

Acta Crystallographica Section E **Structure Reports** Online

ISSN 1600-5368

2-(4-{4-[4-(Oxiran-2-vlmethoxy)phenoxy]phenyl}phenoxymethyl)oxirane

Tao Song, Jin-gang Liu* and Shi-yong Yang*

Laboratory of Advanced Polymer Materials, Institute of Chemistry, Chinese Academy of Sciences (ICCAS), Beijing 100190, People's Republic of China Correspondence e-mail: liujg@iccas.ac.cnx, shiyang@iccas.ac.cn

Received 8 February 2012; accepted 9 February 2012

Key indicators: single-crystal X-ray study; T = 173 K; mean σ (C–C) = 0.009 Å; disorder in main residue; R factor = 0.085; wR factor = 0.172; data-to-parameter ratio = 6.2.

In the title epoxy monomer, $C_{24}H_{22}O_5$, the dihedral angle in the biphenyl residue is $3.34 (19)^\circ$, indicating a nearly coplanar conformation; this residue is not planar with the adjacent benzene ring [dihedral angle = $58.93 (14)^{\circ}$]. Each of the epoxide rings is disordered. Each epoxide ring was resolved over two alternative positions with site-occupancy ratios of 0.638 (10):0.362 (10) and 0.797 (9):0.203 (9).

Related literature

For micro-electronic applications of biphenyl-type epoxy compounds, see: Lee & Neville (1990); Yoda (1997); Kim & Lee (2002). For related structures, see: Cho et al. (1999); Flippen-Anderson & Gilardi (1981).



Experimental

Crystal data

C ₂₄ H ₂₂ O ₅	V = 951.2 (3) Å ³
$M_r = 390.42$	Z = 2
Monoclinic, Pc	Mo $K\alpha$ radiation
a = 21.261 (4) Å	$\mu = 0.10 \text{ mm}^{-1}$
b = 7.3103 (15) Å	$T = 173 { m K}$
c = 6.1322 (12) Å	$0.35 \times 0.15 \times 0.08$
$\beta = 93.59 \ (3)^{\circ}$	

Data collection

Rigaku Saturn724+ CCD diffractometer Absorption correction: multi-scan (CrystalClear; Rigaku, 2008) $T_{\min} = 0.983, T_{\max} = 0.992$

Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.085$ $wR(F^2) = 0.172$ S = 1.181965 reflections 318 parameters

mm

6607 measured reflections 1965 independent reflections 1728 reflections with $I > 2\sigma(I)$ $R_{\rm int} = 0.065$

264 restraints H-atom parameters constrained $\Delta \rho_{\rm max} = 0.23 \text{ e} \text{ Å}^{-3}$ $\Delta \rho_{\rm min} = -0.19$ e Å⁻³

Data collection: CrystalClear (Rigaku, 2008); cell refinement: CrystalClear; data reduction: CrystalClear; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008): program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: Mercury (Macrae et al., 2006); software used to prepare material for publication: SHELXL97.

The authors are grateful to the National Natural Science Foundation of China for financial support. They thank Dr Lin Wang of ICCAS for the X-ray data collection.

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: TK5057).

References

Cho, C.-S., Liau, W.-B. & Chen, L.-W. (1999). Acta Cryst. B55, 525-529. Flippen-Anderson, J. L. & Gilardi, R. (1981). Acta Cryst. B37, 1433-1435. Kim, W. G. & Lee, J. Y. (2002). J. Appl. Polym. Sci. 86, 1942-1952.

Lee, H. & Neville, K. (1990). In Handbook of Epoxy Resins. New York: McGraw-Hill

Macrae, C. F., Edgington, P. R., McCabe, P., Pidcock, E., Shields, G. P., Taylor, R., Towler, M. & van de Streek, J. (2006). J. Appl. Cryst. 39, 453-457.

Rigaku (2008). CrystalClear. Rigaku Corporation, Tokyo, Japan.

Sheldrick, G. M. (2008). Acta Cryst. A64, 112-122.

