

Acta Crystallographica Section E Structure Reports Online

ISSN 1600-5368

# *N,N'*-Bis(3-nitrobenzylidene)-2,2'-[2-(3-nitrophenyl)imidazolidine-1,3-diyl]-diethanamine

## Mohammad Hossein Habibi,<sup>a</sup>\* Narges Abarghooei-Shirazi,<sup>a</sup> Yuki Yamane<sup>b</sup> and Takayoshi Suzuki<sup>b</sup>

<sup>a</sup>Catalysis Division, Department of Chemistry, University of Isfahan, Isfahan 81746-73441, Iran, and <sup>b</sup>Department of Chemistry, Faculty of Science, Okayama University, Tsushima-naka 3-1-1, Okayama 700-8530, Japan Correspondence e-mail: habibi284@gmail.com

Received 19 January 2010; accepted 25 January 2010

Key indicators: single-crystal X-ray study; T = 193 K; mean  $\sigma$ (C–C) = 0.005 Å; R factor = 0.035; wR factor = 0.100; data-to-parameter ratio = 8.5.

The title compound,  $C_{27}H_{27}N_7O_6$ , a Schiff base, was synthesized by the reaction of triethylenetetramine with 3-nitrobenzealdehyde. There are two independent molecules in the asymmetric unit. The central aromatic ring in one molecule makes dihedral angles of 23.99 (7) and 20.06 (6)° with the two terminal rings; for the second molecule, these angles are 26.14 (6) and 24.64 (6)°.

# **Related literature**

For related structures, see: Glidewell *et al.* (2005, 2006); Habibi *et al.* (2007); Li *et al.* (2005).



**Experimental** 

Crystal data C<sub>27</sub>H<sub>27</sub>N<sub>7</sub>O<sub>6</sub>

 $M_r = 545.56$ 

organic compounds

Z = 4Mo *K* $\alpha$  radiation

 $\mu = 0.10 \text{ mm}^{-1}$ 

 $0.30 \times 0.20 \times 0.15 \text{ mm}$ 

T = 193 K

Monoclinic, *Pn*  a = 13.3411 (12) Å b = 10.4347 (8) Å c = 19.8517 (17) Å  $\beta = 103.446$  (3)° V = 2687.8 (4) Å<sup>3</sup>

#### Data collection

Rigaku R-AXIS RAPID	25846 measured reflections
diffractometer	6145 independent reflections
Absorption correction: multi-scan	4184 reflections with $I > 2\sigma(I)$
(ABSCOR; Higashi, 1995)	$R_{\rm int} = 0.035$
$T_{\min} = 0.971, \ T_{\max} = 0.985$	

#### Refinement

 $\begin{array}{ll} R[F^2 > 2\sigma(F^2)] = 0.035 & 2 \text{ restraints} \\ wR(F^2) = 0.100 & \text{H-atom parameters constrained} \\ S = 1.09 & \Delta\rho_{\text{max}} = 0.18 \text{ e} \text{ Å}^{-3} \\ 6145 \text{ reflections} & \Delta\rho_{\text{min}} = -0.19 \text{ e} \text{ Å}^{-3} \\ 722 \text{ parameters} \end{array}$ 

Data collection: *PROCESS-AUTO* (Rigaku, 1998); cell refinement: *PROCESS-AUTO*; data reduction: *CrystalStructure* (Rigaku, 2004); program(s) used to solve structure: *SIR2004* (Burla *et al.*, 2005); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *ORTEP-3 for Windows* (Farrugia, 1997); software used to prepare material for publication: *SHELXL97*.

We thank the University of Isfahan for partial support of this work.

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: BT5175).

#### References

- Burla, M. C., Caliandro, R., Camalli, M., Carrozzini, B., Cascarano, G. L., De Caro, L., Giacovazzo, C., Polidori, G. & Spagna, R. (2005). J. Appl. Cryst. 38, 381–388.
- Farrugia, L. J. (1997). J. Appl. Cryst. 30, 565.
- Glidewell, C., Low, J. N., Skakle, J. M. S. & Wardell, J. L. (2005). Acta Cryst. E61, 03551–03553.
- Glidewell, C., Low, J. N., Skakle, J. M. S. & Wardell, J. L. (2006). *Acta Cryst.* C62, 01–04.
- Habibi, M. H., Mokhtari, R., Harrington, R. W. & Clegg, W. (2007). Acta Cryst. E63, 02881.

Higashi, T. (1995). ABSCOR. Rigaku Corporation, Tokyo, Japan.

Li, Y.-G., Zhu, H.-L., Chen, X.-Z. & Song, Y. (2005). Acta Cryst. E61, 04156-04157.

Rigaku (1998). PROCESS-AUTO. Rigaku Corporation, Tokyo, Japan.

Rigaku (2004). Crystal Structure. Rigaku/MSC, The Woodlands, Texas,USA. Sheldrick, G. M. (2008). Acta Cryst. A64, 112–122.

# supporting information

Acta Cryst. (2010). E66, o501 [doi:10.1107/S1600536810003168]

# *N,N'*-Bis(3-nitrobenzylidene)-2,2'-[2-(3-nitrophenyl)imidazolidine-1,3diyl]diethanamine

# Mohammad Hossein Habibi, Narges Abarghooei-Shirazi, Yuki Yamane and Takayoshi Suzuki

# S1. Comment

The design of Schiff-base complexes has received long-lasting research interest not only because of their attractive structural and topological novelty. Structures of Schiff bases derived from nitrobenzaldehydes and related to the title compound have been reported by Li *et al.* (2005), Glidewell *et al.* (2005, 2006), and Habibi *et al.* (2007).

The title compound (Fig. 1) was synthesized by the reaction of triethylenetetramine with 3-nitrobenzealdehyde, and its crystal structure is reported here.

The orientations of the C1–C6 and C15–C20 benzene rings respect to the C22–C27 ring are indicated by the dihedral angles of 23.90 (5) and 20.43 (5) $^{\circ}$ , respectively.

# S2. Experimental

The title compound was synthesized by adding triethylenetetramine (0.146 g, 1 mmol) into a solution of 3-nitrobenzealdehyde (0.453 g, 3 mmol) in methanol (10 ml). The mixture was refluxed with stirring for 3 d. The resultant yellow solution was filtered. Pale yellow columnar single crystals of (I) were formed after slow evaporation of the solvent at room temperature (81% yield).

# S3. Refinement

In the absence of anomalous scatterers, Friedel pairs were merged. Hydrogen atoms were refined using a riding model with C-H ranging from 0.95 to 1.00Å and U(H)= $1.2U_{eq}(C)$ .



## Figure 1

A view of the title compound, showing the atom-numbering scheme. Displacement ellipsoids are drawn at the 30% probability level and the hydrogen atoms are omitted for clarity.

