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1-Diphenylmethylene-2-(9H-fluoren-9vlidene)hydrazine

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Key indicators: single-crystal X-ray study; T = 110 K; mean σ (C–C) = 0.002 Å; R factor = 0.037; wR factor = 0.102; data-to-parameter ratio = 14.6.

In the title molecule, $C_{26}H_{18}N_2$, the 9*H*-fluorene unit is almost planar, as the cyclopentadiene ring makes dihedral angles of 1.12 (6) and 1.46 (6) $^{\circ}$ with the fused benzene rings. The dihedral angle between the two phenyl rings of the diphenylmethylene residue is $61.78 (6)^{\circ}$.

Related literature

For the synthesis, see: Lewis & Glaser (2002). For the crystal structures of some aromatic azines, for example, fluorenone azine, see: Hagen et al. (1977). For the other heterocyclic aldehyde azines, see: Chen et al. (1995). For quadratic nonlinear optical properties, see: Wolff & Wortmann (1999).



Experimental

Crystal data

$C_{26}H_{18}N_2$	$V = 3736.31 (10) \text{ Å}^3$
$M_r = 358.42$	Z = 8
Monoclinic, $C2/c$	Cu Ka radiation
a = 22.8362 (3) Å	$\mu = 0.58 \text{ mm}^{-1}$
b = 13.1432 (2) Å	$T = 110 { m K}$
c = 12.4642 (2) Å	$0.46 \times 0.41 \times 0.32$ r
$\beta = 92.874 \ (1)^{\circ}$	

Data collection

Oxford Xcalibur diffractometer with a Ruby Gemini detector Absorption correction: multi-scan (CrysAlis PRO; Oxford Diffraction, 2009) $T_{\min} = 0.955, T_{\max} = 1.000$

Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.037$ $wR(F^2) = 0.102$ S = 1.063682 reflections

 mm^{-1} $41 \times 0.32 \text{ mm}$

7177 measured reflections 3682 independent reflections 3147 reflections with $I > 2\sigma(I)$ $R_{\rm int} = 0.019$

253 parameters H-atom parameters constrained $\Delta \rho_{\rm max} = 0.23 \ {\rm e} \ {\rm \AA}^{-1}$ $\Delta \rho_{\rm min} = -0.20 \text{ e } \text{\AA}^{-3}$

Data collection: CrysAlis PRO (Oxford Diffraction, 2009); cell refinement: CrysAlis PRO; data reduction: CrysAlis PRO; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008): program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: ORTEP-3 (Farrugia, 1997); software used to prepare material for publication: PLATON (Spek, 2009).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: TK2612).

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R. Archana, R. Anbazhagan, K. R. Sankaran, A. Thiruvalluvar and R. J. Butcher

S1. Comment

Azines have received attention due to their unusual reactivity and spectral properties. For instance they are potential nonlinear optical (NLO) material. Molecular materials with quadratic nonlinear optical properties are currently attracting considerable interest (Wolff & Wortmann, 1999; Chen *et al.*, 1995). Some crystal structures are known (Hagen *et al.*, 1977). Optoelectronics has stimulated the search of highly nonlinear organic crystals for efficient signal processing. The title compound is an example of unsymmetrical fluorenone azine and shows a nonlinear optical behaviour. Herein, we report its crystal structure.

In the title molecule, $C_{26}H_{18}N_2$, the 9*H*-fluorene unit is planar. The cyclopentadiene ring makes dihedral angles of 1.12 (6)° and 1.46 (6)° with the fused benzene rings. The dihedral angle between the two phenyl rings of the diphenyl-methylene residue is 61.78 (6)°.

S2. Experimental

The compound was prepared in accord with literature precedents Lewis & Glaser (2002). The mixture of fluorenone hydrazone (1.94 g, 0.01 mol) and benzophenone (1.82 g, 0.01 mol) in ethanol with acetic acid was refluxed for 2 h. A mixture was cooled to room temperature over several hours. The solid obtained was separated, dried and then recrystallized from absolute ethanol. The yield of isolated product was (3.07 g, 78%).