Yoda, N. (1997). Polym. Adv. Technol. 8, 215-226.

supporting information

Acta Cryst. (2012). E68, o719 [doi:10.1107/S1600536812005740]

2-(4-{4-[4-(Oxiran-2-ylmethoxy)phenoxy]phenyl}phenoxymethyl)oxirane

Tao Song, Jin-gang Liu and Shi-yong Yang

S1. Comment

The title compound can be used as matrix for epoxy coating, paintings, composites and adhesives (Lee & Neville, 1990). Especially, this compound is a very useful component for advanced epoxy molding compounds (EMCs) for microelectronic packaging. The asymmetric crystalline nature of the title epoxy compound endows the obtained EMCs with very low melting viscosity, thus providing good flow-ability during molding process (Kim & Lee, 2002). Good flow-ability of the EMCs is crucial for the packaging of thin type microelectronic devices (Yoda, 1997).

The title compound has an asymmetrical structure. The dihedral angle between the benzene ring (C16—C21) and the biphenyl ring is $58.93 (14)^{\circ}$. The dihedral angle in the biphenyl moiety is $3.34 (19)^{\circ}$, indicating a essentially co-planar conformation.

As can be seen from Fig. 1, the epoxide rings in molecule (I) are locally disordered. The two disordered residues consist of two alternative orientations for the epoxide rings connected to C3 and C22, respectively. Such disorder for epoxide rings has been noted in the literature (Cho *et al.*, 1999; Flippen-Anderson & Gilardi, 1981).

S2. Experimental

4-(*p*-Hydroxyphenoxy)-4'-hydroxybiphenyl (27.8 g, 0.1 mol), epichlorohydrin (222 g, 2.4 mol), and the phase transfer agent, benzyltrimethylammonium chloride (BTMAC, 0.216 g, 1 mmol) were put into a 250 ml four-necked flask equipped with a stirrer, a drop funnel, a condenser, and a thermometer. The reaction mixture was then heated to reflux for 60 min. until a homogeneous solution formed. An aqueous solution of NaOH (45 wt%, 20 g) was added drop wise over 3 h at 333 K. Then, the reaction was heated under reflux for 2 h and cooled to room temperature. The obtained white precipitate was filtered, washed with deionized water and dried *in vacuo* at 353 K overnight. The white crystalline powder was further purified by recrystallization from acetonitrile to afford the title compound (29.2 g, 75% yield). Elemental analysis: calculated for $C_{24}H_{22}O_5$: C, 73.83; H, 5.68%. Found: C, 73.73; H, 5.69%. EI—MS, *m/z*: 390(100, *M*⁺). Colourless crystals were grown by slow evaporation of an acetone-diethyl ether solution (1:3, volume ratio) over a period of several days, M.pt:. 438 K.

S3. Refinement

H atoms were positioned geometrically (C—H = 0.95–1.00 Å) and refined using a riding model with the $U_{iso}(H) = 1.2U_{eq}(C)$.



Figure 1

The molecular structure of (I) showing the atom numbering scheme. Displacement ellipsoids are drawn at the 30% probability level. H atoms are not shown. The atoms labelled with a prime correspond to the minor components of the disordered residues.

2-(4-{4-[4-(Oxiran-2-ylmethoxy)phenoxy]phenyl}phenoxymethyl)oxirane

Crystal data	
C ₂₄ H ₂₂ O ₅	F(000) = 412
$M_r = 390.42$	$D_{\rm x} = 1.363 {\rm ~Mg} {\rm ~m}^{-3}$
Monoclinic, Pc	Melting point: 438 K
Hall symbol: P -2yc	Mo <i>K</i> α radiation, $\lambda = 0.71073$ Å
a = 21.261 (4) Å	Cell parameters from 2903 reflections
b = 7.3103 (15) Å	$\theta = 1.9-27.4^{\circ}$
c = 6.1322 (12) Å	$\mu = 0.10 \text{ mm}^{-1}$
$\beta = 93.59 \ (3)^{\circ}$	T = 173 K
V = 951.2 (3) Å ³	Rod, colourless
Z = 2	$0.35 \times 0.15 \times 0.08 \text{ mm}$

