cr2$ — $N7$ — $C7$	-9.2(17)	$C_{23}$ $C_{24}$ $C_{25}$ $C_{29}$	179.9 (4)
N8— $Cr2$ — $N7$ — $C7$	-1033(17)	$C_{26} - C_{24} - C_{25} - C_{29}$	03(6)
$N6-Cr^2-N7-C7$	74 (3)	$C_{23}$ $C_{24}$ $C_{26}$ $C_{27}$	-1782(4)
N12—Cr2—N7—C7	85.8 (17)	$C_{25}$ $C_{24}$ $C_{26}$ $C_{27}$	1.4 (6)
N11— $Cr2$ — $N7$ — $C7$	165.6(17)	$C_{24}$ $C_{26}$ $C_{27}$ $C_{28}$	-1.7(6)
N7— $Cr2$ — $N8$ — $C8$	-11(2)	$C_{26} - C_{27} - C_{28} - C_{30}$	1785(4)
N5-Cr2-N8-C8	-100(2)	$C_{26}$ $C_{27}$ $C_{28}$ $C_{29}$	0.3 (6)
N6-Cr2-N8-C8	169 (2)	$C_{32}$ $N_{12}$ $C_{29}$ $C_{28}$	0.6(5)
N12— $Cr2$ — $N8$ — $C8$	65 (2)	Cr2 N12 C29 C28	-177.9(3)
$N11 - Cr^2 - N8 - C8$	80 (2)	$C_{12} = 0_{112} = 0_{20} = 0_{20}$	1790(3)
N4-Cr1-N9-C9	93.9(3)	$C_{12} = C_{23} = C_{23}$ Cr2 = N12 = C29 = C25	0.5(4)
N3 Cr1 N9 C9	0.9(3)	$C_{12} = C_{12} = C_{23} = C$	1.3(5)
113-011-117-09	0.9 (3)	CJU-CZ0-CZ9-IN12	1.5 (5)

N2—Cr1—N9—C9	-90.4 (3)	C27—C28—C29—N12	179.6 (3)
N1—Cr1—N9—C9	177.8 (10)	C30—C28—C29—C25	-177.0(3)
N10—Cr1—N9—C9	-178.1 (4)	C27—C28—C29—C25	1.3 (5)
N4—Cr1—N9—C13	-86.6 (3)	N11—C25—C29—N12	-1.4(5)
N3—Cr1—N9—C13	-179.6(3)	C24—C25—C29—N12	-180.0(3)
N2-Cr1-N9-C13	89.2 (3)	N11-C25-C29-C28	177.0 (3)
N1-Cr1-N9-C13	-2.7(12)	$C_{24}$ $C_{25}$ $C_{29}$ $C_{28}$	-15(5)
N10-Cr1-N9-C13	14(2)	$C_{29}$ $C_{28}$ $C_{30}$ $C_{31}$	-2.1(6)
N4-Cr1-N10-C20	-935(3)	$C_{27}$ $C_{28}$ $C_{30}$ $C_{31}$	1797(4)
$N_{1} = Cr_{1} = N_{10} = C_{20}$	169.8 (10)	$C_{28}$ $C_{30}$ $C_{31}$ $C_{32}$	10(6)
$N_{2}$ Cr1 $N_{10}$ C20	89.2 (3)	$C_{20} = 0.00 = 0.001 = 0.002$	-1.8(6)
N1 - Cr1 - N10 - C20	-2.5(3)	$Cr^2 = N12 = C32 = C31$	1.0(0) 176 5 (3)
$N_{1} = C_{11} = N_{10} = C_{20}$	2.5(3)	$C_{12} = 1012 = C_{32} = C_{31}$	1/0.5(5)
$N_{4} = Cr_{1} = N_{10} = C_{20}$	86.9.(3)	$C_{30} - C_{31} - C_{32} - N_{12}$	1.0(0) 1.2(6)
$N_{1} = C_{1} = N_{10} = C_{17}$	-0.8(12)	$F_{e1}$ N13 C33 C34	-179.2(3)
$N_{2} = C_{*1} = N_{10} = C_{17}$	-9.0(12)	N13 C23 C34 C35	-0.2(7)
$N_2 - C_{11} - N_{10} - C_{17}$	90.4(3)	$C_{23} = C_{24} = C_{25} = C_{26}$	0.2(7)
NI = CII = NI0 = CI7	-1.6(2)	$C_{33} - C_{34} - C_{35} - C_{30}$	-0.7(7)
N7 Cr2 N11 C21	-1.0(2)	$C_{34} = C_{35} = C_{30} = C_{37}$	0.3(0)