S3. Refinement

H atoms were positioned geometrically and allowed to ride on their parent atoms, with C—H = 0.95 Å. $U_{iso}(H) = 1.2U_{eq}(C)$.



Figure 1

The molecular structure of the title compound, showing the atom-numbering scheme and displacement ellipsoids drawn at the 50% probability level. H atoms are shown as small spheres of arbitrary radius.

1-Diphenylmethylene-2-(9H-fluoren-9-ylidene)hydrazine

Crystal data

 $C_{26}H_{18}N_2$ $M_r = 358.42$ Monoclinic, C2/cHall symbol: -C 2yc a = 22.8362 (3) Å b = 13.1432 (2) Å c = 12.4642 (2) Å $\beta = 92.874$ (1)° V = 3736.31 (10) Å³ Z = 8

Data collection

Oxford Xcalibur diffractometer with a Ruby Gemini detector Radiation source: Enhance (Cu) X-ray Source F(000) = 1504 $D_x = 1.274 \text{ Mg m}^{-3}$ Melting point: 377 K Cu Ka radiation, $\lambda = 1.54184 \text{ Å}$ Cell parameters from 4987 reflections $\theta = 5.1-73.9^{\circ}$ $\mu = 0.58 \text{ mm}^{-1}$ T = 110 KChunk, pale-yellow $0.46 \times 0.41 \times 0.32 \text{ mm}$

Graphite monochromator Detector resolution: 10.5081 pixels mm⁻¹ ω scans

Absorption correction: multi-scan	$R_{\rm int} = 0.019$
(CrysAlis PRO; Oxford Diffraction, 2009)	$\theta_{\rm max} = 74.1^{\circ}, \ \theta_{\rm min} = 5.2^{\circ}$
$T_{\min} = 0.955, T_{\max} = 1.000$	$h = -27 \rightarrow 28$
7177 measured reflections	$k = -10 \rightarrow 15$
3682 independent reflections	$l = -14 \rightarrow 15$
3147 reflections with $I > 2\sigma(I)$	
Refinement	
Refinement on F^2	Secondary atom site location: difference Fourier
Least-squares matrix: full	map
$R[F^2 > 2\sigma(F^2)] = 0.037$	Hydrogen site location: inferred from
$wR(F^2) = 0.102$	neighbouring sites
S = 1.06	H-atom parameters constrained
3682 reflections	$w = 1/[\hat{\sigma^2}(F_o^2) + (0.0563P)^2 + 1.6279P]$
253 parameters	where $P = (F_o^2 + 2F_c^2)/3$
0 restraints	$(\Delta/\sigma)_{\rm max} = 0.001$
Primary atom site location: structure-invariant	$\Delta a_{mm} = 0.23 \text{ e} \text{ Å}^{-3}$

Special details

direct methods

Geometry. Bond distances, angles *etc*. have been calculated using the rounded fractional coordinates. All su's are estimated from the variances of the (full) variance-covariance matrix. The cell e.s.d.'s are taken into account in the estimation of distances, angles and torsion angles

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > 2\sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