# N,N'-Bis(3-nitrobenzylidene)-2,2'-[2-(3- nitrophenyl)imidazolidine-1,3-diyl]diethanamine

Crystal data

 $C_{27}H_{27}N_7O_6$  $M_r = 545.56$ Monoclinic, Pn *a* = 13.3411 (12) Å b = 10.4347 (8) Å c = 19.8517 (17) Å $\beta = 103.446 (3)^{\circ}$ V = 2687.8 (4) Å<sup>3</sup> Z = 4

### Data collection

Rigaku R-AXIS RAPID	25846 measured
diffractometer	6145 independe
Radiation source: fine-focus sealed tube	4184 reflections
Graphite monochromator	$R_{\rm int} = 0.035$
Detector resolution: 10.00 pixels mm <sup>-1</sup>	$\theta_{\rm max} = 27.5^{\circ},  \theta_{\rm min}$
$\omega$ scans	$h = -14 \rightarrow 17$
Absorption correction: multi-scan	$k = -13 \rightarrow 13$
(ABSCOR; Higashi, 1995)	$l = -25 \rightarrow 25$
$T_{\min} = 0.971, T_{\max} = 0.985$	

F(000) = 1144 $D_{\rm x} = 1.348 {\rm Mg} {\rm m}^{-3}$ Mo *Ka* radiation,  $\lambda = 0.71075$  Å Cell parameters from 16587 reflections  $\theta = 3.0 - 27.5^{\circ}$  $\mu = 0.10 \text{ mm}^{-1}$ T = 193 KColumnar, pale yellow  $0.30 \times 0.20 \times 0.15 \text{ mm}$ 

reflections nt reflections with  $I > 2\sigma(I)$  $n = 3.0^{\circ}$ 

Refinement

Refinement on $F^2$	Secondary atom site location: difference Fourier
Least-squares matrix: full	map
$R[F^2 > 2\sigma(F^2)] = 0.035$	Hydrogen site location: inferred from
$wR(F^2) = 0.100$	neighbouring sites
S = 1.09	H-atom parameters constrained
6145 reflections	$w = 1/[\sigma^2(F_o^2) + (0.0478P)^2 + 0.1416P]$
722 parameters	where $P = (F_{o}^{2} + 2F_{c}^{2})/3$
2 restraints	$(\Delta/\sigma)_{\rm max} < 0.001$
Primary atom site location: structure-invariant	$\Delta \rho_{\rm max} = 0.18 \ {\rm e} \ {\rm \AA}^{-3}$
direct methods	$\Delta \rho_{\rm min} = -0.19 \text{ e} \text{ Å}^{-3}$

## Special details

**Geometry**. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor wR and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) etc. and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(\mathring{A}^2)$ 

	x	У	Ζ	$U_{\rm iso}*/U_{\rm eq}$
O1	0.0261 (2)	0.4566 (3)	0.46260 (13)	0.0776 (8)
O2	0.1679 (2)	0.4288 (3)	0.53838 (12)	0.0808 (8)
O3	0.0613 (2)	-0.2237 (3)	0.39419 (13)	0.0810 (8)
O4	0.1978 (2)	-0.2651 (3)	0.47154 (12)	0.0814 (8)
O5	-0.0390 (4)	0.0881 (4)	0.40416 (15)	0.1298 (16)
O6	0.0861 (4)	0.0839 (4)	0.35339 (15)	0.1206 (13)
07	0.5520 (2)	0.4584 (3)	0.46114 (12)	0.0697 (7)
08	0.6983 (2)	0.3902 (3)	0.52061 (12)	0.0825 (8)
O9	0.5988 (2)	-0.1978 (3)	0.39002 (12)	0.0752 (8)
O10	0.7406 (2)	-0.2761 (3)	0.44742 (12)	0.0821 (8)
O11	0.5285 (2)	0.1248 (2)	0.41710 (10)	0.0660 (7)
O12	0.62082 (19)	0.0972 (3)	0.34332 (11)	0.0711 (7)
N1	0.1186 (3)	0.4350 (3)	0.47827 (14)	0.0571 (7)
N2	0.0276 (2)	0.4744 (2)	0.20934 (12)	0.0454 (6)
N3	-0.01869 (19)	0.2649 (2)	0.10578 (11)	0.0388 (5)
N4	-0.00579 (18)	0.05332 (19)	0.08514 (11)	0.0376 (5)
N5	0.0705 (2)	-0.2008 (2)	0.14601 (12)	0.0444 (6)
N6	0.1529 (2)	-0.2459 (3)	0.41122 (13)	0.0519 (7)
N7	-0.0057 (4)	0.0868 (3)	0.35173 (16)	0.0824 (12)
N8	0.6402 (3)	0.4212 (3)	0.46565 (14)	0.0583 (8)
N9	0.4868 (2)	0.4884 (2)	0.20265 (11)	0.0452 (6)
N10	0.42653 (18)	0.27230 (19)	0.10836 (11)	0.0360 (5)
N11	0.43561 (19)	0.0591 (2)	0.08579 (11)	0.0404 (5)
N12	0.5201 (3)	-0.1971 (2)	0.13218 (12)	0.0509 (7)
N13	0.6844 (2)	-0.2400 (3)	0.39346 (13)	0.0514 (7)

N14	0.5375 (2)	0.1073 (2)	0.35797 (12)	0.0478 (6)
C1	0.1207 (2)	0.4378 (3)	0.35527 (15)	0.0446 (7)
H1	0.0503	0.4625	0.3448	0.053*
C2	0.1723 (3)	0.4170 (3)	0.42276 (16)	0.0468 (7)
C3	0.2741 (3)	0.3794 (3)	0.44019 (18)	0.0591 (9)
H3	0.3083	0.3649	0.4871	0.071*
C4	0.3250 (3)	0.3634 (3)	0.3877 (2)	0.0678 (10)
H4	0.3951	0.3370	0.3985	0.081*
C5	0.2750 (3)	0.3854 (3)	0.31987 (18)	0.0582 (9)
Н5	0.3115	0.3751	0.2844	0.070*
C6	0.1723 (2)	0.4224 (3)	0.30228 (15)	0.0452 (7)
C7	0.1219 (3)	0.4467 (3)	0.22959 (15)	0.0464 (7)
H7	0.1622	0.4414	0.1960	0.056*
C8	-0.0121 (3)	0.4944 (3)	0.13518 (15)	0.0483 (7)
H8A	0.0461	0.5042	0.1125	0.058*
H8B	-0.0535	0.5741	0.1274	0.058*
C9	-0.0786(2)	0.3817 (3)	0.10338 (15)	0.0452 (7)
H9A	-0.1335	0.3681	0.1287	0.054*
H9B	-0.1121	0.4018	0.0546	0.054*
C10	0.0469 (2)	0.2563 (3)	0.05557 (14)	0.0429 (7)
H10A	0.1189	0.2800	0.0774	0.051*
H10B	0.0210	0.3133	0.0154	0.051*
C11	0.0395 (2)	0.1166 (2)	0.03351 (14)	0.0422 (7)
H11A	-0.0052	0.1066	-0.0136	0.051*
H11B	0.1085	0.0811	0.0341	0.051*
C12	-0.0516(2)	-0.0713 (3)	0.06384 (14)	0.0431 (7)
H12A	-0.0892	-0.0671	0.0146	0.052*
H12B	-0.1021	-0.0922	0.0917	0.052*
C13	0.0282 (3)	-0.1764(3)	0.07264 (14)	0.0469(7)
H13A	-0.0037	-0.2557	0.0498	0.056*
H13B	0.0843	-0.1507	0.0504	0.056*
C14	0.1664 (3)	-0.2193(3)	0.16574 (15)	0.0450 (7)
H14	0.2071	-0.2177	0.1324	0.054*
C15	0.2170 (2)	-0.2432(3)	0.23866 (15)	0.0431(7)
C16	0.3208(3)	-0.2737(3)	0.25746 (18)	0.0552(8)
H16	0.3593	-0.2799	0.2229	0.066*
C17	0.3691 (3)	-0.2950(3)	0.3262(2)	0.0651 (10)
H17	0 4402	-0.3163	0 3382	0.078*
C18	0.3153(3)	-0.2857(3)	0.37732(17)	0.0538 (8)
H18	0.3482	-0.3005	0.4245	0.065*
C19	0.2116(2)	-0.2541(3)	0.35782(15)	0.0434(7)
C20	0.1617(2)	-0.2336(2)	0.39702(13) 0.29012(14)	0.0391 (6)
H20	0.0904	-0.2132	0.2784	0.047*
C21	-0.0790(2)	0.1478(2)	0.09801(14)	0.0389(6)
H21	-0.1387	0.1545	0.0570	0.047*
C22	-0.1167(3)	0.1193(3)	0.16267 (15)	0.0455(7)
C23	-0.2200(3)	0.0999 (3)	0.1606 (2)	0.0587(9)
H23	-0.2690	0.1038	0.1175	0.070*

