organic compounds

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Tuberostemoamide hemihydrate

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Key indicators: single-crystal X-ray study; T = 298 K; mean σ (C–C) = 0.005 Å; R factor = 0.050; wR factor = 0.142; data-to-parameter ratio = 11.7.

In the crystal structure of the title compound {systematic (1'S,2R,2'R,3'S,6'R)-3'-ethyl-4-methyl-5H-5'-oxa-10'name: azaspiro[furan-2,4'-tricyclo[8.3.0.0^{2,6}]tridecane]-5,11'-dione hemihydrate}, $C_{17}H_{23}NO_4 \cdot 0.5H_2O$, the asymmetric unit contains two molecules of tuberostemoamide with similar conformations and one water molecule. The tuberostemoamide molecule is composed of one seven-membered ring (A)and three five-membered rings (B, C and D). Ring A exists in a chair conformation, both rings B and C exist in envelope conformations, and ring D is almost planar with a mean deviation of 0.0143 (4) Å in one molecule and 0.0095 (3) Å in the other.. The dihedral angles between the planes of rings Cand D are 75.1 (3)° in one molecule and 74.5 (3)° for the other. The solvent water molecule links the tuberostemoamide molecules through $O-H \cdots O(\text{ketone})$ hydrogen bonds. Weak C-H···O interactions are also present, involving both the water molecule and a heterocyclic ether O-atom acceptor.

Related literature

For general background, see: Pilli & Ferreira de Oliveira (2000); Jiang et al. (2006). For the biological activity of Stemona alkaloids, see: Xu et al. (2010); Lin et al. (2008); Hu et al. (2009).



Experimental

Crystal data

C17H23NO4.0.5H2O $M_r = 314.37$ Orthorhombic, $P2_12_12_1$ a = 8.6412 (2) Å b = 10.7998 (2) Å c = 36.1685 (7) Å

Data collection

Oxford Diffraction Gemini S Ultra CCD diffractometer Absorption correction: multi-scan (SADABS; Sheldrick, 2004) $T_{\min} = 0.822, T_{\max} = 1.000$

Refinement

$R[F^2 > 2\sigma(F^2)] = 0.050$	H atoms treated by a mixture of
$wR(F^2) = 0.142$	independent and constrained
S = 1.06	refinement
4837 reflections	$\Delta \rho_{\rm max} = 0.51 \ {\rm e} \ {\rm \AA}^{-3}$
412 parameters	$\Delta \rho_{\rm min} = -0.24 \text{ e} \text{ Å}^{-3}$
2 restraints	Absolute structure: Flack (1983),
	1743 Friedel pairs
	Flack parameter: -0.1 (2)

 $V = 3375.36 (12) \text{ Å}^3$

 $0.42 \times 0.30 \times 0.27 \text{ mm}$

8573 measured reflections

4837 independent reflections

4514 reflections with I > 2I)

Cu Ka radiation

 $\mu = 0.73 \text{ mm}^{-1}$

T = 298 K

 $R_{\rm int} = 0.021$

Z = 8

Table 1 Hydrogen-bond geometry (Å, °).

D-H	$H \cdot \cdot \cdot A$	$D \cdots A$	$D - \mathbf{H} \cdots A$
0.81	1.98	2.796 (3)	175
0.83	1.97	2.784 (3)	171
0.97	2.58	3.545 (4)	178
0.98	2.58	3.450 (4)	149
	<i>D</i> -H 0.81 0.97 0.98	$\begin{array}{c c} D-H & H \cdots A \\ \hline 0.81 & 1.98 \\ 0.83 & 1.97 \\ 0.97 & 2.58 \\ 0.98 & 2.58 \\ \hline \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

Symmetry codes: (i) $x + \frac{3}{2}, -y + \frac{3}{2}, -z$; (ii) $x - \frac{1}{2}, -y + \frac{1}{2}, -z$.

Data collection: SMART (Bruker, 1998); cell refinement: SAINT (Bruker, 1998); data reduction: SAINT; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: XP (Bruker, 1998); software used to prepare material for publication: SHELXTL (Sheldrick, 2008).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: ZS2152).

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supporting information

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Tuberostemoamide hemihydrate

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S1. Comment

The title compound $2(C_{17}H_{23}NO_4)$. H₂O (Fig. 1) is a hydrate of tuberostemoamide which has been isolated from the roots of Stemona tuberosa. This plant is a rich source of Stemona alkaloids (Pilli & Ferreira de Oliveira, 2000; Jiang *et al.*, 2006) with anti-tussive activity (Xu *et al.*, 2010). Although the phytochemical properties of tuberostemoamide have been studied Hu *et al.*, 2009); Lin *et al.*, 2008) the crystal structure has not previously been reported. In this study, we report the structure of tuberostemoamide hemihydrate.

The asymmetric unit contains two molecules of tuberostemoamide [(1) and (2)] with similar conformations and one water molecule (Fig. 1). The tuberostemoamide molecule is composed of one seven-membered ring (*A*) and three five-membered rings (*B*, *C* and *D*). Ring *A* exists in a chair conformation. Ring *B* exists in an envelope conformation with C1 displaced by 0.4695 Å from the least-squares plane of the remaining four atoms (C2, C3, N4 and C9*A*), and the corresponding value for molecule (2) is 0.4868 Å. Ring *C* also exhibits an envelope conformation with C10 displaced by 0.5930 Å from the least-squares plane of the remaining four atoms (C8, C8, O2 and C11), and the corresponding value for molecule (2) is 0.5886 Å. Ring *D* is planar with a mean deviation 0.0142 Å for (1) and 0.0101 Å for (2). The dihedral angles between the planes of the rings *C* and *D* in molecule (1) is 75.1 (3)° and 74.5 (3)° for molecule (2). The absolute configuration for the compound was not determined with certainty in this analysis.