 $\Delta \rho_{\rm min} = -0.20 \text{ e} \text{ Å}^{-3}$

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	
N1	0.35481 (4)	0.16268 (8)	0.34487 (8)	0.0276 (3)	
N2	0.30117 (4)	0.20980 (8)	0.32203 (8)	0.0266 (3)	
C1	0.48097 (6)	0.08981 (10)	0.38410 (10)	0.0325 (4)	
C2	0.54135 (6)	0.07751 (12)	0.40371 (11)	0.0381 (4)	
C3	0.57819 (6)	0.16072 (12)	0.41540 (11)	0.0385 (4)	
C4	0.55662 (6)	0.25969 (11)	0.40685 (10)	0.0329 (4)	
C4A	0.49686 (5)	0.27237 (10)	0.38678 (9)	0.0264 (3)	
C4B	0.46148 (5)	0.36564 (10)	0.37429 (9)	0.0252 (3)	
C5	0.47889 (5)	0.46657 (10)	0.37629 (9)	0.0291 (4)	
C6	0.43594 (6)	0.54174 (10)	0.36409 (10)	0.0309 (4)	
C7	0.37714 (6)	0.51540 (10)	0.35090 (9)	0.0295 (4)	
C8	0.35919 (5)	0.41379 (10)	0.34822 (9)	0.0262 (3)	
C8A	0.40189 (5)	0.33819 (9)	0.35879 (9)	0.0238 (3)	
C9	0.39839 (5)	0.22522 (9)	0.35779 (9)	0.0247 (3)	
C9A	0.45920 (5)	0.18833 (10)	0.37629 (9)	0.0266 (3)	
C10	0.25572 (5)	0.16399 (9)	0.35694 (9)	0.0225 (3)	
C11	0.25793 (5)	0.07200 (8)	0.42731 (9)	0.0215 (3)	
C12	0.22316 (5)	-0.01253 (9)	0.39994 (9)	0.0259 (3)	
C13	0.22468 (5)	-0.09829 (9)	0.46475 (10)	0.0281 (3)	
C14	0.25979 (5)	-0.09989 (9)	0.55906 (10)	0.0277 (3)	

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $(Å^2)$

C15	0.29376 (5)	-0.01569 (9)	0.58763 (9)	0.0264 (3)
C16	0.29369 (5)	0.06937 (9)	0.52151 (9)	0.0233 (3)
C21	0.19789 (5)	0.20994 (9)	0.32457 (9)	0.0226 (3)
C22	0.19408 (5)	0.28377 (9)	0.24323 (9)	0.0257 (3)
C23	0.14141 (6)	0.33068 (10)	0.21489 (10)	0.0319 (4)
C24	0.09125 (6)	0.30600 (11)	0.26812 (11)	0.0348 (4)
C25	0.09424 (5)	0.23372 (10)	0.34938 (10)	0.0307 (4)
C26	0.14706 (5)	0.18576 (9)	0.37725 (9)	0.0251 (3)
H1	0.45565	0.03265	0.37637	0.0390*
H2	0.55735	0.01088	0.40909	0.0457*
Н3	0.61900	0.15017	0.42955	0.0462*
H4	0.58209	0.31666	0.41454	0.0395*
H5	0.51916	0.48422	0.38577	0.0350*
H6	0.44700	0.61143	0.36480	0.0370*
H7	0.34848	0.56765	0.34354	0.0355*
H8	0.31883	0.39663	0.33940	0.0315*
H12	0.19833	-0.01119	0.33649	0.0310*
H13	0.20167	-0.15608	0.44465	0.0337*
H14	0.26053	-0.15842	0.60383	0.0332*
H15	0.31719	-0.01624	0.65280	0.0317*
H16	0.31802	0.12588	0.54040	0.0279*
H22	0.22823	0.30178	0.20708	0.0308*
H23	0.13947	0.37987	0.15898	0.0382*
H24	0.05507	0.33849	0.24892	0.0417*
H25	0.06007	0.21698	0.38608	0.0369*
H26	0.14866	0.13604	0.43264	0.0301*

Atomic displacement parameters (\mathring{A}^2)