Data collection

Rigaku Saturn724+ CCD diffractometer Radiation source: fine-focus sealed tube Graphite monochromator Detector resolution: 28.5714 pixels mm ⁻¹ ω scans at fixed $\chi = 45^{\circ}$ Absorption correction: multi-scan (<i>CrystalClear</i> ; Rigaku, 2008) $T_{\min} = 0.983, T_{\max} = 0.992$	6607 measured reflections 1965 independent reflections 1728 reflections with $I > 2\sigma(I)$ $R_{int} = 0.065$ $\theta_{max} = 26.5^{\circ}, \theta_{min} = 2.8^{\circ}$ $h = -26 \rightarrow 26$ $k = -9 \rightarrow 8$ $l = -6 \rightarrow 7$
Refinement	
Refinement on F^2 Least-squares matrix: full $R[F^2 > 2\sigma(F^2)] = 0.085$ $wR(F^2) = 0.172$ S = 1.18 1965 reflections 318 parameters 264 restraints Primary atom site location: structure-invariant direct methods	Secondary atom site location: difference Fourier map Hydrogen site location: inferred from neighbouring sites H-atom parameters constrained $w = 1/[\sigma^2(F_o^2) + (0.0442P)^2 + 0.969P]$ where $P = (F_o^2 + 2F_c^2)/3$ $(\Delta/\sigma)_{max} = 0.001$ $\Delta\rho_{max} = 0.23$ e Å ⁻³ $\Delta\rho_{min} = -0.19$ e Å ⁻³

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $(Å^2)$

	x	у	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	Occ. (<1)
O2	0.9679 (2)	0.7379 (6)	0.1402 (7)	0.0392 (11)	
03	0.54379 (19)	0.7479 (6)	-0.6168 (6)	0.0332 (10)	
O4	0.3068 (2)	0.7607 (6)	-0.2978 (7)	0.0410 (11)	
01	1.0723 (6)	0.8198 (13)	0.6156 (15)	0.061 (2)	0.638 (10)
C1	1.0717 (6)	0.6394 (13)	0.5111 (18)	0.060 (2)	0.638 (10)
H1B	1.1127	0.5836	0.4810	0.072*	0.638 (10)
H1A	1.0386	0.5516	0.5492	0.072*	0.638 (10)
C2	1.0523 (4)	0.7999 (16)	0.3903 (17)	0.055 (2)	0.638 (10)
H2	1.0802	0.8476	0.2777	0.066*	0.638 (10)
01′	1.0674 (10)	0.770 (3)	0.653 (2)	0.060 (3)	0.362 (10)
C1′	1.0982 (9)	0.767 (3)	0.449 (3)	0.059 (3)	0.362 (10)
H1′B	1.1318	0.6756	0.4321	0.070*	0.362 (10)
H1'A	1.1042	0.8853	0.3743	0.070*	0.362 (10)
C2′	1.0322 (7)	0.700 (2)	0.466 (3)	0.058 (3)	0.362 (10)
H2′	1.0254	0.5642	0.4592	0.070*	0.362 (10)
C3	0.9816 (3)	0.8206 (11)	0.3504 (11)	0.0502 (19)	