The water molecule links the tuberostemoamide molecules through O—H···O(ketone) hydrogen bonds (Table 1) with only weak intermolecular C—H···O interactions present, involving both the water molecule and a hetero-ring ether O-acceptor (Fig. 2).

S2. Experimental

The dry ground herbal sample Radix stemonae (8.0 kg) was refluxed with 95% EtOH. After evaporation of the solvent, the crude extract was acidified with 4% HCl and filtered, and the filtrate was washed with diethyl ether (800 ml). The pH of the aqueous layer was raised to 9 with aqueous ammonia (35%) and then extracted with Et₂O (800 ml). The Et₂O layer was evaporated to afford the crude alkaloids (25 g), which was subjected to column chromatography over silica gel, and eluted with cyclohexane-ethyl acetate (10:1 to 0:1) to yield fourteen fractions. Fraction 8 (4 g) was subjected to reverse phase silica gel chromatography to yield seven subfractions, after which the second subfraction (60% CH₃CN, 8 mg) was purified by preparative HPLC eluted by 25% CH₃CN to yield tuberostemoamide (4 mg). The colorless crystals were obtained from a methanol solution at room temperature.

S3. Refinement

The C-bound H atoms were positioned geometrically and were included in the refinement in the riding-model approximation, with C—H = 0.96 Å (CH₃) and $U_{iso}(H) = 1.5U_{eq}(C)$; 0.97 Å (CH₂) and $U_{iso}(H) = 1.2U_{eq}(C)$; 0.93 Å (aryl H) and $U_{iso}(H) = 1.2U_{eq}(C)$; O—H = 0.82 Å and $U_{iso}(H) = 1.5U_{eq}(O)$. In the absence of a suitable heavy atom the Flack

parameter determined for the parent compound [-0.1 (2) for 1743 Friedel pairs] is not definitive of the absolute configuration of tuberostemoamide but for the chosen enantiomer, the 5 chiral centers of both independent molecules are C8(R), C9(R), C9A(S), C10(S), C11(R).



Figure 1

The molecular structure of the title compound showing 30% probability displacement ellipsoids and the atom-numbering scheme. Inter-species hydrogen bonds are shown as dashed lines.



Figure 2

Packing diagram viewed down the *a* axis showing O—H…O and C—H…O hydrogen bonds as dashed lines.

(1'S,2R,2'R,3'S,6'R)-3'-ethyl-4-methyl- 5H-5'-oxa-10'-azaspiro[furan-2,4'-tricyclo[8.3.0.0^{2,6}]tridecane]- 5,11'dione hemihydrate

Crystal data

 $C_{17}H_{23}NO_4 \cdot 0.5H_2O$ $M_r = 314.37$ Orthorhombic, $P2_12_12_1$ Hall symbol: P 2ac 2ab a = 8.6412 (2) Å b = 10.7998 (2) Å c = 36.1685 (7) Å V = 3375.36 (12) Å³ Z = 8 F(000) = 1352 $D_x = 1.237 \text{ Mg m}^{-3}$ Cu K\alpha radiation, $\lambda = 1.54184 \text{ Å}$ Cell parameters from 4774 reflections $\theta = 3.7-62.5^{\circ}$ $\mu = 0.73 \text{ mm}^{-1}$ T = 298 KBlock, colorless $0.42 \times 0.30 \times 0.27 \text{ mm}$ Data collection

Oxford Diffraction Gemini S Ultra CCD diffractometer Radiation source: fine-focus sealed tube Graphite monochromator ω scans Absorption correction: multi-scan (<i>SADABS</i> ; Sheldrick, 2004) $T_{min} = 0.822, T_{max} = 1.000$ <i>Refinement</i>	8573 measured reflections 4837 independent reflections 4514 reflections with $I > 2 \tilde{I}$) $R_{int} = 0.021$ $\theta_{max} = 62.6^{\circ}, \theta_{min} = 4.3^{\circ}$ $h = -9 \rightarrow 9$ $k = -12 \rightarrow 10$ $l = -19 \rightarrow 41$
Refinement on F^2	Hydrogen site location: inferred from
Least-squares matrix: full	neighbouring sites
$R[F^2 > 2\sigma(F^2)] = 0.050$	H atoms treated by a mixture of independent
$wR(F^2) = 0.142$	and constrained refinement
S = 1.06	$w = 1/[\sigma^2(F_o^2) + (0.0913P)^2 + 0.4948P]$
4837 reflections	where $P = (F_o^2 + 2F_c^2)/3$
412 parameters	$(\Delta/\sigma)_{max} < 0.001$
2 restraints	$\Delta\rho_{max} = 0.51$ e Å ⁻³
Primary atom site location: structure-invariant	$\Delta\rho_{min} = -0.24$ e Å ⁻³
direct methods	Absolute structure: Flack (1983), 1743 Friedel
Secondary atom site location: difference Fourier	pairs
map	Absolute structure parameter: -0.1 (2)

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $(Å^2)$

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	
01′	0.3987 (3)	0.6908 (2)	0.08626 (7)	0.0818 (7)	
O2′	0.9749 (2)	0.7450 (2)	0.18688 (6)	0.0688 (6)	
O3′	1.0512 (3)	0.9441 (2)	0.20168 (6)	0.0792 (7)	
O4′	1.2437 (4)	1.0530 (3)	0.22680 (11)	0.1210 (12)	
C1′	0.4852 (4)	0.7634 (3)	0.18058 (9)	0.0663 (8)	
H1'A	0.4397	0.8047	0.2018	0.080*	
H1′B	0.5442	0.6924	0.1890	0.080*	
C2′	0.3601 (4)	0.7249 (4)	0.15240 (10)	0.0828 (10)	
H2'A	0.3262	0.6405	0.1567	0.099*	
H2′B	0.2713	0.7797	0.1537	0.099*	
C3′	0.4403 (3)	0.7360 (3)	0.11593 (9)	0.0614 (7)	
N4′	0.5691 (3)	0.8034 (2)	0.12056 (6)	0.0530 (5)	
C5′	0.6762 (4)	0.8299 (3)	0.09050 (7)	0.0583 (7)	
H5′A	0.7141	0.9140	0.0931	0.070*	
H5′B	0.6214	0.8244	0.0672	0.070*	