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	U ²³
N1	0.0245 (5)	0.0310 (5)	0.0277 (5)	0.0046 (4)	0.0057 (4)	0.0066 (4)
N2	0.0237 (5)	0.0284 (5)	0.0279 (5)	0.0023 (4)	0.0034 (4)	0.0040 (4)
C1	0.0348 (7)	0.0340 (7)	0.0293 (6)	0.0097 (5)	0.0066 (5)	0.0068 (5)
C2	0.0384 (7)	0.0428 (8)	0.0334 (7)	0.0195 (6)	0.0056 (6)	0.0080 (6)
C3	0.0270 (6)	0.0556 (9)	0.0328 (7)	0.0157 (6)	0.0012 (5)	0.0020 (6)
C4	0.0252 (6)	0.0463 (8)	0.0273 (6)	0.0066 (5)	0.0011 (5)	-0.0002(5)
C4A	0.0263 (6)	0.0356 (7)	0.0174 (5)	0.0066 (5)	0.0036 (4)	0.0022 (5)
C4B	0.0245 (5)	0.0346 (7)	0.0167 (5)	0.0055 (5)	0.0023 (4)	0.0011 (4)
C5	0.0276 (6)	0.0364 (7)	0.0233 (6)	0.0004 (5)	0.0003 (5)	-0.0011 (5)
C6	0.0379 (7)	0.0302 (6)	0.0245 (6)	0.0014 (5)	0.0011 (5)	-0.0001 (5)
C7	0.0343 (7)	0.0320 (7)	0.0224 (6)	0.0103 (5)	0.0023 (5)	0.0028 (5)
C8	0.0242 (5)	0.0336 (6)	0.0210 (5)	0.0069 (5)	0.0028 (4)	0.0044 (5)
C8A	0.0247 (6)	0.0314 (6)	0.0157 (5)	0.0036 (5)	0.0039 (4)	0.0034 (4)
C9	0.0240 (6)	0.0310 (6)	0.0195 (5)	0.0056 (4)	0.0060 (4)	0.0059 (4)
C9A	0.0254 (6)	0.0350 (7)	0.0198 (5)	0.0067 (5)	0.0055 (4)	0.0050 (5)
C10	0.0261 (6)	0.0219 (6)	0.0198 (5)	0.0001 (4)	0.0029 (4)	-0.0030 (4)
C11	0.0229 (5)	0.0207 (5)	0.0214 (5)	0.0021 (4)	0.0051 (4)	-0.0015 (4)
C12	0.0282 (6)	0.0255 (6)	0.0240 (5)	-0.0002(5)	0.0022 (4)	-0.0043 (5)

C13	0.0291 (6)	0.0205 (6)	0.0354 (6)	-0.0017 (4)	0.0086 (5)	-0.0045 (5)
C14	0.0299 (6)	0.0221 (6)	0.0318 (6)	0.0065 (5)	0.0100 (5)	0.0046 (5)
C15	0.0270 (6)	0.0279 (6)	0.0245 (6)	0.0077 (5)	0.0026 (4)	0.0009 (5)
C16	0.0232 (5)	0.0220 (5)	0.0248 (6)	0.0016 (4)	0.0036 (4)	-0.0036 (4)
C21	0.0262 (6)	0.0213 (5)	0.0202 (5)	0.0000 (4)	0.0015 (4)	-0.0038 (4)
C22	0.0289 (6)	0.0251 (6)	0.0233 (6)	0.0005 (5)	0.0035 (4)	-0.0010 (4)
C23	0.0347 (7)	0.0315 (7)	0.0291 (6)	0.0053 (5)	-0.0012 (5)	0.0031 (5)
C24	0.0274 (6)	0.0375 (7)	0.0389 (7)	0.0072 (5)	-0.0029 (5)	-0.0018 (6)
C25	0.0241 (6)	0.0344 (7)	0.0339 (7)	-0.0012 (5)	0.0043 (5)	-0.0048 (5)
C26	0.0276 (6)	0.0245 (6)	0.0232 (5)	-0.0018 (4)	0.0029 (4)	-0.0029 (4)

Geometric parameters (Å, °)