	0.0.501		0.4646	0.0.0.0.	
H3A	0.9591	0.7566	0.4646	0.060*	
H3B	0.9692	0.9512	0.3485	0.060*	
C4	0.9072 (2)	0.7504 (8)	0.0492 (9)	0.0279 (13)	
C5	0.8585 (3)	0.8380 (8)	0.1427 (9)	0.0354 (15)	
H5	0.8656	0.8995	0.2784	0.042*	
C6	0.7988 (3)	0.8361 (8)	0.0377 (9)	0.0346 (14)	
H6	0.7654	0.8960	0.1051	0.041*	
C7	0.7856 (3)	0.7487 (8)	-0.1651 (9)	0.0267 (12)	
C8	0.8369 (3)	0.6606 (8)	-0.2527 (9)	0.0317 (14)	
H8	0.8308	0.5998	-0.3893	0.038*	
C9	0.8956 (3)	0.6597 (8)	-0.1472 (9)	0.0300 (13)	
H9	0.9289	0.5957	-0.2098	0.036*	
C10	0.7221 (3)	0.7498 (7)	-0.2772(9)	0.0263 (12)	
C11	0.6702 (3)	0.8303 (8)	-0.1862(9)	0.0336 (14)	
H11	0.6764	0.8877	-0.0475	0.040*	
C12	0.6101 (3)	0.8307 (8)	-0.2881(10)	0.0343 (14)	
H12	0 5760	0 8871	-0.2209	0.041*	
C13	0.6008 (3)	0 7464 (8)	-0.4914(9)	0.0313(14)	
C14	0.6509(3)	0.6685 (8)	-0.5893(9)	0.0313(14) 0.0299(13)	
H14	0.6449	0.6136	-0.7295	0.0255 (15)	
C15	0.0449 0.7100 (3)	0.6714 (8)	-0.4809(9)	0.030	
U15	0.7100 (5)	0.6714 (8)	-0.5500	0.0313 (13)	
C16	0.7441 0.4871 (2)	0.0100 0.7515 (8)	-0.5172(0)	0.038°	
C10	0.4671(3)	0.7515(8)	-0.3173(9)	0.0294(13)	
U17	0.4739 (3)	0.0301 (8)	-0.3279(9)	0.0292 (12)	
HI/	0.5092	0.5914	-0.251/	0.035*	
C18	0.4161 (3)	0.6554 (8)	-0.2499 (10)	0.0370(14)	
HI8	0.4082	0.5906	-0.1202	0.044*	
C19	0.3672 (3)	0.7514 (8)	-0.3645 (9)	0.0311 (14)	
C20	0.3787 (3)	0.8422 (8)	-0.5512 (9)	0.0349 (14)	
H20	0.3453	0.9050	-0.6294	0.042*	
C21	0.4385 (3)	0.8444 (8)	-0.6291 (9)	0.0299 (13)	
H21	0.4460	0.9096	-0.7589	0.036*	
C22	0.2927 (3)	0.6724 (9)	-0.1012 (10)	0.0426 (16)	
H22B	0.3163	0.7297	0.0254	0.051*	
H22A	0.3041	0.5412	-0.1060	0.051*	
05	0.2061 (4)	0.6830 (10)	0.1419 (11)	0.061 (2)	0.797 (9)
C23	0.2222 (4)	0.6948 (12)	-0.0834 (13)	0.056 (2)	0.797 (9)
H23	0.1924	0.6448	-0.2014	0.067*	0.797 (9)
C24	0.2043 (5)	0.8605 (11)	0.0384 (15)	0.063 (2)	0.797 (9)
H24B	0.2380	0.9489	0.0829	0.075*	0.797 (9)
H24A	0.1626	0.9157	0.0004	0.075*	0.797 (9)
O5′	0.1776 (12)	0.714 (4)	-0.023 (4)	0.063 (3)	0.203 (9)
C23′	0.2400 (10)	0.788 (4)	-0.012(6)	0.059 (3)	0.203 (9)
H23A	0.2427	0.9221	-0.0413	0.071*	0.203 (9)
C24′	0.207 (2)	0.737 (8)	0.193 (4)	0.061 (3)	0.203 (9)
H24C	0.2210	0.6258	0.2739	0.073*	0.203 (9)
H24D	0.1915	0.8373	0.2843	0.073*	0.203 (9)
114 112	0.1710	0.0010	0.2012	0.075	5.205 ())