C6′	0.8127 (4)	0.7416 (3)	0.08984 (7)	0.0617 (7)
H6'A	0.7732	0.6575	0.0902	0.074*
H6′B	0.8673	0.7527	0.0666	0.074*
C7′	0.9266 (3)	0.7555 (3)	0.12079 (8)	0.0612 (7)
H7'A	0.9796	0.8341	0.1181	0.073*
H7′B	1.0035	0.6904	0.1188	0.073*
C8′	0.8538 (3)	0.7500 (3)	0.15902 (7)	0.0513 (6)
H8′A	0.7900	0.6752	0.1609	0.062*
C9′	0.7566 (3)	0.8615 (2)	0.16928 (7)	0.0477 (6)
H9'A	0.8006	0.9338	0.1567	0.057*
C9A'	0.5859 (3)	0.8521 (2)	0.15822 (7)	0.0514 (6)
H9AB	0.5397	0.9349	0.1592	0.062*
C10′	0.7858 (4)	0.8767 (3)	0.21083 (7)	0.0547 (6)
H10B	0.7249	0.8140	0.2239	0.066*
C11′	0.9562 (4)	0.8396 (3)	0.21282 (8)	0.0596 (7)
C12′	1.0220 (4)	0.8032 (3)	0.24871 (9)	0.0681 (8)
H12B	0.9854	0.7383	0.2632	0.082*
C13′	1.1403 (4)	0.8751 (4)	0.25765 (9)	0.0762 (9)
C14′	1.1569 (4)	0.9670 (4)	0.22847 (11)	0.0810 (10)
C15′	1.2413 (6)	0.8803 (6)	0.29114 (12)	0.1187 (17)
H15D	1.2159	0.8129	0.3073	0.178*
H15E	1.2251	0.9574	0.3038	0.178*
H15F	1.3478	0.8739	0.2838	0.178*
C16′	0.7445 (6)	1.0033 (4)	0.22668 (10)	0.0858 (11)
H16C	0.8230	1.0618	0.2188	0.103*
H16D	0.6473	1.0294	0.2158	0.103*
C17′	0.7300 (10)	1.0123 (6)	0.26649 (16)	0.157 (3)
H17D	0.7049	1.0960	0.2732	0.236*
H17E	0.8260	0.9891	0.2779	0.236*
H17F	0.6493	0.9579	0.2748	0.236*
01	-0.0168 (3)	0.5873 (2)	0.01640 (7)	0.0779 (6)
O2	-0.5911 (2)	0.31108 (18)	-0.03973 (5)	0.0528 (4)
03	-0.6774 (2)	0.36455 (16)	-0.09836 (5)	0.0564 (5)
04	-0.8917 (3)	0.3499 (2)	-0.13237 (6)	0.0742 (6)
C1	-0.1041 (3)	0.3420 (3)	-0.04581 (9)	0.0591 (7)
H1A	-0.1618	0.2844	-0.0305	0.071*
H1B	-0.0599	0.2974	-0.0665	0.071*
C2	0.0210(3)	0.4071 (3)	-0.02354 (9)	0.0595 (7)
H2A	0.0564	0.3556	-0.0033	0.071*
H2B	0.1087	0.4283	-0.0390	0.071*
C3	-0.0582 (3)	0.5213 (3)	-0.00945 (8)	0.0545 (6)
N4	-0.1863 (2)	0.5401 (2)	-0.02972 (6)	0.0515 (5)
C5	-0.2939 (3)	0.6411 (3)	-0.02211 (9)	0.0610(7)
H5A	-0.3387	0.6697	-0.0452	0.073*
H5B	-0.2378	0.7097	-0.0111	0.073*
C6	-0.4218 (3)	0.6016 (3)	0.00366 (9)	0.0610(7)
H6A	-0.4763	0.6751	0.0120	0.073*
H6B	-0.3755	0.5633	0.0252	0.073*

C7	-0.5400 (3)	0.5116 (3)	-0.01270 (8)	0.0544 (7)
H7A	-0.6114	0.4867	0.0066	0.065*
H7B	-0.5992	0.5543	-0.0316	0.065*
C8	-0.4694 (3)	0.3976 (2)	-0.02940 (7)	0.0437 (5)
H8A	-0.4020	0.3583	-0.0111	0.052*
C9	-0.3777 (3)	0.4177 (2)	-0.06508 (7)	0.0457 (6)
H9A	-0.4245	0.4879	-0.0781	0.055*
C9A	-0.2073 (3)	0.4480 (2)	-0.05906 (7)	0.0493 (6)
H9AA	-0.1645	0.4812	-0.0821	0.059*
C10	-0.4123 (3)	0.3013 (3)	-0.08746 (7)	0.0529 (6)
H10A	-0.3504	0.2334	-0.0772	0.063*
C11	-0.5799 (3)	0.2795 (2)	-0.07690 (7)	0.0500 (6)
C12	-0.6566 (3)	0.1570 (2)	-0.08304 (8)	0.0576 (7)
H12A	-0.6192	0.0819	-0.0742	0.069*
C13	-0.7846 (3)	0.1697 (2)	-0.10266 (7)	0.0536 (6)
C14	-0.7969 (3)	0.3011 (2)	-0.11322 (7)	0.0523 (6)
C15	-0.9043 (4)	0.0787 (3)	-0.11504 (10)	0.0691 (8)
H15A	-0.8783	-0.0022	-0.1059	0.104*
H15B	-0.9079	0.0770	-0.1416	0.104*
H15C	-1.0036	0.1028	-0.1056	0.104*
C16	-0.3768 (5)	0.3105 (4)	-0.12896 (9)	0.0858 (11)
H16A	-0.4557	0.3617	-0.1404	0.103*
H16B	-0.2787	0.3530	-0.1319	0.103*
C17	-0.3690 (9)	0.1966 (7)	-0.14874 (13)	0.158 (3)
H17A	-0.3458	0.2129	-0.1742	0.238*
H17B	-0.4666	0.1546	-0.1470	0.238*
H17C	-0.2892	0.1455	-0.1383	0.238*
O1W	0.1914 (4)	0.5014 (3)	0.06972 (10)	0.1025 (9)
H1WA	0.128 (6)	0.529 (6)	0.0552 (14)	0.154*
H1WB	0.256 (6)	0.553 (5)	0.0765 (16)	0.154*