C24	-0.2533 (3)	0.0747 (3)	0.2207 (2)	0.0729 (13)
H24	-0.3244	0.0613	0.2184	0.088*
C25	-0.1831 (4)	0.0692 (3)	0.2832 (2)	0.0747 (13)
H25	-0.2048	0.0527	0.3247	0.090*
C26	-0.0809(3)	0.0882 (3)	0.28462 (17)	0.0608 (10)
C27	-0.0458 (3)	0.1124 (3)	0.22580 (16)	0.0518 (8)
H27	0.0257	0.1241	0.2285	0.062*
C28	0.6116 (2)	0.4386 (3)	0.33961 (14)	0.0426 (7)
H28	0.5416	0.4593	0.3375	0.051*
C29	0.6790 (3)	0.4144 (3)	0.40212 (15)	0.0467 (7)
C30	0.7810 (3)	0.3836 (3)	0.40797 (19)	0.0586 (9)
H30	0.8256	0.3683	0.4520	0.070*
C31	0.8168 (3)	0.3758 (3)	0.3483(2)	0.0625 (9)
H31	0.8867	0.3537	0.3509	0.075*
C32	0.7508 (3)	0.3999 (3)	0.28452 (19)	0.0567 (8)
H32	0.7763	0.3943	0.2437	0.068*
C33	0.6485(2)	0.4322(3)	0.27917(15)	0.0427(7)
C34	0.5801(3)	0.4583(3)	0.21081(14)	0.0455(7)
H34	0.6079	0.4520	0.1710	0.055*
C35	0.4290(3)	0.5037 (3)	0.13124(14)	0.033 0.0475(7)
H35A	0.4773	0.5162	0.1007	0.057*
H35B	0 3842	0.5803	0.1273	0.057*
C36	0.3637(2)	0.3855 (2)	0.1275	0.037 0.0426(7)
Н36А	0.3177	0.3717	0.1408	0.051*
H36R	0.3199	0.3995	0.0618	0.051*
C37	0.3799 0.4791 (3)	0.2630 (3)	0.05098(14)	0.051 0.0453(7)
H37A	0.5527	0.2866	0.05696 (14)	0.054*
H37B	0.4463	0.3200	0.0123	0.054*
C38	0.4405	0.3202 0.1237 (3)	0.0125 0.02864 (14)	0.054 0.0466 (7)
H38A	0.4149	0.1237 (3)	-0.0152	0.056*
H38B	0.5340	0.0888	0.0132	0.056*
C30	0.3833 (3)	-0.0623(3)	0.0224 0.06658 (15)	0.050
H30A	0.3348	-0.0532	0.0208	0.063*
H30R	0.3426	-0.0843	0.0208	0.003
C40	0.3420 0.4574(3)	-0.1695 (3)	0.06335 (15)	0.005
U40 H40A	0.4186	-0.2472	0.00335 (13)	0.0390 (9)
H40R	0.4180	-0.1450	0.0323	0.072*
C41	0.5020	-0.2077(3)	0.0323	0.072
U41	0.6438	-0.1078	0.13940 (13)	0.0510(8)
C42	0.6867 (3)	-0.2344(3)	0.0998	0.002
C42	0.0307(3) 0.7885(3)	-0.2686(3)	0.20033(13) 0.21040(10)	0.0402(7)
U12	0.7885 (5)	-0.2748	0.21040 (19)	0.0380 (9)
C14	0.8125	-0.2937(3)	0.1091 0.2732(2)	$0.070^{\circ}$
U77 H//	0.0330 (3)	-0.2757(5)	0.2732(2)	0.0027 (9)
C45	0.724/	-0.2840(2)	0.2770 (19)	$0.075^{\circ}$
U45	0.0224 (3)	-0.2040(3)	0.35572 (16)	0.0331(8)
п <del>ч</del> 3 С46	0.00/9	-0.3003	0.3773 0.32022 (15)	$0.000^{*}$
C40	0.7211(2) 0.6526(2)	-0.2490(3)	0.32922(13) 0.26752(14)	0.0434(7)
C47	0.0320 (2)	-0.2248 (2)	0.20733 (14)	0.0419(/)

H47	0.5833	-0.2017	0.2664	0.050*	
C48	0.3706 (2)	0.1528 (2)	0.11034 (13)	0.0386 (6)	
H48	0.3009	0.1570	0.0781	0.046*	
C49	0.3613 (2)	0.1228 (2)	0.18271 (14)	0.0391 (6)	
C50	0.2689 (3)	0.0929 (3)	0.19902 (16)	0.0458 (7)	
H50	0.2077	0.0904	0.1632	0.055*	
C51	0.2637 (3)	0.0662 (3)	0.26671 (17)	0.0511 (8)	
H51	0.1993	0.0457	0.2767	0.061*	
C52	0.3514 (3)	0.0695 (3)	0.31922 (15)	0.0471 (7)	
H52	0.3485	0.0522	0.3657	0.056*	
C53	0.4438 (2)	0.0987 (3)	0.30269 (14)	0.0403 (6)	
C54	0.4506 (2)	0.1249 (3)	0.23579 (14)	0.0407 (6)	
H54	0.5153	0.1442	0.2260	0.049*	