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	U^{23}
02	0.028 (2)	0.047 (3)	0.042 (3)	0.011 (2)	-0.0011 (18)	-0.008 (2)
03	0.030(2)	0.042 (3)	0.028 (2)	-0.0026 (18)	0.0013 (17)	-0.0061 (18)
04	0.040 (3)	0.042 (3)	0.041 (2)	0.006 (2)	0.001 (2)	0.011 (2)
01	0.060 (4)	0.069 (5)	0.053 (4)	0.006 (4)	-0.008 (3)	-0.003 (4)
C1	0.057 (4)	0.064 (5)	0.058 (4)	0.004 (4)	-0.005 (4)	-0.005 (4)
C2	0.053 (4)	0.063 (5)	0.048 (4)	0.002 (4)	-0.001 (4)	-0.003 (4)
01′	0.058 (4)	0.069 (5)	0.052 (5)	0.005 (4)	-0.003 (4)	-0.003 (4)
C1′	0.056 (5)	0.067 (5)	0.052 (5)	0.003 (4)	-0.001 (4)	0.000 (4)
C2′	0.056 (5)	0.064 (5)	0.053 (5)	0.003 (4)	-0.007 (4)	-0.002 (4)
C3	0.039 (4)	0.062 (5)	0.047 (4)	0.015 (3)	-0.012 (3)	-0.011 (4)
C4	0.022 (3)	0.029 (3)	0.032 (3)	0.007 (2)	0.002 (2)	0.005 (2)
C5	0.045 (4)	0.029 (3)	0.032 (3)	-0.003 (3)	0.000 (3)	0.003 (2)
C6	0.045 (4)	0.027 (3)	0.032 (3)	0.009 (3)	0.001 (3)	0.001 (3)
C7	0.031 (3)	0.024 (3)	0.025 (3)	-0.004 (2)	0.005 (2)	0.011 (2)
C8	0.033 (3)	0.032 (3)	0.031 (3)	0.004 (3)	0.007 (3)	-0.006 (2)
C9	0.024 (3)	0.033 (3)	0.035 (3)	0.009 (2)	0.013 (2)	-0.003 (3)
C10	0.031 (3)	0.022 (3)	0.026 (3)	0.003 (2)	0.008 (2)	-0.002 (2)
C11	0.044 (4)	0.026 (3)	0.030 (3)	-0.002 (3)	0.000 (3)	-0.006 (2)
C12	0.037 (4)	0.028 (3)	0.038 (3)	-0.005 (3)	-0.001 (3)	-0.005 (3)
C13	0.036 (3)	0.026 (3)	0.032 (3)	-0.018 (3)	0.004 (3)	0.002 (2)
C14	0.033 (3)	0.035 (3)	0.022 (3)	0.005 (3)	0.002 (2)	-0.006 (2)
C15	0.025 (3)	0.039 (3)	0.032 (3)	-0.003 (3)	0.016 (2)	-0.004 (3)
C16	0.036 (3)	0.020 (3)	0.033 (3)	0.001 (2)	0.003 (2)	-0.011 (2)
C17	0.028 (3)	0.028 (3)	0.031 (3)	0.000 (2)	-0.002 (2)	0.002 (2)
C18	0.045 (4)	0.030 (3)	0.036 (3)	-0.003 (3)	0.001 (3)	-0.004 (3)
C19	0.019 (3)	0.034 (3)	0.040 (3)	0.007 (2)	-0.005 (2)	-0.009 (3)
C20	0.041 (4)	0.033 (3)	0.030 (3)	0.009 (3)	-0.008 (3)	0.007 (3)
C21	0.033 (3)	0.030 (3)	0.027 (3)	0.000 (3)	0.004 (2)	0.007 (2)
C22	0.034 (3)	0.050 (4)	0.044 (4)	0.004 (3)	0.007 (3)	0.017 (3)
05	0.057 (3)	0.071 (4)	0.058 (3)	0.011 (3)	0.024 (3)	0.009 (3)
C23	0.055 (4)	0.063 (4)	0.053 (4)	0.006 (4)	0.020 (3)	0.001 (4)
C24	0.060 (4)	0.066 (4)	0.064 (4)	0.006 (4)	0.016 (3)	0.002 (4)
O5′	0.061 (5)	0.070 (5)	0.061 (5)	0.005 (5)	0.017 (4)	0.002 (5)
C23′	0.058 (5)	0.064 (5)	0.057 (5)	0.005 (5)	0.015 (5)	0.004 (5)
C24′	0.060 (5)	0.067 (6)	0.058 (5)	0.007 (5)	0.017 (5)	0.002 (5)

Geometric parameters (Å, °)

02—C4	1.378 (7)	C11—C12	1.386 (8)	
O2—C3	1.437 (7)	C11—H11	0.9500	
O3—C16	1.385 (7)	C12—C13	1.393 (8)	
O3—C13	1.395 (7)	C12—H12	0.9500	
O4—C19	1.374 (7)	C13—C14	1.377 (8)	
O4—C22	1.416 (7)	C14—C15	1.385 (8)	
O1—C2	1.427 (8)	C14—H14	0.9500	