N1—N2	1,3893 (13)	C15—C16	1,3889 (16)
N1—C9	1.2946 (15)	C21—C22	1.4029 (16)
N2-C10	1.2940 (15)	C21—C26	1.3986 (16)
C1-C2	1 3976 (19)	C^{22} $-C^{23}$	1 3817 (18)
C1—C9A	1.3887 (18)	C23—C24	1.3906 (19)
C2-C3	1.383 (2)	C24—C25	1.3878 (19)
C3—C4	1.393 (2)	C25—C26	1.3896 (17)
C4—C4A	1.3851 (18)	C1—H1	0.9500
C4A—C4B	1.4721 (18)	C2—H2	0.9500
C4A—C9A	1.4020 (18)	C3—H3	0.9500
C4B—C5	1.3847 (18)	C4—H4	0.9500
C4B—C8A	1.4117 (16)	С5—Н5	0.9500
C5—C6	1.3951 (18)	С6—Н6	0.9500
C6—C7	1.3884 (19)	С7—Н7	0.9500
C7—C8	1.3969 (19)	С8—Н8	0.9500
C8—C8A	1.3938 (17)	C12—H12	0.9500
C8A—C9	1.4870 (17)	C13—H13	0.9500
С9—С9А	1.4780 (16)	C14—H14	0.9500
C10—C11	1.4931 (16)	C15—H15	0.9500
C10—C21	1.4893 (16)	C16—H16	0.9500
C11—C12	1.3979 (16)	C22—H22	0.9500
C11—C16	1.3966 (16)	С23—Н23	0.9500
C12—C13	1.3862 (17)	C24—H24	0.9500
C13—C14	1.3895 (17)	С25—Н25	0.9500
C14—C15	1.3877 (17)	C26—H26	0.9500
N1C16	2 9339 (15)	C21…H7 ^{vii}	2 9600
N2C8	3 0012 (16)	$C_{21} H_{16^{v}}$	2.9000
N1H1	2 8800	$C22\cdots H14^{i}$	2.8800
N1H16	2.6600	C22H16v	2.0000
N2H8	2.0000	$C_{22} = H_{10}$	3,0700
N2H16	2.9000	C25H16 ^v	3.0100
N2H22	2.24600	C26···H12	2 9000
N2…H14 ⁱ	2.1000	C26···H16 ^v	2.7800
	3 4960 (18)	H1N1	2.8800
	5.1900 (10)	111 111	2.0000