$N = C_1 Z = N_1 I_1 = C_2 I_1$	90.3(3)	$C_{34} = C_{35} = C_{30} = C_{38}$	-1/7.0(4)
$N_{3} = C_{12} = N_{11} = C_{21}$	1/8(01)	$C_{33}$ N13 $C_{37}$ C36	-1.4(0)
$N_{0} = C_{12} = N_{11} = C_{21}$	0.8(3)	FeI = N13 = C37 = C30	179.0(3)
N0 - Cr2 - N11 - C21	-95.8(3)	$C_{33}$ N13 $C_{37}$ C41	1/8.1(3)
N12-CF2-N11-C21	1/8.4 (4)	FeI = N13 = C37 = C41	-1.5(4)
N = Cr2 = N11 = C25	-88.9(3)	$C_{35} = C_{36} = C_{37} = N_{13}$	0.6(6)
$N_{2} = C_{12} = N_{11} = C_{25}$	-1./(16)	$C_{38} = C_{30} = C_{37} = N_{13}$	1/9.0 (4)
N8 - Cr2 - N11 - C25	-1/8.5(3)	$C_{35} - C_{36} - C_{37} - C_{41}$	-1/9.0(4)
N6—Cr2—N11—C25	86.8 (3)	$C_{38} = C_{36} = C_{37} = C_{41}$	-0.5 (6)
N12—Cr2—N11—C25	-1.0(2)	$C_{3}/-C_{3}6-C_{3}8-C_{3}9$	-1.0 (7)
N/-Cr2-N12-C32	-87.0(3)	C35—C36—C38—C39	177.3 (5)
N5—Cr2—N12—C32	1.9 (3)	C36—C38—C39—C40	1.2 (7)
N8—Cr2—N12—C32	-162.8 (7)	C38—C39—C40—C41	0.2 (7)
N6—Cr2—N12—C32	92.1 (3)	C38—C39—C40—C42	-17/.8(5)
N11—Cr2—N12—C32	-178.0 (3)	C44—N14—C41—C40	0.0 (6)
N7—Cr2—N12—C29	91.3 (3)	Fe1—N14—C41—C40	178.7 (3)
N5—Cr2—N12—C29	-179.7 (3)	C44—N14—C41—C37	-178.5 (3)
N8—Cr2—N12—C29	15.6 (9)	Fe1—N14—C41—C37	0.2 (4)
N6—Cr2—N12—C29	-89.5 (3)	C42—C40—C41—N14	-2.0 (6)
N11—Cr2—N12—C29	0.3 (2)	C39—C40—C41—N14	179.8 (4)
N16—Fe1—N13—C33	141.1 (10)	C42—C40—C41—C37	176.5 (4)
N15—Fe1—N13—C33	88.9 (4)	C39—C40—C41—C37	-1.7 (6)
N18—Fe1—N13—C33	-85.6 (4)	N13—C37—C41—N14	0.9 (5)
N17—Fe1—N13—C33	-3.4 (4)	C36—C37—C41—N14	-179.5 (4)
N14—Fe1—N13—C33	-178.3 (4)	N13—C37—C41—C40	-177.7 (4)
N16—Fe1—N13—C37	-39.3 (12)	C36—C37—C41—C40	1.9 (6)
N15—Fe1—N13—C37	-91.5 (3)	C41—C40—C42—C43	1.6 (6)
N18—Fe1—N13—C37	94.0 (3)	C39—C40—C42—C43	179.7 (4)
N17—Fe1—N13—C37	176.2 (3)	C40—C42—C43—C44	0.5 (7)
N14—Fe1—N13—C37	1.2 (3)	C41—N14—C44—C43	2.4 (6)

N16—Fe1—N14—C44	-6.8 (4)	Fe1—N14—C44—C43	-176.0 (3)
N15—Fe1—N14—C44	-89.9 (4)	C42—C43—C44—N14	-2.7 (7)
N13—Fe1—N14—C44	177.7 (4)	C49—N15—C45—C46	-1.6(5)
N18—Fe1—N14—C44	88.4 (3)	Fe1—N15—C45—C46	-179.3 (3)
N17—Fe1—N14—C44	128.1 (11)	N15—C45—C46—C47	1.9 (6)
N16—Fe1—N14—C41	174.7 (3)	C45—C46—C47—C48	-1.3(7)
N15—Fe1—N14—C41	91.7 (3)	C46—C47—C48—C49	0.5 (6)
N13—Fe1—N14—C41	-0.7 (3)	C46—C47—C48—C50	-179.8 (4)
N18—Fe1—N14—C41	-90.0 (3)	C45—N15—C49—C48	0.8 (5)