01—C1	1.466 (9)	C15—H15	0.9500
C1—C2	1.434 (13)	C16—C21	1.382 (8)
C1—H1B	0.9900	C16—C17	1.388 (8)
C1—H1A	0.9900	C17—C18	1.387 (8)
C2—C3	1.517 (8)	С17—Н17	0.9500
C2—H2	1.0000	C18—C19	1.405 (8)
01′—C2′	1.423 (10)	С18—Н18	0.9500
01'	1 444 (10)	C19-C20	1 359 (9)
C1' - C2'	1 498 (18)	C_{20} C_{21}	1 386 (8)
C1'—H1'B	0.9900	C20—H20	0.9500
C1' - H1'A	0.9900	C_{21} H21	0.9500
C^{2} – C^{3}	1 532 (10)	C^{22} C^{23}	1 519 (8)
C2'_H2'	1,0000	$C_{22} = C_{23}$	1.519(0) 1.532(10)
C3—H3A	0.9900	C22_H22B	0.9900
C3_H3B	0.9900	C22_H22A	0.9900
C4—C5	1 373 (8)	05-024	1.444(8)
$C_1 = C_2$	1.373 (8)	05 C23	1.447(8)
C_{1}	1.303 (0)	C_{23}^{23} C_{24}^{24}	1.447 (8)
C5_H5	0.0500	$C_{23} = C_{24}$	1.485 (8)
C6 C7	1 410 (8)	C24 H24P	0.0000
C6C7	1.410 (8)	C_{24} H24B	0.9900
C_{0}	1 404 (8)	$C_2 - 112 + A$	1.420(10)
$C_{7} = C_{8}$	1.404(6) 1.476(7)	03 - 023	1.430(10) 1.435(10)
C^{2}	1.470(7) 1.260(8)	$C_{23'}$ $C_{24'}$	1.433(10) 1.526(10)
C_{0}	1.509 (6)	$C_{23} = C_{24}$	1.520 (10)
	0.9500	$C_{23} - \Pi_{23} A$	1.0000
C10 C15	0.9300	$C_{24} = H_{24}C$	0.9900
	1.383 (8)	C24—H24D	0.9900
C10C11	1.398 (8)		
C4—O2—C3	117.8 (4)	C13—C12—H12	120.8
C16—O3—C13	120.6 (4)	C14—C13—C12	120.2 (6)
C19—O4—C22	118.8 (5)	C14—C13—O3	115.6 (5)
C2—O1—C1	59.4 (6)	C12—C13—O3	124.0 (6)
C2—C1—O1	59.0 (5)	C13—C14—C15	119.1 (5)
C2—C1—H1B	117.9	C13—C14—H14	120.4
O1—C1—H1B	117.9	C15—C14—H14	120.4
C2—C1—H1A	117.9	C10—C15—C14	123.5 (5)
O1—C1—H1A	117.9	C10—C15—H15	118.3
H1B—C1—H1A	115.0	C14—C15—H15	118.3
O1—C2—C1	61.6 (5)	C21—C16—O3	115.8 (5)
O1—C2—C3	112.2 (9)	C21—C16—C17	120.0 (5)
C1—C2—C3	114.5 (10)	O3—C16—C17	123.9 (5)
O1—C2—H2	118.6	C18—C17—C16	119.9 (5)
С1—С2—Н2	118.6	C18—C17—H17	120.0
С3—С2—Н2	118.6	C16—C17—H17	120.0
C2'—O1'—C1'	63.0 (9)	C17—C18—C19	119.4 (6)
O1'—C1'—C2'	57.8 (6)	C17—C18—H18	120.3
O1′—C1′—H1′B	118.0	C19—C18—H18	120.3