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	U ²³
01′	0.0742 (14)	0.0875 (15)	0.0837 (14)	-0.0204 (13)	-0.0242 (12)	-0.0017 (13)
O2′	0.0611 (12)	0.0800 (13)	0.0653 (11)	0.0199 (11)	-0.0105 (10)	-0.0137 (10)
O3′	0.0698 (14)	0.0857 (15)	0.0821 (14)	-0.0206 (13)	-0.0149 (12)	0.0174 (13)
O4′	0.091 (2)	0.112 (2)	0.160 (3)	-0.042 (2)	-0.032 (2)	0.014 (2)
C1′	0.0494 (15)	0.082 (2)	0.0676 (16)	-0.0068 (16)	0.0064 (14)	0.0036 (15)
C2′	0.0488 (17)	0.102 (3)	0.098 (2)	-0.0145 (18)	0.0042 (17)	0.005 (2)
C3′	0.0522 (15)	0.0579 (16)	0.0743 (18)	-0.0020 (14)	-0.0125 (15)	0.0050 (14)
N4′	0.0514 (12)	0.0490 (11)	0.0584 (12)	-0.0085 (10)	-0.0059 (10)	0.0023 (10)
C5′	0.0723 (18)	0.0559 (15)	0.0468 (13)	-0.0160 (15)	-0.0060 (13)	0.0078 (11)
C6′	0.0733 (19)	0.0614 (16)	0.0504 (13)	-0.0130 (16)	0.0116 (14)	-0.0043 (12)
C7′	0.0525 (15)	0.0713 (17)	0.0600 (15)	-0.0030 (14)	0.0116 (14)	-0.0109 (14)
C8′	0.0498 (14)	0.0514 (13)	0.0527 (13)	0.0004 (12)	-0.0008 (12)	-0.0050 (11)
C9′	0.0488 (14)	0.0443 (13)	0.0499 (12)	-0.0011 (11)	0.0021 (11)	-0.0011 (10)
C9A′	0.0452 (14)	0.0500 (14)	0.0590 (13)	0.0032 (12)	-0.0023 (11)	-0.0015 (12)

C10′	0.0597 (16)	0.0550 (15)	0.0495 (13)	-0.0005 (14)	0.0021 (12)	-0.0034 (12)
C11′	0.0627 (17)	0.0599 (17)	0.0562 (14)	-0.0039 (15)	-0.0038 (13)	-0.0001 (13)
C12′	0.078 (2)	0.0655 (18)	0.0606 (15)	-0.0022 (17)	-0.0118 (15)	0.0012 (14)
C13′	0.077 (2)	0.081 (2)	0.0708 (18)	-0.0006 (19)	-0.0223 (17)	-0.0044 (17)
C14′	0.063 (2)	0.083 (2)	0.097 (3)	-0.0072 (19)	-0.0125 (18)	-0.006 (2)
C15′	0.115 (4)	0.149 (4)	0.092 (3)	-0.008 (3)	-0.049 (3)	-0.011 (3)
C16′	0.113 (3)	0.071 (2)	0.073 (2)	0.017 (2)	0.002 (2)	-0.0231 (16)
C17′	0.199 (7)	0.147 (5)	0.126 (4)	0.035 (5)	0.007 (5)	-0.050 (4)
01	0.0652 (13)	0.0750 (14)	0.0937 (15)	-0.0013 (12)	-0.0213 (12)	-0.0129 (12)
O2	0.0478 (10)	0.0594 (10)	0.0513 (9)	-0.0123 (9)	0.0013 (8)	-0.0019 (8)
O3	0.0622 (11)	0.0405 (9)	0.0666 (10)	-0.0009 (9)	-0.0147 (9)	0.0045 (8)
O4	0.0718 (13)	0.0615 (12)	0.0894 (14)	-0.0005 (11)	-0.0272 (12)	0.0171 (11)
C1	0.0472 (14)	0.0535 (15)	0.0766 (17)	0.0057 (13)	0.0086 (14)	-0.0014 (13)
C2	0.0387 (13)	0.0603 (16)	0.0796 (17)	0.0042 (12)	0.0029 (13)	0.0114 (14)
C3	0.0432 (13)	0.0489 (14)	0.0715 (16)	-0.0047 (12)	-0.0008 (13)	0.0056 (13)
N4	0.0423 (11)	0.0430 (11)	0.0694 (13)	0.0004 (10)	-0.0003 (10)	0.0047 (10)
C5	0.0508 (14)	0.0412 (13)	0.0910 (19)	0.0048 (12)	-0.0096 (15)	-0.0014 (13)
C6	0.0551 (16)	0.0517 (15)	0.0762 (17)	0.0089 (13)	-0.0022 (14)	-0.0142 (14)
C7	0.0451 (14)	0.0561 (15)	0.0621 (15)	0.0054 (12)	0.0043 (12)	-0.0048 (12)
C8	0.0390 (12)	0.0449 (12)	0.0471 (12)	-0.0019 (11)	-0.0027 (10)	0.0023 (10)
C9	0.0458 (12)	0.0465 (13)	0.0449 (12)	0.0005 (11)	0.0003 (11)	0.0059 (10)
C9A	0.0465 (13)	0.0511 (14)	0.0504 (13)	-0.0016 (12)	0.0086 (11)	0.0050 (11)
C10	0.0575 (15)	0.0511 (13)	0.0501 (13)	0.0047 (13)	0.0009 (12)	-0.0020 (11)
C11	0.0543 (15)	0.0437 (13)	0.0520 (13)	0.0039 (12)	-0.0072 (12)	0.0008 (11)
C12	0.0657 (17)	0.0416 (13)	0.0656 (15)	0.0039 (13)	-0.0101 (14)	0.0035 (12)
C13	0.0589 (15)	0.0397 (13)	0.0621 (14)	0.0011 (12)	-0.0061 (13)	-0.0011 (11)
C14	0.0556 (15)	0.0461 (13)	0.0553 (13)	0.0025 (13)	-0.0057 (13)	0.0019 (11)
C15	0.0646 (18)	0.0528 (16)	0.090 (2)	-0.0069 (15)	-0.0156 (17)	-0.0028 (15)
C16	0.102 (3)	0.097 (3)	0.0583 (17)	0.010 (2)	0.0197 (19)	-0.0043 (17)
C17	0.192 (6)	0.202 (6)	0.081 (3)	0.027 (6)	0.009 (4)	-0.047 (4)
O1W	0.104 (2)	0.0833 (18)	0.120 (2)	-0.0337 (17)	-0.0342 (18)	0.0232 (15)