N17—Fe1—N14—C41	-50.4 (13)	Fe1—N15—C49—C48	178.9 (3)
N16—Fe1—N15—C45	177.4 (3)	C45—N15—C49—C53	-178.8(3)
N13—Fe1—N15—C45	-8.1 (3)	Fe1—N15—C49—C53	-0.8(4)
N18—Fe1—N15—C45	105.9 (13)	C47—C48—C49—N15	-0.2(6)
N17—Fe1— $N15$ —C45	85.3 (3)	C50-C48-C49-N15	-180.0(4)
N14—Fe1—N15—C45	-90.6 (3)	C47—C48—C49—C53	179.4 (4)
N16—Fe1—N15—C49	-0.3(2)	$C_{50}$ $C_{48}$ $C_{49}$ $C_{53}$	-0.4(6)
N13—Fe1—N15—C49	174.2 (3)	C47 - C48 - C50 - C51	179.6 (5)
N18—Fe1— $N15$ —C49	-71.9(14)	C49—C48—C50—C51	-0.7(7)
N17—Fe1—N15—C49	-92.4(3)	C48 - C50 - C51 - C52	0.6 (8)
N14—Fe1—N15—C49	91.6 (3)	$C_{50}$ $C_{51}$ $C_{52}$ $C_{54}$	-178.4(5)
N15—Fe1— $N16$ —C56	178.0 (3)	C50-C51-C52-C53	0.6 (7)
N13—Fe1—N16—C56	125.3 (10)	C56—N16—C53—C52	1.5 (5)
N18—Fe1—N16—C56	-7.8 (3)	Fe1—N16—C53—C52	178.6 (3)
N17—Fe1—N16—C56	-90.2(3)	$C_{56}$ N16 $C_{53}$ C49	-179.2(3)
N14—Fe1— $N16$ —C56	85.1 (3)	Fe1—N16—C53—C49	-2.1(4)
N15—Fe1—N16—C53	1.3 (2)	C54—C52—C53—N16	-3.4(6)
N13—Fe1—N16—C53	-51.4 (11)	C51—C52—C53—N16	177.5 (4)
N18—Fe1—N16—C53	175.6 (2)	C54—C52—C53—C49	177.4 (4)
N17—Fe1—N16—C53	93.2 (3)	C51—C52—C53—C49	-1.7(6)
N14—Fe1—N16—C53	-91.5 (3)	N15-C49-C53-N16	1.9 (5)
N16—Fe1—N17—C57	-83.2 (4)	C48—C49—C53—N16	-177.7(3)
N15—Fe1—N17—C57	-0.2 (4)	N15—C49—C53—C52	-178.8(3)
N13—Fe1—N17—C57	92.7 (4)	C48—C49—C53—C52	1.6 (6)
N18—Fe1—N17—C57	-178.1 (4)	C53—C52—C54—C55	2.5 (6)
N14—Fe1—N17—C57	141.9 (11)	C51—C52—C54—C55	-178.4 (4)
N16—Fe1—N17—C61	101.1 (3)	C52—C54—C55—C56	-0.1 (6)
N15—Fe1—N17—C61	-175.9 (3)	C53—N16—C56—C55	1.1 (6)
N13—Fe1—N17—C61	-83.0 (3)	Fe1—N16—C56—C55	-175.4 (3)
N18—Fe1—N17—C61	6.2 (3)	C54—C55—C56—N16	-1.8 (6)
N14—Fe1—N17—C61	-33.8 (13)	C61—N17—C57—C58	0.5 (6)
N16—Fe1—N18—C68	86.4 (3)	Fe1—N17—C57—C58	-175.1 (3)
N15—Fe1—N18—C68	157.4 (12)	N17—C57—C58—C59	-0.1 (7)
N13—Fe1—N18—C68	-88.5 (3)	C57—C58—C59—C60	-0.4 (7)
N17—Fe1—N18—C68	178.1 (4)	C58—C59—C60—C61	0.5 (7)
N14—Fe1—N18—C68	-6.1 (3)	C58—C59—C60—C62	178.5 (5)
N16—Fe1—N18—C65	-98.4 (3)	C57—N17—C61—C60	-0.4 (6)
N15—Fe1—N18—C65	-27.5 (14)	Fe1—N17—C61—C60	175.9 (3)
N13—Fe1—N18—C65	86.6 (3)	C57—N17—C61—C65	179.0 (4)