C1···C2 ⁱⁱⁱ	3.4966 (19)	H1…C2 ⁱⁱⁱ	3.1000
C2…C1 ⁱⁱⁱ	3.4966 (19)	H2…C1 ⁱⁱⁱ	3.0600
C3…C9 ⁱⁱ	3.5752 (18)	H3…C14 ⁱⁱⁱ	2.8400
C3…C15 ⁱⁱⁱ	3.4924 (18)	H3…C15 ⁱⁱⁱ	2.6800
C4···C9 ⁱⁱ	3.5328 (17)	H3…H15 ⁱⁱⁱ	2.5300
C4A…C4A ⁱⁱ	3.4199 (16)	H4…C5	3.0900
C5…C5 ⁱⁱ	3.3384 (16)	H5…C4	3.0800
C5…C5 ^{iv}	3.3036 (16)	H5····C5 ^{iv}	3.0300
C7…C14 ^v	3.5528 (18)	H7…C21 ^{vi}	2.9600
C7…C13 ^v	3.5226 (17)	H7…C13 ^v	3.0100
C8…N2	3.0012 (16)	H7…C14 ^v	2.8400
C8A…C26 ^v	3.5415 (16)	H8…N2	2.5000
C9…C4 ⁱⁱ	3.5328 (17)	H8…H12 ^{vi}	2.5200
C9…C3 ⁱⁱ	3.5752 (18)	H12…C21	2.9100
C12…C26	3.1373 (17)	H12…C26	2.9000
C13···C7 ^v	3.5226 (17)	H12…H26	2.5700
C14…C7 ^v	3.5528 (18)	H12····C7 ^{vii}	2.8500
C15C3 ⁱⁱⁱ	3,4924 (18)	H12···C8 ^{vii}	2.7700
C16…N1	2,9339 (15)	H12···H8 ^{vii}	2.5200
$C16\cdots C2^{v}$	3 5100 (16)	H13H22 ^{vii}	2.6000
$C16 \cdots C21^{v}$	3 4776 (16)	H14···N2 ^{viii}	2.9100
C^{21} ····C16 ^v	3 4776 (16)	H14····C22 ^{viii}	2 8800
C^{22} ····C16 ^v	3 5100 (16)	H14···H22 ^{viii}	2.0000
$C_{26}^{26} C_{8A^{v}}^{v}$	3 5415 (16)	H15H3 ⁱⁱⁱ	2.5300
C26···C12	3 1373 (17)	H15C23 ^v	3.0700
C1H2 ⁱⁱⁱ	3.0600	H16N1	2 6600
C2H1 ⁱⁱⁱ	3 1000	H16N2	2.0000
C4H5	3 0800	$H16C21^{v}$	2.7400
C5H4	3,0000	H16C22v	2.7700
C5H5 ^{iv}	3.0300	H16C25 ^v	2.9700
C7H12 ^{vi}	2 8500	H16C26 ^v	2 7800
C8H26v	2.8300	H10 C20	2.7800
C8 H120	2.8200	$H_{22} = H_{2}$ $H_{22} = H_{14}^{i}$	2.4000
C8AH26v	2.7700	H_{22} C_{12} ^{vi}	2.4200
C11H26	2.9200	H_{22} H	3.0200
C12H26	2.0400	H22	2.7700
C12···H20	2.0300	H22H13	2.0000
	2.7700	H26C11	2.5200
C13H7v	2.7700	H26C12	2.0400
	3.0100	H26U12	2.0300
	2.8400		2.3700
С14н.з	2.8400		2.8200
С15нз	2.0800	H20C8A	2.9200
C21···H12	2.9100		
N2—N1—C9	114.01 (10)	C22—C23—C24	120.09 (12)
N1—N2—C10	115.95 (10)	C23—C24—C25	119.76 (12)
C2—C1—C9A	117.82 (12)	C24—C25—C26	120.22 (11)
C1—C2—C3	121.10 (14)	C21—C26—C25	120.67 (11)