Geometric parameters (Å, °)

01′—C3′	1.233 (4)	O2—C11	1.390 (3)
O2'—C11'	1.396 (4)	O2—C8	1.455 (3)
O2'—C8'	1.454 (3)	O3—C14	1.351 (3)
O3'—C14'	1.354 (4)	O3—C11	1.468 (3)
O3'—C11'	1.453 (4)	O4—C14	1.195 (3)
O4'—C14'	1.195 (5)	C1—C2	1.521 (4)
C1'—C9A'	1.525 (4)	C1—C9A	1.528 (4)
C1′—C2′	1.542 (5)	C1—H1A	0.9700
С1'—Н1'А	0.9700	C1—H1B	0.9700
С1′—Н1′В	0.9700	C2—C3	1.499 (4)
C2'—C3'	1.495 (5)	C2—H2A	0.9700
C2'—H2'A	0.9700	C2—H2B	0.9700
C2'—H2'B	0.9700	C3—N4	1.343 (4)
C3'—N4'	1.340 (4)	N4—C5	1.460 (3)

N4'—C5'	1.456 (4)	N4—C9A	1.466 (3)
N4'—C9A'	1.467 (3)	C5—C6	1.507 (4)
C5'—C6'	1.517 (4)	C5—H5A	0.9700
С5'—Н5'А	0.9700	С5—Н5В	0.9700
С5′—Н5′В	0.9700	C6—C7	1.529 (4)
C6'—C7'	1.498 (4)	C6—H6A	0.9700
С6'—Н6'А	0.9700	C6—H6B	0.9700
С6'—Н6'В	0.9700	C7—C8	1.501 (4)
C7′—C8′	1.520 (4)	C7—H7A	0.9700
С7′—Н7′А	0.9700	C7—H7B	0.9700
С7'—Н7'В	0.9700	C8—C9	1.530 (3)
C8′—C9′	1.515 (4)	C8—H8A	0.9800
С8′—Н8′А	0.9800	C9—C10	1.524 (4)
C9′—C9A′	1.532 (4)	C9—C9A	1.524 (4)
C9′—C10′	1.533 (3)	С9—Н9А	0.9800
С9'—Н9'А	0.9800	С9А—Н9АА	0.9800
С9А'—Н9АВ	0.9800	C10—C11	1.517 (4)
C10'—C16'	1.525 (4)	C10—C16	1.535 (4)
C10'—C11'	1.528 (4)	C10—H10A	0.9800
C10′—H10B	0.9800	C11—C12	1.496 (4)
C11'-C12'	1.470 (4)	C12—C13	1.321 (4)
C12' - C13'	1.324 (5)	C12—H12A	0.9300
C12'—H12B	0.9300	C13— $C14$	1.473 (4)
C13'-C14'	1.456 (5)	C13—C15	1.496 (4)
C13'—C15'	1.494 (5)	C15—H15A	0.9600
C15'—H15D	0.9600	C15—H15B	0.9600
C15'—H15E	0.9600	C15—H15C	0.9600
C15'—H15E	0.9600	C16-C17	1425(7)
C16' - C17'	1 449 (6)	C16—H16A	0.9700
C16' - H16C	0.9700	C16—H16B	0.9700
C_{16} H16D	0.9700	C17—H17A	0.9600
C17'—H17D	0.9700	C17—H17B	0.9600
C17'—H17E	0.9600	C17 - H17C	0.9600
C17' H17E	0.9600	01W H1WA	0.9000
O1 C3	1 229 (4)	O1W H1WB	0.81(2) 0.82(2)
01-03	1.229 (4)		0.82 (2)
C11'O2'C8'	110.8(2)	C14-O3-C11	109 35 (19)
C11' - 02' - C3'	10.0(2)	$C_{1} = 0_{2} = 0_{1}$	109.55(19) 103.5(2)
$C_{14} = 03 = C_{11}$	103.9(3)	$C_2 = C_1 = H_1 \Lambda$	105.5 (2)
C9A = C1 = C2	102.0 (5)	$C_2 - C_1 - H_1 A$	111.1
C_{2} C_{1} H_{1}	111.2	C_{2} C_{1} $H_{1}B$	111.1
$C_2 - C_1 - III A$	111.2	C_{2} C_{1} H_{1B}	111.1
C_{2} C_{1} H_{1} H_{2}	111.2	$H_{1A} = C_{1} = H_{1B}$	100.0
$L_2 - L_1 - III B$	100.2	C_{2}^{2} C_{2}^{2} C_{1}^{1}	109.0
$\begin{array}{cccc} & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & $	107.2 103 7 (2)	$C_3 = C_2 = C_1$	105.0 (2)
$C_3 = C_2 = C_1$	103.7(2)	C_{3} C_{2} H_{2}	111.0
$C_3 - C_2 - \Pi_2 A$	111.0	$C_1 = C_2 = \Pi_2 A$	111.0
$C_1 - C_2 - \Pi_2 A$ $C_{2'} - C_{2'} - \Pi_{2'} D$	111.0	$C_3 - C_2 - \Pi_2 D$	111.0
$U_J - U_L - \Pi_L D$	111.0	$U_1 - U_2 - \Pi_2 D$	111.0