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$\begin{array}{l} N17 - Fe1 - N18 - C65 \\ N14 - Fe1 - N18 - C65 \\ Cr1 - N1 - C1 - S1 \\ Cr1 - N2 - C2 - S2 \\ Cr1 - N3 - C3 - S3 \\ Cr1 - N4 - C4 - S4 \\ Cr2 - N5 - C5 - S5 \\ Cr2 - N6 - C6 - S6 \\ Cr2 - N7 - C7 - S7 \\ Cr2 - N8 - C8 - S8 \\ C13 - N9 - C9 - C10 \\ Cr1 - N9 - C9 - C10 \\ N9 - C9 - C10 - C11 \end{array}$	$\begin{array}{c} -6.7 (2) \\ 169.0 (3) \\ -6 (14) \\ 108 (22) \\ -12 (36) \\ 164 (11) \\ -173 (100) \\ -102 (11) \\ -167 (100) \\ -146 (16) \\ 0.0 (6) \\ 179.5 (3) \\ 0.6 (7) \end{array}$	$\begin{array}{l} Fe1 &N17 &C61 &C65 \\ C59 &C60 &C61 &N17 \\ C62 &C60 &C61 &N17 \\ C59 &C60 &C61 &C65 \\ C62 &C60 &C62 &C63 \\ C60 &C62 &C63 \\ C60 &C62 &C63 \\ C62 &C63 &C64 \\ C62 &C63 &C64 \\ C62 &C63 &C64 \\ Fe1 &N18 &C65 &C64 \\ C68 &N18 &C65 &C64 \\ C68 &N18 &C65 &C61 \\ \end{array}$	$\begin{array}{c} -4.8 (4) \\ -0.1 (6) \\ -178.2 (4) \\ -179.4 (4) \\ 2.4 (6) \\ -1.8 (6) \\ -179.8 (4) \\ -0.5 (7) \\ 2.0 (6) \\ -177.3 (4) \\ 1.3 (5) \\ -174.5 (3) \\ -178.1 (3) \end{array}$
Cr1—N4—C4—S4	164 (11)	C61—C60—C62—C63	-1.8(6)
Cr2—N5—C5—S5	-173 (100)	C59—C60—C62—C63	-179.8(4)
Cr2—N6—C6—S6	-102 (11)	C60—C62—C63—C64	-0.5(7)
Cr2—N5—C5—S5	-173 (100)	C59—C60—C62—C63	-179.8 (4)
Cr2—N6—C6—S6	-102 (11)	C60—C62—C63—C64	-0.5 (7)
$Cr2_N/-C/-S/$	-167(100)	C62 - C63 - C64 - C65	2.0(6)
$Cr2_N8_C8_S8$	-146(16)	C62 - C63 - C64 - C66	-177.3(4)
$C13_N9_C9_C10$	0.0(6)	C68 - N18 - C65 - C64	1.3(5)
Cr1—N9—C9—C10	179.5 (3)	Fe1—N18—C65—C64	-174.5(3)
N9—C9—C10—C11	0.6 (7)	C68—N18—C65—C61	-178.1(3)
C9—C10—C11—C12	-0.8 (6)	Fe1—N18—C65—C61	6.1 (4)
C10—C11—C12—C13	0.4 (6)	C66—C64—C65—N18	-1.3 (6)
C10—C11—C12—C14	-179.0 (4)	C63—C64—C65—N18	179.3 (3)
C9—N9—C13—C12	-0.5 (5)	C66—C64—C65—C61	178.0 (4)
Cr1—N9—C13—C12	179.9 (3)	C63—C64—C65—C61	-1.3 (6)
C9—N9—C13—C17	178.6 (3)	N17—C61—C65—N18	-0.9 (5)
Cr1—N9—C13—C17 C11—C12—C13—N9 C14—C12—C13—N9	-1.0(4) 0.3(6) 1797(3)	C60—C61—C65—N18 N17—C61—C65—C64	178.5(3) 179.7(4) -0.9(6)
C11—C12—C13—C17 C14—C12—C13—C17 C14—C12—C13—C17	-178.7(3) 0 7 (5)	C65—C64—C66—C67 C63—C64—C66—C67	-0.9 (0) 0.6 (6) 179 9 (4)
C11—C12—C14—C15	178.5 (4)	C64—C66—C67—C68	0.1 (7)
C13—C12—C14—C15	-0.9 (6)	C65—N18—C68—C67	-0.5 (6)
C12—C14—C15—C16 C14—C15—C16—C18 C14—C15—C16—C17	-0.1 (6) -177.4 (4)	Fe1—N18—C68—C67 C66—C67—C68—N18	174.5 (3) -0.2 (7)
	1.T (U)		