Atomic displacement parameters  $(Å^2)$ 

	$U^{11}$	$U^{22}$	$U^{33}$	$U^{12}$	$U^{13}$	$U^{23}$
01	0.0682 (19)	0.111 (2)	0.0588 (16)	-0.0063 (16)	0.0245 (15)	-0.0097 (14)
O2	0.103 (2)	0.098 (2)	0.0386 (14)	-0.0036 (16)	0.0100 (13)	0.0131 (13)
O3	0.0531 (17)	0.148 (3)	0.0426 (14)	-0.0008 (17)	0.0129 (12)	0.0006 (15)
O4	0.087 (2)	0.118 (2)	0.0335 (13)	-0.0012 (17)	0.0018 (13)	0.0044 (13)
05	0.209 (4)	0.149 (3)	0.0532 (17)	0.081 (3)	0.074 (2)	0.0374 (19)
O6	0.130 (3)	0.195 (4)	0.0390 (16)	0.005 (3)	0.025 (2)	0.0121 (19)
O7	0.082 (2)	0.0833 (18)	0.0458 (13)	-0.0087 (15)	0.0182 (14)	-0.0057 (12)
08	0.094 (2)	0.102 (2)	0.0379 (13)	-0.0326 (17)	-0.0144 (13)	0.0177 (13)
09	0.0601 (17)	0.125 (2)	0.0423 (13)	0.0025 (16)	0.0165 (13)	-0.0044 (13)
O10	0.084 (2)	0.117 (2)	0.0357 (13)	0.0067 (17)	-0.0046 (13)	0.0056 (13)
011	0.0762 (17)	0.0962 (18)	0.0251 (11)	0.0074 (14)	0.0111 (11)	0.0000 (11)
O12	0.0516 (16)	0.120 (2)	0.0399 (13)	0.0023 (14)	0.0069 (11)	0.0042 (13)
N1	0.074 (2)	0.0565 (16)	0.0415 (16)	-0.0090 (15)	0.0150 (15)	0.0024 (12)
N2	0.0597 (18)	0.0381 (12)	0.0393 (13)	-0.0023 (12)	0.0135 (12)	-0.0042 (10)
N3	0.0482 (15)	0.0378 (12)	0.0306 (12)	-0.0011 (10)	0.0097 (11)	0.0013 (9)
N4	0.0485 (15)	0.0373 (11)	0.0277 (11)	-0.0026 (10)	0.0105 (10)	0.0007 (9)
N5	0.0650 (19)	0.0387 (12)	0.0307 (12)	0.0001 (12)	0.0135 (12)	0.0005 (10)
N6	0.061 (2)	0.0648 (16)	0.0272 (13)	-0.0085 (13)	0.0037 (13)	0.0000 (11)
N7	0.137 (4)	0.079 (2)	0.0431 (18)	0.030 (2)	0.046 (2)	0.0179 (15)
N8	0.075 (2)	0.0571 (16)	0.0353 (15)	-0.0220 (16)	-0.0019 (15)	0.0034 (12)
N9	0.0639 (19)	0.0375 (12)	0.0302 (12)	0.0017 (12)	0.0026 (12)	-0.0027 (9)
N10	0.0453 (14)	0.0339 (11)	0.0288 (11)	-0.0003 (10)	0.0082 (10)	0.0015 (9)
N11	0.0560 (16)	0.0363 (12)	0.0268 (11)	-0.0016 (10)	0.0053 (11)	-0.0001 (9)
N12	0.082 (2)	0.0359 (12)	0.0296 (13)	0.0015 (13)	0.0015 (13)	-0.0004 (10)
N13	0.0582 (19)	0.0609 (16)	0.0328 (14)	-0.0116 (14)	0.0062 (13)	-0.0036 (11)
N14	0.0582 (18)	0.0567 (15)	0.0273 (12)	0.0035 (13)	0.0076 (12)	0.0053 (10)
C1	0.0492 (19)	0.0394 (14)	0.0445 (17)	-0.0036 (13)	0.0096 (15)	-0.0016 (12)
C2	0.055 (2)	0.0399 (14)	0.0424 (17)	-0.0038 (14)	0.0062 (15)	-0.0009 (12)
C3	0.062 (2)	0.0527 (18)	0.054 (2)	0.0063 (16)	-0.0031 (18)	-0.0061 (15)
C4	0.054 (2)	0.072 (2)	0.068 (2)	0.0124 (18)	-0.0045 (19)	-0.0197 (19)
C5	0.051 (2)	0.062 (2)	0.061 (2)	0.0056 (16)	0.0131 (18)	-0.0193 (16)