C1′—C2′—H2′B	111.0	H2A—C2—H2B	109.0
H2'A—C2'—H2'B	109.0	O1—C3—N4	124.6 (3)
O1'—C3'—N4'	124.5 (3)	O1—C3—C2	127.0 (3)
O1′—C3′—C2′	126.9 (3)	N4—C3—C2	108.4 (2)
N4′—C3′—C2′	108.6 (3)	C3—N4—C5	122.3 (2)
C3'—N4'—C5'	122.8 (2)	C3—N4—C9A	113.2 (2)
C3'—N4'—C9A'	113.1 (2)	C5—N4—C9A	124.4 (2)
C5'—N4'—C9A'	124.0 (2)	N4—C5—C6	111.9 (2)
N4′—C5′—C6′	112.5 (2)	N4—C5—H5A	109.2
N4′—C5′—H5′A	109.1	C6—C5—H5A	109.2
C6'—C5'—H5'A	109.1	N4—C5—H5B	109.2
N4′—C5′—H5′B	109.1	C6—C5—H5B	109.2
C6'—C5'—H5'B	109.1	H5A—C5—H5B	107.9
H5'A—C5'—H5'B	107.8	C5—C6—C7	115.5 (2)
C7'—C6'—C5'	115.9 (2)	С5—С6—Н6А	108.4
C7'—C6'—H6'A	108.3	С7—С6—Н6А	108.4
C5'-C6'-H6'A	108.3	C5—C6—H6B	108.4
C7'— $C6'$ —H6'B	108.3	C7—C6—H6B	108.4
C5' - C6' - H6'B	108.3	H6A - C6 - H6B	107.5
H6'A - C6' - H6'B	107.4	C8 - C7 - C6	107.5 113.9(2)
C6' - C7' - C8'	113.8 (2)	C8 - C7 - H7A	108.8
C6' - C7' - H7'A	108.8	C6-C7-H7A	108.8
C8' - C7' - H7'A	108.8	C8 - C7 - H7B	108.8
C6' - C7' - H7'B	108.8	C6-C7-H7B	108.8
C8' - C7' - H7'B	108.8	H7A - C7 - H7B	107.7
$H7' \Delta - C7' - H7' B$	107.7	$0^{2}-0^{8}-0^{7}$	107.7 109.7(2)
$\Omega'' - \Omega'' - \Omega''$	107.7 105.0(2)	02 - 03 - 07	109.7(2) 104.40(18)
02 - 03 - 07	109.0(2) 109.5(2)	$C_2 = C_3 = C_2$	104.40(10) 115.7(2)
$C_{2} = C_{3} = C_{7}$	109.5(2) 114.9(2)	$C_{1} = C_{2} = C_{2}$	108.9
$C_{2} = C_{3} = C_{1}$	114.9 (2)	C_{2} C_{8} H_{8A}	108.9
$C_2 - C_3 - H_3 A$	109.1	C_{1} C_{0} C_{0} H_{0} H_{0}	108.9
$C_{2} = C_{3} = H_{3} A$	109.1	C_{3} C_{0} C_{0} C_{0}	106.9
C' = Co' = CoA'	109.1	C_{10} C_{9} C_{8}	110.2(2) 103.2(2)
$C_{0} = C_{0} = C_{0}$	114.0(2) 102.5(2)	C_{10}	103.3(2)
$C_{0} = C_{0} = C_{10}$	103.3(2)	$C_{9}A = C_{9} = C_{8}$	114.2 (2)
$C_{2}^{2} - C_{2}^{2} - C_{10}^{2}$	114.9 (2)	C_{10} C_{20} C	107.5
$C_0 - C_9 - H_9 A$	107.8	$C_{A} = C_{A} = C_{A} = C_{A}$	107.5
$C_{9}A - C_{9} - H_{9}A$	107.8	$C_0 - C_9 - H_9 A$	107.5
C10 - C9 - H9 A	107.8	N4 - C9A - C9	111.0(2)
N4 - C9A - C1	102.2(2)	N4 - C9A - C1	102.1(2)
N4 - C9A - C9	111.2(2)	C_{9}	110.0 (2)
$CI = C9A^{-} = C9^{-}$	116.9 (2)	N4 - C9A - H9AA	108.7
$N4^{\prime}$ —C9 A^{\prime} —H9 AB	108.7	C_{9} C_{9	108.7
$C_1 - C_2 A_2 - H_2 A_2 B_3$	108./	CI - CYA - HYAA	108./
Су'—СУА'—НУАВ	108.7	C11—C10—C9	100.5 (2)
C16' - C10' - C11'	116.3 (3)	C11 - C10 - C16	116.5 (3)
C16'-C10'-C9'	115.2 (3)	C9—C10—C16	115.3 (3)
C11'-C10'-C9'	100.2 (2)	C11—C10—H10A	108.0
C16'—C10'—H10B	108.2	C9—C10—H10A	108.0