C^2 C^2 C^4	121 20 (12)	C_{2} C_{1} U_{1}	121.00
$C_2 = C_3 = C_4$	121.29 (13)	$C_2 - C_1 - H_1$	121.00
$C_3 = C_4 = C_4 A$	117.00(13) 120.52(12)	$C_{2} = C_{1} = H_{1}$	121.00
C4 = C4A = C4B	130.33(12) 121.08(12)	$C_1 = C_2 = H_2$	119.00
C4 - C4A - C9A	121.06(12) 109.29(10)	$C_3 = C_2 = H_2$	119.00
C4B - C4A - C9A	108.38 (10)	C2-C3-H3	119.00
C4A - C4B - C5	129.81 (11)	C4 - C3 - H3	119.00
C4A - C4B - C8A	108.77 (11)	C3-C4-H4	121.00
C5—C4B—C8A	121.41 (11)	C4A - C4 - H4	121.00
C4B—C5—C6	118.48 (11)	C4B—C5—H5	121.00
C5—C6—C7	120.45 (12)	C6—C5—H5	121.00
C6—C7—C8	121.47 (12)	С5—С6—Н6	120.00
C7—C8—C8A	118.44 (11)	С7—С6—Н6	120.00
C4B—C8A—C8	119.72 (11)	С6—С7—Н7	119.00
C4B—C8A—C9	107.90 (10)	С8—С7—Н7	119.00
C8—C8A—C9	132.38 (11)	С7—С8—Н8	121.00
N1—C9—C8A	132.51 (11)	C8A—C8—H8	121.00
N1—C9—C9A	121.43 (11)	C11—C12—H12	120.00
C8A—C9—C9A	106.06 (10)	C13—C12—H12	120.00
C1—C9A—C4A	120.82 (11)	C12—C13—H13	120.00
C1—C9A—C9	130.32 (12)	C14—C13—H13	120.00
C4A—C9A—C9	108.86 (11)	C13—C14—H14	120.00
N2—C10—C11	124.77 (10)	C15—C14—H14	120.00
N2-C10-C21	115.82 (10)	C14—C15—H15	120.00
C11—C10—C21	119.40 (10)	С16—С15—Н15	120.00
C10-C11-C12	119.88 (10)	С11—С16—Н16	120.00
C10-C11-C16	121.00 (10)	C15—C16—H16	120.00
C12-C11-C16	119 11 (10)	$C_{21} - C_{22} - H_{22}$	120.00
$C_{11} - C_{12} - C_{13}$	120 45 (10)	C_{23} C_{22} H_{22}	119.00
C12 - C13 - C14	120.12(10) 120.12(11)	$C_{22} = C_{23} = H_{23}$	120.00
C12 - C13 - C14	119 77 (11)	$C_{22} = C_{23} = H_{23}$	120.00
C_{14} C_{15} C_{16}	120.38 (11)	C_{23} C_{24} H_{24}	120.00
$C_{11} = C_{15} = C_{10}$	120.33(11) 120.13(11)	$C_{25} = C_{24} = H_{24}$	120.00
$C_{10} = C_{10} = C_{13}$	120.13(11) 110.80(10)	$C_{25} = C_{24} = 1124$	120.00
$C_{10} = C_{21} = C_{22}$	119.09(10) 121.75(10)	$C_{24} = C_{25} = H_{25}$	120.00
$C_{10} = C_{21} = C_{20}$	121.73(10) 118.27(10)	$C_{20} = C_{23} = H_{23}$	120.00
$C_{22} = C_{21} = C_{20}$	116.27(10) 121.00(11)	$C_{21} = C_{20} = H_{20}$	120.00
C21-C22-C23	121.00 (11)	C25—C26—H26	120.00
C9—N1—N2—C10	-14847(11)	C4B—C8A—C9—C9A	1 37 (12)
N2—N1—C9—C8A	3 86 (18)	C8 - C8A - C9 - N1	15(2)
$N_2 N_1 C_9 C_9 A$	-17638(10)	C8 - C8A - C9 - C9A	-17831(12)
N1 - N2 - C10 - C11	6 19 (17)	N1 - C9 - C9A - C1	-0.58(19)
N1 - N2 - C10 - C21	-175.08(10)	N1 - C9 - C9A - C4A	17970(11)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.26(10)	$C_{8} C_{9} C_{9} C_{7} C_{7} C_{7}$	170.70(11)
$C_{2} = C_{1} = C_{2} = C_{3}$	0.20(17)	$C_{0A} = C_{0A} = C_{0A} = C_{0A}$	-0.40(12)
$C_2 = C_1 = C_2 A = C_4 A$	-170.00(10)	$V_{2} = C_{1} = C_{1} = C_{1}$	0.47(12)
$C_2 = C_1 = C_2 = C_4$	-1/9.09(12) -0.8(2)	$N_2 = C_{10} = C_{11} = C_{12}$	-130.13(13)
$C_1 - C_2 - C_3 - C_4$	-0.8(2)	1N2 - CIU - CII - CIO	50.85(17)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.35 (19)	$C_{1} = C_{10} = C_{11} = C_{12}$	31.19(15)
C3—C4—C4A—C4B	1/9.63 (12)	C21—C10—C11—C16	-127.84 (12)

Symmetry codes: (i) x, -y, z-1/2; (ii) -x+1, y, -z+1/2; (iii) -x+1, -y, -z+1; (iv) -x+1, -y+1, -z+1; (v) -x+1/2, -y+1/2, -z+1; (vi) -x+1/2, y+1/2, -z+1/2; (vii) -x+1/2, y-1/2, -z+1/2; (viii) x, -y, z+1/2; (ix) -x, y, -z+1/2.