C6	0.0486 (19)	0.0409 (15)	0.0455 (17)	-0.0025 (13)	0.0096 (15)	-0.0095 (12)
C7	0.054 (2)	0.0446 (16)	0.0431 (17)	-0.0017 (14)	0.0154 (15)	-0.0100 (13)
C8	0.067 (2)	0.0389 (15)	0.0386 (15)	-0.0011 (14)	0.0109 (15)	-0.0003(12)
C9	0.0540 (19)	0.0409 (14)	0.0390 (15)	0.0029 (13)	0.0071 (14)	0.0024 (12)
C10	0.0529 (18)	0.0433 (15)	0.0337 (15)	-0.0043 (13)	0.0125 (14)	0.0033 (11)
C11	0.0545 (18)	0.0463 (15)	0.0265 (13)	-0.0055 (13)	0.0109 (13)	0.0023 (11)
C12	0.059 (2)	0.0379 (14)	0.0316 (14)	-0.0072(13)	0.0087 (14)	-0.0023 (11)
C13	0.067 (2)	0.0418 (15)	0.0312 (15)	-0.0001(14)	0.0108 (14)	-0.0014(12)
C14	0.063 (2)	0.0393 (15)	0.0368 (16)	-0.0051(14)	0.0202 (16)	-0.0046(12)
C15	0.0499(19)	0.0379 (14)	0.0426 (16)	-0.0072(13)	0.0130 (14)	-0.0069(12)
C16	0.049 (2)	0.0596 (19)	0.060(2)	-0.0045(15)	0.0190 (17)	-0.0140(16)
C17	0.047(2)	0.072 (2)	0.070(3)	0.0045 (17)	0.0008 (19)	-0.0147(19)
C18	0.049(2)	0.0567(18)	0.0471(18)	-0.0007(15)	-0.0061(16)	-0.0064(15)
C19	0.019(2)	0.0207(10) 0.0406(14)	0.0367(15)	-0.0047(12)	0.0001(10) 0.0045(14)	-0.0023(12)
C20	0.0201(17)	0.0402(14)	0.0349(14)	-0.0060(12)	0.0013(11)	-0.0020(12)
C21	0.0405(16)	0.0405(14)	0.0344(14)	-0.0026(12)	0.0002(12)	0.0007(11)
C21	0.0102(10)	0.0109(11) 0.0380(14)	0.0311(11) 0.0478(18)	-0.0014(13)	0.0002(12) 0.0228(16)	-0.0020(12)
C22	0.050(2) 0.058(2)	0.0380(14) 0.0480(17)	0.078(2)	-0.0017(15)	0.0228(10) 0.0318(19)	-0.0136(16)
C24	0.030(2)	0.0456(19)	0.070(2) 0.113(4)	-0.0134(18)	0.0510(1)	-0.013(2)
C25	0.001(3) 0.115(4)	0.0456(19)	0.019(1)	0.0137(10)	0.000(3)	0.013(2)
C26	0.119(4) 0.100(3)	0.0450(19) 0.0452(16)	0.000(5)	0.000(2) 0.0045(18)	0.075(3)	0.0001(19) 0.0065(14)
C27	0.100(3)	0.0502(10)	0.0465(18)	0.0015(10) 0.0026(15)	0.010(2) 0.0283(17)	0.0000 (11) 0.0080 (14)
C28	0.000(2)	0.0302(17) 0.0382(14)	0.0344(15)	-0.0020(13)	0.0203(17) 0.0033(14)	-0.0000(11)
C20	0.0510(1)	0.0382(11) 0.0381(14)	0.0379(16)	-0.0087(13)	0.0005(11)	0.0000 (11)
C30	0.055(2)	0.0501(11) 0.0504(18)	0.0577(10)	-0.0016(16)	-0.0009(17)	0.0052(12) 0.0058(15)
C31	0.033(2) 0.047(2)	0.0567(10)	0.000(2) 0.077(3)	0.0010(10)	0.0009(17)	-0.0090(17)
C32	0.017(2)	0.0535(18)	0.077(3)	-0.0013(16)	0.0000(19) 0.0138(18)	-0.0132(15)
C33	0.057(2)	0.0355(10)	0.000(2) 0.0397(16)	-0.0040(13)	0.0130(10) 0.0044(14)	-0.0048(12)
C34	0.063(2)	0.0397(11)	0.0333(15)	-0.0055(14)	0.00110(15)	-0.0054(11)
C35	0.003(2)	0.0357(15)	0.0319(15)	0.00000(11)	0.0010(15)	0 0004 (11)
C36	0.071(2)	0.0405(14)	0.0317(12)	0.0010(11) 0.0064(13)	0.0010(13)	0.0000(11)
C37	0.0510(10)	0.0443(15)	0.0319(14)	-0.0033(14)	0.0020(13) 0.0144(14)	-0.0020(11)
C38	0.061(2)	0.0448(15)	0.0292(14)	0.0033(11)	0.0105(14)	0.0006(11)
C39	0.076(2)	0.0385(15)	0.0342(16)	-0.0087(14)	-0.0032(15)	-0.0003(12)
C40	0.102(3)	0.0370(15)	0.0324(16)	0.0032 (16)	-0.0001(16)	-0.0030(12)
C41	0.087(3)	0.0377(15)	0.0320(16)	-0.0007(16)	0.0198(17)	-0.0057(12)
C42	0.067(3)	0.0379(13)	0.0408 (16)	-0.0062(14)	0.0157(15)	-0.0038(12)
C43	0.069(2)	0.0529(11) 0.0528(18)	0.061(2)	-0.0030(17)	0.013 (2)	-0.0074(15)
C44	0.003(2)	0.0520(10)	0.001(2)	-0.0019(17)	0.033(2)	-0.0092(18)
C45	0.033(2) 0.047(2)	0.000(2) 0.0577(19)	0.076(2)	-0.0019(17)	0.010(2)	-0.0052(10)
C46	0.0480(19)	0.0377(15) 0.0443(15)	0.0374(15)	-0.0059(13)	0.0020(10) 0.0091(14)	-0.0031(12)
C47	0.0514(19)	0.0381(14)	0.0377(15)	-0.0047(13)	0.0091(11) 0.0088(14)	-0.0039(12)
C48	0.0211(17) 0.0445(17)	0.0394(14)	0.0291(13)	-0.0012(12)	0.0000(11) 0.0026(12)	0.0025(11)
C49	0.0465(18)	0.0391(11) 0.0362(13)	0.0291(13) 0.0329(14)	-0.0012(12)	0.0020(12) 0.0059(13)	0.0025(11)
C50	0.0500(19)	0.0424(15)	0.0424(16)	-0.0086(13)	0.0053(14)	0.0029(12)
C51	0.056 (2)	0.0504(17)	0.0495 (18)	-0.0110(15)	0.0170 (16)	0.0057(14)
C52	0.063 (2)	0.0436 (15)	0.0376 (16)	-0.0042(14)	0.0187 (16)	0.0046 (12)
C53	0.0504 (18)	0.0394 (14)	0.0302 (14)	0.0002 (13)	0.0076 (13)	0.0005 (11)
					···· ()	···· ()

C54	0.0494 (18)	0.0433 (15)	0.0297 (14)	-0.0001 (13)	0.0098 (13)	0.0018 (11)
Geome	tric parameters (À	, <i>°</i> )				
01—N	[1	1.222 (4)	)	C16—H16		0.9500
02—N	[1	1.223 (4)	)	C17—C18		1.375 (5)
03—N	6	1.213 (4)	)	С17—Н17		0.9500
04—N	6	1.224 (3)	)	C18—C19		1.387 (5)
05—N	17	1.223 (4)	)	C18—H18		0.9500
06—N	7	1.218 (5)	)	C19—C20		1.371 (4)
07—N	8	1.223 (4)	)	С20—Н20		0.9500
08—N	8	1.226 (4)	)	C21—C22		1.513 (4)
09—N	13	1.212 (4)	)	C21—H21		1.0000
O10—	N13	1.215 (4)	)	C22—C23		1.384 (5)
011-1	N14	1.221 (3)	)	C22—C27		1.386 (5)
012—	N14	1.217 (3)	)	C23—C24		1.390 (5)
N1—C	2	1.459 (4)	)	С23—Н23		0.9500
N2—C	27	1.262 (4)	)	C24—C25		1.371 (6)
N2—C	8	1.459 (4)	)	C24—H24		0.9500
N3—C	21	1.451 (3)	)	C25—C26		1.371 (6)
N3—C	9	1.453 (3)	)	С25—Н25		0.9500
N3—C	10	1.474 (4)	)	C26—C27		1.379 (4)
N4—C	21	1.452 (3)	)	С27—Н27		0.9500
N4—C	12	1.458 (3)	)	C28—C29		1.376 (4)
N4—C	11	1.462 (3)	)	C28—C33		1.400 (4)
N5—C	14	1.263 (4)	)	C28—H28		0.9500
N5—C	213	1.457 (4)	)	C29—C30		1.377 (5)
N6—C	19	1.459 (4)	)	C30—C31		1.378 (5)
N7—C	26	1.470 (5)	)	C30—H30		0.9500
N8—C	29	1.472 (4)	)	C31—C32		1.387 (5)
N9—C	34	1.258 (4)	)	C31—H31		0.9500
N9—C	35	1.456 (4)	)	C32—C33		1.386 (4)
N10—	C36	1.450 (3)	)	С32—Н32		0.9500
N10—	C48	1.459 (3)	)	C33—C34		1.474 (4)
N10—	C37	1.473 (3)	)	C34—H34		0.9500
N11—	C39	1.454 (3)	)	C35—C36		1.516 (4)
N11—	C48	1.463 (4)	)	С35—Н35А		0.9900
N11—	C38	1.467 (3)	)	C35—H35B		0.9900
N12—	C41	1.260 (4)	)	C36—H36A		0.9900
N12—	C40	1.455 (4)	)	C36—H36B		0.9900
N13—	C46	1.472 (4)	)	C37—C38		1.517 (4)
N14—	C53	1.462 (4)	)	С37—Н37А		0.9900
C1—C	2	1.373 (4)	)	С37—Н37В		0.9900
C1—C	6	1.394 (4)	)	C38—H38A		0.9900
С1—Н	1	0.9500		C38—H38B		0.9900
С2—С	3	1.378 (5)	)	C39—C40		1.504 (5)
С3—С	4	1.380 (5)	)	С39—Н39А		0.9900
С3—Н	3	0.9500		С39—Н39В		0.9900