C11'—C10'—H10B	108.2	C16—C10—H10A	108.0
C9'—C10'—H10B	108.2	O2—C11—O3	108.5 (2)
O2'—C11'—O3'	108.5 (2)	O2—C11—C12	109.3 (2)
O2'—C11'—C12'	110.7 (3)	O3—C11—C12	102.7 (2)
O3'—C11'—C12'	103.6 (2)	O2—C11—C10	105.8 (2)
O2'—C11'—C10'	105.7 (2)	O3—C11—C10	108.5 (2)
O3'—C11'—C10'	109.1 (2)	C12—C11—C10	121.6 (2)
C12'—C11'—C10'	119.0 (3)	C13—C12—C11	111.0 (2)
C13'—C12'—C11'	110.9 (3)	C13—C12—H12A	124.5
C13'—C12'—H12B	124.5	C11—C12—H12A	124.5
C11′—C12′—H12B	124.5	C12—C13—C14	107.5 (2)
C12'—C13'—C14'	107.4 (3)	C12—C13—C15	132.2 (3)
C12'—C13'—C15'	132.1 (4)	C14—C13—C15	120.4 (2)
C14′—C13′—C15′	120.3 (4)	O4—C14—O3	122.0 (2)
O4'—C14'—O3'	121.9 (4)	O4—C14—C13	128.7 (3)
O4'—C14'—C13'	128.9 (4)	O3—C14—C13	109.3 (2)
O3'—C14'—C13'	109.1 (3)	C13—C15—H15A	109.5
C13'—C15'—H15D	109.5	C13—C15—H15B	109.5
C13'—C15'—H15E	109.5	H15A—C15—H15B	109.5
H15D—C15′—H15E	109.5	C13—C15—H15C	109.5
C13'—C15'—H15F	109.5	H15A—C15—H15C	109.5
H15D—C15′—H15F	109.5	H15B—C15—H15C	109.5
H15E—C15′—H15F	109.5	C17—C16—C10	116.4 (4)
C17'—C16'—C10'	117.0 (4)	C17—C16—H16A	108.2
C17'—C16'—H16C	108.0	C10—C16—H16A	108.2
C10'—C16'—H16C	108.0	C17—C16—H16B	108.2
C17'—C16'—H16D	108.0	C10—C16—H16B	108.2
C10'—C16'—H16D	108.0	H16A—C16—H16B	107.3
H16C—C16′—H16D	107.3	С16—С17—Н17А	109.5
C16'—C17'—H17D	109.5	С16—С17—Н17В	109.5
C16'—C17'—H17E	109.5	H17A—C17—H17B	109.5
H17D—C17′—H17E	109.5	С16—С17—Н17С	109.5
C16'—C17'—H17F	109.5	H17A—C17—H17C	109.5
H17D—C17′—H17F	109.5	H17B—C17—H17C	109.5
H17E—C17′—H17F	109.5	H1WA—O1W—H1WB	113 (6)
$C_{11} = 02 = C_8$	110.84 (19)		110 (0)
011 02 00	110101 (15)		
C9A'—C1'—C2'—C3'	28.3 (4)	C9A—C1—C2—C3	28.4(3)
C1' - C2' - C3' - O1'	1634(3)	$C_1 - C_2 - C_3 - O_1$	1617(3)
C1' - C2' - C3' - N4'	-158(4)	C1 - C2 - C3 - N4	-17.6(3)
01' - C3' - N4' - C5'	-0.5(5)	$01 - C_3 - N_4 - C_5$	-2.0(4)
C2'-C3'-N4'-C5'	178 8 (3)	$C_{2}-C_{3}-N_{4}-C_{5}$	1773(2)
01' - C3' - N4' - C9A'	176.5(3)	01 - C3 - N4 - C9A	1795(2)
C2'-C3'-N4'-C9A'	-42(3)	$C_2 - C_3 - N_4 - C_9 A$	-13(3)
$C_{3'}$ N4' $C_{5'}$ C6'	-97 1 (3)	C_{3} N4 C_{5} C6	-91.8(3)
C9A' - N4' - C5' - C6'	86 2 (3)	C9A - N4 - C5 - C6	86 6 (3)
N4' - C5' - C6' - C7'	-69.8 (3)	N4	-703(3)
$C_{5'} = C_{5'} = C_{5'} = C_{5'}$	53.7 (A)	C_{5}	53 6 (3)
	55.7 (4)		55.0 (5)