C2′—C1′—H1′B	118.0	C20—C19—O4	116.6 (5)
01′—C1′—H1′A	118.0	C20-C19-C18	119.9 (6)
C2'—C1'—H1'A	118.0	O4—C19—C18	123.5 (5)
H1′B—C1′—H1′A	115.2	C19—C20—C21	120.9 (5)
O1'—C2'—C1'	59.2 (6)	С19—С20—Н20	119.6
O1'—C2'—C3	118.9 (16)	С21—С20—Н20	119.6
C1'—C2'—C3	114.3 (16)	C16—C21—C20	119.8 (5)
O1'—C2'—H2'	117.2	C16—C21—H21	120.1
C1'—C2'—H2'	117.2	C20—C21—H21	120.1
C3—C2'—H2'	117.2	04-C22-C23	105.8 (5)
02-C3-C2	104.2 (6)	$04-C^{2}-C^{2}3'$	104.5(14)
02-C3-C2'	105.6 (8)	O4-C22-H22B	110.6
02—C3—H3A	110.9	C23—C22—H22B	110.6
C2—C3—H3A	110.9	$C_{23}' - C_{22} - H_{22B}$	80.3
C2'-C3-H3A	75.9	O4-C22-H22A	110.6
Ω^2 C^3 H^3B	110.9	C^{23} C^{22} H^{22A}	110.6
$C_2 = C_3 = H_3 B$	110.9	$C_{23}' - C_{22} - H_{22}A$	136.9
C2' = C3 = H3B	137.7	H_{22B} C_{22} H_{22A}	108 7
$H_{3}A = C_{3} = H_{3}B$	108.9	$C_{24} = 05 = C_{23}$	61 8 (4)
$C_{5} - C_{4} - O_{2}^{2}$	125.1 (5)	05-023-024	59 0 (4)
$C_{5} - C_{4} - C_{9}$	119 3 (5)	$05 - C^{23} - C^{22}$	110.8(7)
02-C4-C9	115.6 (5)	C_{24} C_{23} C_{22}	110.0(7) 114 1 (8)
$C_{4} - C_{5} - C_{6}$	119.6 (5)	05-023-H23	119.5
C4-C5-H5	120.2	C_{24} C_{23} H_{23}	119.5
С4—С5—Н5	120.2	$C_{2}^{2} = C_{2}^{2} = H_{2}^{2}$	119.5
C_{5} C_{6} C_{7}	120.2	05-024-023	59 2 (4)
$C_5 = C_6 = H_6$	118 7	05 - 024 + 025	117 Q
C7_C6_H6	118.7	C_{23} C_{24} H_{24B}	117.9
$C_{1}^{2} = C_{1}^{2} = C_{1}^{2}$	115.7	05 C24 H24A	117.9
$C_8 = C_7 = C_1^{-10}$	113.4(0) 122.3(5)	$C_{24} = H_{24} A$	117.9
$C_{8} = C_{7} = C_{10}$	122.3(5)	H_{24} H	117.9
$C_0 = C_1 $	122.3(5) 121.0(5)	1124B - C24 - 1124A	64.3 (6)
$C_{2} = C_{3} = C_{1}$	121.9 (5)	$C_{23} = 03 = C_{24}$	58 0 (6)
$C_7 = C_8 = H_8$	119.0	05 - C23 - C24	38.0(0)
$C^{2} = C^{2} = C^{2}$	119.0	$C_{23} = C_{23} = C_{22}$	110(2) 123(3)
C_{8} C_{9} H_{0}	121.1(3)	$C_{24} = C_{23} = C_{22}$	125 (5)
C_{0} C_{0} H_{0}	119.4	$C_{23} - C_{23} - C_{23} - C_{23}$	115.1
$C_{4} - C_{9} - H_{9}$	119.4	$C_{24} = C_{23} = H_{23}A$	115.1
C15 - C10 - C11	113.3(3) 122.1(5)	C_{22} — C_{23} — Π_{23} A	113.1 577(5)
$C_{13} = C_{10} = C_7$	122.1(3)	03 - 024 - 023	<i>37.7</i> (<i>3</i>)
	122.0 (5)	$03 - C_{24} - H_{24}C_{24}$	118.0
C12 $C11$ $U11$	123.3 (5)	$C_{23} = C_{24} = H_{24}C_{23}$	118.0
	110.3	$O_3 - C_2 4 - H_2 4 D$	118.0
$C_{10} - C_{11} - H_{11}$	118.3	$U_{23} = U_{24} = H_{24} D$	118.0
$C_{11} = C_{12} = C_{13}$	110.3 (0)	$\Pi_{24} - U_{24} - \Pi_{24} D$	115.2
UII—UI2—HI2	120.8		
C1 - O1 - C2 - C3	106 7 (11)	C16-03-C13-C14	1540(5)
01-C1-C2-C3	-1031(10)	$C_{16} = 03 = C_{13} = C_{14}$	-316(8)
01 01 02 03	100,1 (10)	010 05 015 012	51.0 (0)