# supporting information

a. a.	1.256 (5)		0.0000
C4—C5	1.376 (5)	C40—H40A	0.9900
C4—H4	0.9500	C40—H40B	0.9900
C5—C6	1.388 (4)	C41—C42	1.466 (5)
С5—Н5	0.9500	C41—H41	0.9500
С6—С7	1.465 (4)	C42—C43	1.388 (5)
С7—Н7	0.9500	C42—C47	1.397 (4)
C8—C9	1.519 (4)	C43—C44	1.379 (5)
C8—H8A	0.9900	C43—H43	0.9500
C8—H8B	0 9900	C44—C45	1 378 (5)
C9—H9A	0.9900	C44—H44	0.9500
C9_H9B	0.9900	C45-C46	1 381 (5)
	1.510(4)	C45 H45	0.0500
	0.0000		0.9300
CIO—HIOA	0.9900	C40-C47	1.372 (4)
CI0—HI0B	0.9900	C4/—H4/	0.9500
CII—HIIA	0.9900	C48—C49	1.503 (4)
C11—H11B	0.9900	C48—H48	1.0000
C12—C13	1.510 (4)	C49—C50	1.381 (4)
C12—H12A	0.9900	C49—C54	1.395 (4)
C12—H12B	0.9900	C50—C51	1.390 (4)
C13—H13A	0.9900	С50—Н50	0.9500
C13—H13B	0.9900	C51—C52	1.374 (5)
C14—C15	1.469 (4)	C51—H51	0.9500
C14—H14	0.9500	C52—C53	1.382 (4)
C15—C16	1 385 (4)	C52—H52	0.9500
$C_{15} - C_{20}$	1 396 (4)	$C_{53}$ $C_{54}$	1.379(3)
C16 C17	1 385 (5)	C54 H54	0.9500
010-017	1.565 (5)	034-1134	0.9500
01 - N1 - 02	122 7 (3)	$C^{23}$ $C^{22}$ $C^{21}$	122.0(3)
O1 N1 C2	122.7(3) 118.4(3)	$C_{23}^{23} = C_{22}^{22} = C_{21}^{21}$	122.0(3)
$O_1 = N_1 = O_2$	110.4(3)	$C_{27} = C_{22} = C_{21}$	117.0(3)
02-N1-C2	116.9 (3)	$C_{22} = C_{23} = C_{24}$	121.1 (4)
$C_{1} = N_{2} = C_{8}$	117.1(3)	C22—C23—H23	119.4
C21—N3—C9	114.6 (2)	C24—C23—H23	119.4
C21—N3—C10	106.2 (2)	C25—C24—C23	119.8 (4)
C9—N3—C10	115.9 (2)	C25—C24—H24	120.1
C21—N4—C12	113.8 (2)	C23—C24—H24	120.1
C21—N4—C11	102.8 (2)	C24—C25—C26	118.6 (3)
C12—N4—C11	114.4 (2)	C24—C25—H25	120.7
C14—N5—C13	117.7 (3)	C26—C25—H25	120.7
O3—N6—O4	122.4 (3)	C25—C26—C27	122.8 (4)
O3—N6—C19	119.0 (3)	C25—C26—N7	118.9 (3)
O4—N6—C19	118.6 (3)	C27—C26—N7	118.3 (4)
O6—N7—O5	122.6 (4)	C26—C27—C22	118.7 (3)
O6—N7—C26	119.7 (3)	C26—C27—H27	120.7
05—N7—C26	1177(5)	С22—С27—Н27	120.7
07-N8-08	123 2 (3)	$C_{29} C_{28} C_{33}$	1186(3)
07 - N8 - C29	123.2(3) 118 5 (3)	C20_C28_H28	120.7
$O_{1} = 100 = O_{2}$	110.3(3) 118.2(3)	$C_{22} = C_{20} = 1120$	120.7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	110.3(3)	$C_{33} = C_{20} = C_{20}$	120.7
U34—IN9—U33	113.9 (2)	U20-U29-U30	123.0(3)

C36—N10—C48	113.4 (2)	C28—C29—N8	118.6 (3)
C36—N10—C37	116.0 (2)	C30—C29—N8	118.5 (3)
C48—N10—C37	107.65 (19)	C29—C30—C31	118.3 (3)
C39—N11—C48	112.6 (2)	С29—С30—Н30	120.8
C39—N11—C38	114.0 (2)	C31—C30—H30	120.8
C48 - N11 - C38	104.7(2)	$C_{30}$ $C_{31}$ $C_{32}$	120.0(3)
C41 - N12 - C40	1181(3)	$C_{30}$ $C_{31}$ $H_{31}$	120.0
09-N13-010	122 8 (3)	$C_{32}$ $C_{31}$ $H_{31}$	120.0
09—N13—C46	1122.0(3)	$C_{33}$ $C_{32}$ $C_{31}$ $C_{31}$	120.0 121.3(3)
010 - N13 - C46	118.8 (3)	$C_{33}$ $C_{32}$ $H_{32}$	119.4
012 - N14 - 011	122 8 (3)	$C_{31}$ $C_{32}$ $H_{32}$	119.1
012 N14 $011$	122.0(3) 1190(2)	$C_{32}$ $C_{33}$ $C_{28}$	118.8 (3)
012 $114$ $033$ $011$ $114$ $153$	119.0(2) 118.2(3)	$C_{32} = C_{33} = C_{34}$	120.2(3)
$C_{2}$	110.2(3)	$C_{22} = C_{33} = C_{34}$	120.2(3)
$C_2 = C_1 = C_0$	120.2	N0 C34 C33	121.0(3)
C6 C1 H1	120.2	$N_{9} = C_{34} = C_{33}$	123.1 (3)
$C_0 = C_1 = C_1$	120.2 122.0(2)	$N_{2} = C_{24} = 1134$	118.4
$C_1 = C_2 = C_3$	122.0(3)	$C_{33} - C_{34} - H_{34}$	110.4
$C_1 = C_2 = N_1$	119.0(3)	N9 - C35 - C30	109.3 (2)
$C_3 = C_2 = C_4$	118.4 (3)	N9 - C35 - H35A	109.8
$C_2 = C_3 = C_4$	118.3 (3)	C30—C35—H35A	109.8
C2C3H3	120.8	N9-C35-H35B	109.8
C4—C3—H3	120.8	С36—С35—Н35В	109.8
C5-C4-C3	120.5 (3)	H35A—C35—H35B	108.2
C5—C4—H4	119.8	N10-C36-C35	111.8 (2)
C3—C4—H4	119.8	N10—C36—H36A	109.3
C4—C5—C6	121.2 (3)	С35—С36—Н36А	109.3
C4—C5—H5	119.4	N10—C36—H36B	109.3
С6—С5—Н5	119.4	С35—С36—Н36В	109.3
C5—C6—C1	118.3 (3)	H36A—C36—H36B	107.9
C5—C6—C7	119.7 (3)	N10—C37—C38	104.8 (2)
C1—C6—C7	121.9 (3)	N10—C37—H37A	110.8
N2—C7—C6	123.3 (3)	С38—С37—Н37А	110.8
N2—C7—H7	118.4	N10—C37—H37B	110.8
С6—С7—Н7	118.4	С38—С37—Н37В	110.8
N2—C8—C9	110.4 (2)	Н37А—С37—Н37В	108.9
N2—C8—H8A	109.6	N11—C38—C37	104.0 (2)
С9—С8—Н8А	109.6	N11—C38—H38A	111.0
N2—C8—H8B	109.6	С37—С38—Н38А	111.0
С9—С8—Н8В	109.6	N11—C38—H38B	111.0
H8A—C8—H8B	108.1	C37—C38—H38B	111.0
N3—C9—C8	111.9 (3)	H38A—C38—H38B	109.0
N3—C9—H9A	109.2	N11—C39—C40	112.3 (3)
С8—С9—Н9А	109.2	N11—C39—H39A	109.1
N3—C9—H9B	109.2	С40—С39—Н39А	109.1
С8—С9—Н9В	109.2	N11—C39—H39B	109.1
Н9А—С9—Н9В	107.9	С40—С39—Н39В	109.1
N3—C10—C11	104.1 (2)	H39A—C39—H39B	107.9
N3—C10—H10A	110.9	N12—C40—C39	110.3 (2)