C11'—O2'—C8'—C9'	1.6 (3)	C11—O2—C8—C7	124.5 (2)
C11′—O2′—C8′—C7′	125.5 (3)	C11—O2—C8—C9	0.0 (3)
C6'—C7'—C8'—O2'	171.3 (3)	C6—C7—C8—O2	172.6 (2)
C6'—C7'—C8'—C9'	-70.9 (3)	C6—C7—C8—C9	-69.7 (3)
O2'—C8'—C9'—C9A'	-150.5 (2)	O2—C8—C9—C10	-23.5(2)
C7'—C8'—C9'—C9A'	89.2 (3)	C7—C8—C9—C10	-144.1(2)
O2'—C8'—C9'—C10'	-24.5 (3)	O2—C8—C9—C9A	-150.7(2)
C7'—C8'—C9'—C10'	-144.9 (2)	C7—C8—C9—C9A	88.7 (3)
C3'—N4'—C9A'—C1'	22.5 (3)	C3—N4—C9A—C9	144.6 (2)
C5'—N4'—C9A'—C1'	-160.5(2)	C5—N4—C9A—C9	-33.9(3)
C3'—N4'—C9A'—C9'	147.9 (2)	C3—N4—C9A—C1	19.3 (3)
C5'—N4'—C9A'—C9'	-35.1 (3)	C5—N4—C9A—C1	-159.2(2)
C2'—C1'—C9A'—N4'	-30.1(3)	C10—C9—C9A—N4	-164.9(2)
C2'—C1'—C9A'—C9'	-151.7(3)	C8—C9—C9A—N4	-44.8(3)
C8'—C9'—C9A'—N4'	-44.1 (3)	C10—C9—C9A—C1	-48.2(3)
C10'—C9'—C9A'—N4'	-163.9(2)	C8—C9—C9A—C1	72.0 (3)
C8'-C9'-C9A'-C1'	72.6(3)	C2-C1-C9A-N4	-286(3)
C10'-C9'-C9A'-C1'	-47.2(3)	C_2 C_1 C_2	-150.5(2)
C8' - C9' - C10' - C16'	161.7(3)	C9A - C9 - C10 - C11	162.2.(2)
C9A' - C9' - C10' - C16'	-72.5(4)	C8-C9-C10-C11	363(2)
C8' - C9' - C10' - C11'	362(3)	C9A - C9 - C10 - C16	-716(3)
C9A' - C9' - C10' - C11'	161.9(2)	C8-C9-C10-C16	162.5(3)
C8' - 02' - C11' - 03'	-947(3)	C8-O2-C11-O3	-92.3(2)
C8' - 02' - C11' - C12'	152.3 (3)	C8 - O2 - C11 - C12	1564(2)
C8' - 02' - C11' - C10'	22.2(3)	C8 - O2 - C11 - C10	240(3)
C14'-03'-C11'-02'	-1189(3)	$C_{14} = 03 = C_{11} = 02$	-1131(2)
C14' - O3' - C11' - C12'	-13(4)	$C_{14} = 03 = C_{11} = C_{12}$	2 5 (3)
C14' - O3' - C11' - C10'	1263 (3)	$C_{14} = 03 = C_{11} = C_{10}$	1324(2)
C16' - C10' - C11' - O2'	-160.9(3)	C9-C10-C11-O2	-374(2)
C9'-C10'-C11'-02'	-360(3)	$C_{16} - C_{10} - C_{11} - O_{2}^{2}$	-1627(3)
$C_{16} = C_{10} = C_{11} = C_{12}$	-444(3)	C9-C10-C11-O3	78.8 (2)
C9'-C10'-C11'-O3'	80 5 (3)	$C_{16} - C_{10} - C_{11} - O_{3}$	-464(3)
$C_{16'} - C_{10'} - C_{11'} - C_{12'}$	74 0 (4)	C9-C10-C11-C12	-162.6(2)
C9'-C10'-C11'-C12'	-1611(3)	C_{16} C_{10} C_{11} C_{12}	722(4)
02'-011'-012'-013'	115.6(3)	$0^{2}-C^{11}-C^{12}-C^{13}$	$\frac{11111}{3}$
$O_{3'} - C_{11'} - C_{12'} - C_{13'}$	-0.4(4)	03-C11-C12-C13	-40(3)
C10'-C11'-C12'-C13'	-1217(3)	C_{10} C_{11} C_{12} C_{13}	-1253(3)
C11'-C12'-C13'-C14'	121.7(5) 19(4)	C_{11} C_{12} C_{13} C_{14}	38(3)
C11' - C12' - C13' - C15'	1.7(4)	C_{11} C_{12} C_{13} C_{14}	-177.6(3)
C11' - C12' - C13' - C13'	-1759(4)	$C_{11} = C_{12} = C_{13} = C_{13}$	-179.0(3)
C11' - O3' - C14' - C13'	25(4)	$C_{11} = 03 = C_{14} = C_{13}$	-0.5(3)
C12'-C13'-C14'-O4'	2.5 (4)	C12-C13-C14-O4	1763(3)
C15' - C13' - C14' - O4'	-0.6(7)	C12 - C13 - C14 - O4	-25(5)
C12' - C13' - C14' - O3'	-2.7(4)	C_{12} C_{13} C_{14} C_{13}	-2.5(3)
$C_{12} = C_{13} = C_{14} = 03$ $C_{15'} = C_{13'} = C_{14'} = 03'$	-1788(4)	$C_{12} = C_{13} = C_{14} = C_{3}$	2.1(3) 1701(2)
$C_{11} = C_{10} = C_{14} = C_{13}$	-794(6)	$C_{11} = C_{13} = C_{14} = C_{15}$	-784(5)
C0' C10' C16' C17'	163.8 (5)	$C_{10} = C_{10} = C_{10} = C_{17}$	164 2 (5)
$C_{2} = C_{10} = C_{10} = C_{11}$	103.0 (3)	C7-C10-C10-C1/	104.2 (3)

D—H···A	<i>D</i> —Н	H···A	$D \cdots A$	D—H···A
01 <i>W</i> —H1 <i>WA</i> ···O1	0.81	1.98	2.796 (3)	175
O1 <i>W</i> —H1 <i>WB</i> ···O1′	0.83	1.97	2.784 (3)	171
C5'—H5'A···O3 ⁱ	0.97	2.58	3.545 (4)	178
C10—H10 A ···O1 W ⁱⁱ	0.98	2.58	3.450 (4)	149

Hydrogen-bond geometry (Å, °)

Symmetry codes: (i) x+3/2, -y+3/2, -z; (ii) x-1/2, -y+1/2, -z.