C1'C2'C3	-103 (2)	C12—C13—C14—C15	1.5 (9)
O1'-C1'-C2'-C3	110.3 (19)	O3—C13—C14—C15	176.2 (5)
C4—O2—C3—C2	-174.2 (6)	C11—C10—C15—C14	-0.9 (8)
C4—O2—C3—C2′	146.9 (9)	C7-C10-C15-C14	179.3 (5)
O1—C2—C3—O2	-161.3 (8)	C13—C14—C15—C10	-0.3 (9)
C1—C2—C3—O2	-93.5 (9)	C13-03-C16-C21	147.4 (5)
O1—C2—C3—C2′	-64.0 (15)	C13—O3—C16—C17	-38.3 (8)
C1—C2—C3—C2′	3.8 (13)	C21—C16—C17—C18	-0.5 (8)
O1'-C2'-C3-O2	163.7 (14)	O3—C16—C17—C18	-174.6 (5)
C1′—C2′—C3—O2	96.8 (14)	C16—C17—C18—C19	0.1 (8)
O1'-C2'-C3-C2	70.6 (16)	C22—O4—C19—C20	-178.4 (6)
C1′—C2′—C3—C2	3.7 (11)	C22—O4—C19—C18	1.3 (9)
C3—O2—C4—C5	0.8 (9)	C17—C18—C19—C20	0.7 (9)
C3—O2—C4—C9	-176.4 (6)	C17—C18—C19—O4	-178.9 (5)
O2—C4—C5—C6	-177.9 (5)	O4-C19-C20-C21	178.5 (5)
C9—C4—C5—C6	-0.8 (9)	C18—C19—C20—C21	-1.2 (9)
C4—C5—C6—C7	-0.7 (9)	O3—C16—C21—C20	174.6 (5)
C5—C6—C7—C8	1.0 (8)	C17—C16—C21—C20	0.1 (8)
C5—C6—C7—C10	-179.1 (5)	C19—C20—C21—C16	0.8 (9)
C6—C7—C8—C9	0.2 (8)	C19—O4—C22—C23	-175.6 (5)
C10—C7—C8—C9	-179.7 (5)	C19—O4—C22—C23′	149.6 (13)
C7—C8—C9—C4	-1.7 (9)	C24—O5—C23—C22	106.3 (8)
C5—C4—C9—C8	2.0 (9)	O4—C22—C23—O5	-155.6 (6)
O2—C4—C9—C8	179.4 (5)	C23'—C22—C23—O5	-63 (3)
C8—C7—C10—C15	-3.2 (8)	O4—C22—C23—C24	-91.2 (7)
C6—C7—C10—C15	176.9 (6)	C23'—C22—C23—C24	1 (2)
C8—C7—C10—C11	177.1 (6)	C22—C23—C24—O5	-100.7 (8)
C6—C7—C10—C11	-2.8 (8)	C24'—O5'—C23'—C22	113 (4)
C15—C10—C11—C12	1.0 (8)	O4—C22—C23'—O5'	107 (2)
C7—C10—C11—C12	-179.2 (5)	C23—C22—C23'—O5'	10.7 (14)
C10-C11-C12-C13	0.1 (9)	O4—C22—C23'—C24'	176 (2)
C11—C12—C13—C14	-1.4 (9)	C23—C22—C23'—C24'	79 (2)
C11—C12—C13—O3	-175.6 (5)	C22—C23'—C24'—O5'	-105 (3)