C11—C10—H10A	110.9	N12—C40—H40A	109.6
N3—C10—H10B	110.9	C39—C40—H40A	109.6
C11—C10—H10B	110.9	N12-C40-H40B	109.6
H10A—C10—H10B	109.0	C39—C40—H40B	109.6
N4—C11—C10	103.9 (2)	H40A—C40—H40B	108.1
N4—C11—H11A	111.0	N12—C41—C42	122.8 (3)
C10—C11—H11A	111.0	N12—C41—H41	118.6
N4—C11—H11B	111.0	C42—C41—H41	118.6
C10—C11—H11B	111.0	C43—C42—C47	118.7 (3)
H11A—C11—H11B	109.0	C43—C42—C41	121.1 (3)
N4—C12—C13	112.2 (2)	C47—C42—C41	120.2 (3)
N4—C12—H12A	109.2	C44—C43—C42	121.4 (3)
C13—C12—H12A	109.2	C44—C43—H43	119.3
N4—C12—H12B	109.2	C42—C43—H43	119.3
C13—C12—H12B	109.2	C45—C44—C43	120.1 (3)
H12A—C12—H12B	107.9	C45—C44—H44	119.9
N5-C13-C12	109.9 (2)	C43—C44—H44	119.9
N5-C13-H13A	109.7	C44-C45-C46	119.9 118.1(3)
C12—C13—H13A	109.7	C44-C45-H45	121.0
N5-C13-H13B	109.7	C46-C45-H45	121.0
C12—C13—H13B	109.7	C47 - C46 - C45	121.0 123.1(3)
H13A—C13—H13B	108.2	C47 - C46 - N13	129.1(3) 1183(3)
N5-C14-C15	122 1 (3)	C45-C46-N13	118.6(3)
N5-C14-H14	118.9	$C_{46} - C_{47} - C_{42}$	118.6(3)
C15-C14-H14	118.9	C46-C47-H47	120.7
C16-C15-C20	119.0 (3)	C42-C47-H47	120.7
$C_{16} - C_{15} - C_{14}$	1204(3)	N10-C48-N11	102.4(2)
$C_{20}$ $C_{15}$ $C_{14}$	120.1(3) 120.6(3)	N10-C48-C49	102.1(2) 111.1(2)
$C_{17}$ $C_{16}$ $C_{15}$ $C_{14}$	120.0(3) 120.6(3)	N11-C48-C49	111.1(2) 111.5(2)
C17 - C16 - H16	119.7	N10-C48-H48	110.5
$C_{15}$ $C_{16}$ $H_{16}$	119.7	N11-C48-H48	110.5
C18 - C17 - C16	120.9 (3)	C49—C48—H48	110.5
C18 - C17 - H17	119.6	$C_{50}$ $C_{49}$ $C_{54}$	118.6(3)
C16 - C17 - H17	119.6	$C_{50}$ $C_{49}$ $C_{48}$	123.2(3)
C17 - C18 - C19	117.9 (3)	$C_{54}$ $C_{49}$ $C_{48}$	123.2(3) 118.2(2)
C17 - C18 - H18	121.0	C49-C50-C51	110.2(2) 1213(3)
C19 - C18 - H18	121.0	C49 - C50 - H50	1193
$C_{20}$ $C_{19}$ $C_{18}$	121.0 122.4(3)	$C_{51} - C_{50} - H_{50}$	119.3
$C_{20}$ $C_{19}$ $N_{6}$	1122.1(3) 118.9(3)	$C_{52} - C_{51} - C_{50}$	120.2 (3)
C18 - C19 - N6	118.7 (3)	$C_{52} = C_{51} = C_{50}$	119.9
C19 - C20 - C15	119.2 (3)	C50—C51—H51	119.9
C19 - C20 - H20	120.4	$C_{51} - C_{52} - C_{53}$	118 3 (3)
$C_{15} = C_{20} = H_{20}$	120.1	$C_{51} = C_{52} = H_{52}$	120.8
N3-C21-N4	102.2(2)	$C_{53}$ $C_{52}$ $H_{52}$	120.8
N3-C21-C22	111 2 (2)	$C_{54}$ $C_{53}$ $C_{52}$	122.3 (3)
N4—C21—C22	112 7 (2)	C54—C53—N14	118 3 (2)
N3-C21-H21	110.2	C52—C53—N14	119.3 (2)
N4—C21—H21	110.2	C53—C54—C49	119.3 (3)

C22—C21—H21	110.2	С53—С54—Н54	120.4
C23—C22—C27	119.0 (3)	С49—С54—Н54	120.4
C6—C1—C2—C3	-0.8 (4)	C33—C28—C29—C30	-0.2 (4)
C6-C1-C2-N1	179.1 (3)	C33—C28—C29—N8	180.0 (2)
O1—N1—C2—C1	6.8 (4)	O7—N8—C29—C28	-5.9 (4)
O2—N1—C2—C1	-172.7 (3)	O8—N8—C29—C28	174.6 (3)
O1—N1—C2—C3	-173.3 (3)	O7—N8—C29—C30	174.3 (3)
O2—N1—C2—C3	7.2 (4)	O8—N8—C29—C30	-5.2 (4)
C1—C2—C3—C4	0.4 (5)	C28—C29—C30—C31	-0.6(5)
N1—C2—C3—C4	-179.5 (3)	N8—C29—C30—C31	179.2 (3)
C2—C3—C4—C5	0.4 (5)	C29—C30—C31—C32	0.7 (5)
C3—C4—C5—C6	-0.9(5)	C30—C31—C32—C33	0.0 (5)
C4—C5—C6—C1	0.4 (5)	C31—C32—C33—C28	-0.8(5)
C4—C5—C6—C7	179.2 (3)	C31—C32—C33—C34	179.6 (3)
C2—C1—C6—C5	0.4 (4)	C29—C28—C33—C32	0.9 (4)
C2-C1-C6-C7	-178.3 (3)	C29—C28—C33—C34	-179.5(3)
C8—N2—C7—C6	-179.2(2)	$C_{35}$ N9 $-C_{34}$ $-C_{33}$	-176.7(2)
C5—C6—C7—N2	176.4 (3)	C32—C33—C34—N9	-179.8(3)
C1-C6-C7-N2	-5.0(5)	C28—C33—C34—N9	0.7 (4)
C7—N2—C8—C9	106.7 (3)	C34—N9—C35—C36	101.8 (3)
C21—N3—C9—C8	160.7 (2)	C48—N10—C36—C35	160.4 (2)
C10—N3—C9—C8	-75.0(3)	C37—N10—C36—C35	-74.3(3)
N2-C8-C9-N3	-66.2 (3)	N9-C35-C36-N10	-64.0(3)
C21—N3—C10—C11	-13.9(3)	C36—N10—C37—C38	-138.6(3)
C9—N3—C10—C11	-142.4(2)	C48—N10—C37—C38	-10.4(3)
C21—N4—C11—C10	37.1 (3)	C39—N11—C38—C37	158.1 (3)
C12 - N4 - C11 - C10	161.0 (2)	C48—N11—C38—C37	34.7 (3)
N3-C10-C11-N4	-14.3(3)	N10-C37-C38-N11	-14.8(3)
C21—N4—C12—C13	-162.0(2)	C48—N11—C39—C40	-161.8(2)
C11—N4—C12—C13	80.3 (3)	C38—N11—C39—C40	79.2 (3)
C14—N5—C13—C12	-138.7 (3)	C41—N12—C40—C39	-132.4(3)
N4—C12—C13—N5	69.7 (3)	N11—C39—C40—N12	66.8 (3)
C13—N5—C14—C15	179.3 (2)	C40—N12—C41—C42	179.6 (2)
N5-C14-C15-C16	174.6 (3)	N12—C41—C42—C43	168.0 (3)
N5-C14-C15-C20	-6.4 (4)	N12—C41—C42—C47	-12.5(4)
C20—C15—C16—C17	0.4 (4)	C47—C42—C43—C44	0.4 (4)
C14—C15—C16—C17	179.4 (3)	C41—C42—C43—C44	179.9 (3)
C15—C16—C17—C18	-0.4 (5)	C42—C43—C44—C45	-0.6(5)
C16—C17—C18—C19	-0.1 (5)	C43—C44—C45—C46	0.4 (5)
C17—C18—C19—C20	0.7 (5)	C44—C45—C46—C47	0.0 (5)
C17—C18—C19—N6	179.0 (3)	C44—C45—C46—N13	179.5 (3)
O3—N6—C19—C20	1.4 (4)	O9—N13—C46—C47	-7.6 (4)
O4—N6—C19—C20	179.5 (3)	O10—N13—C46—C47	171.4 (3)
O3—N6—C19—C18	-176.9 (3)	O9—N13—C46—C45	172.9 (3)
O4—N6—C19—C18	1.2 (4)	O10—N13—C46—C45	-8.1 (4)
C18—C19—C20—C15	-0.8 (4)	C45—C46—C47—C42	-0.2 (4)
N6—C19—C20—C15	-179.0 (2)	N13—C46—C47—C42	-179.7 (2)

C16—C15—C20—C19	0.2 (4)	C43—C42—C47—C46	0.0 (4)
C14—C15—C20—C19	-178.8 (2)	C41—C42—C47—C46	-179.5 (2)
C9—N3—C21—N4	166.4 (2)	C36—N10—C48—N11	161.3 (2)
C10—N3—C21—N4	37.1 (3)	C37—N10—C48—N11	31.6 (3)
C9—N3—C21—C22	-73.1 (3)	C36—N10—C48—C49	-79.5 (3)
C10—N3—C21—C22	157.6 (2)	C37—N10—C48—C49	150.8 (2)
C12—N4—C21—N3	-170.3 (2)	C39—N11—C48—N10	-165.4 (2)
C11—N4—C21—N3	-46.1 (2)	C38—N11—C48—N10	-41.1 (3)
C12—N4—C21—C22	70.3 (3)	C39—N11—C48—C49	75.7 (3)
C11—N4—C21—C22	-165.5 (2)	C38—N11—C48—C49	-160.0 (2)
N3—C21—C22—C23	125.4 (3)	N10-C48-C49-C50	129.1 (3)
N4—C21—C22—C23	-120.5 (3)	N11-C48-C49-C50	-117.3 (3)
N3—C21—C22—C27	-54.5 (3)	N10-C48-C49-C54	-51.1 (3)
N4—C21—C22—C27	59.5 (3)	N11—C48—C49—C54	62.4 (3)
C27—C22—C23—C24	0.4 (4)	C54—C49—C50—C51	0.5 (4)
C21—C22—C23—C24	-179.5 (3)	C48—C49—C50—C51	-179.7 (3)
C22—C23—C24—C25	0.2 (5)	C49—C50—C51—C52	0.1 (4)
C23—C24—C25—C26	-0.4(5)	C50—C51—C52—C53	-0.6 (4)
C24—C25—C26—C27	-0.1 (5)	C51—C52—C53—C54	0.3 (4)
C24—C25—C26—N7	178.0 (3)	C51—C52—C53—N14	177.8 (3)
O6—N7—C26—C25	168.9 (4)	O12—N14—C53—C54	-22.7 (4)
O5—N7—C26—C25	-10.9 (5)	O11—N14—C53—C54	157.1 (3)
O6—N7—C26—C27	-13.0 (6)	O12—N14—C53—C52	159.7 (3)
O5—N7—C26—C27	167.3 (3)	O11—N14—C53—C52	-20.4 (4)
C25—C26—C27—C22	0.7 (5)	C52—C53—C54—C49	0.3 (4)
N7—C26—C27—C22	-177.3 (3)	N14—C53—C54—C49	-177.2 (2)
C23—C22—C27—C26	-0.9 (4)	C50—C49—C54—C53	-0.7 (4)
C21—C22—C27—C26	179.1 (3)	C48—C49—C54—C53	179.5 (2)