# 1-(2,4-Dinitrophenyl)-3,3-dinitro-azetidine

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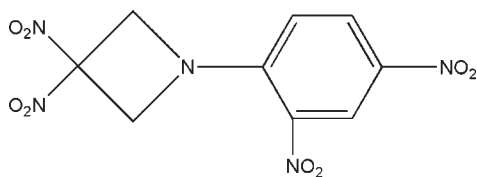
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In the title compound, $C_9H_7N_5O_8$, the dihedral angle between the mean plane of the azetidine ring and that of the benzene ring is 26.1 (1)°; the planes of the two nitro groups of the azetidine ring are aligned at 88.7 (1)°.

## Related literature

Highly nitrated small-ring heterocycles are good candidates for energetic materials because of the increased performance from the additional energy release upon opening of the strained ring system during decomposition, see: Frumkin *et al.* (1999). Azetidine-based explosives, such as 1,3,3-trinitro-azetidine (TNAZ) demonstrate excellent performance, see: Archibald *et al.*, (1990); Hiskey & Coburn (1994*a,b*). The title compound is a derivative of 3,3-dinitroazetidine (DNAZ) (Hiskey *et al.*, 1992, 1993), which is a derivative of TNAZ. For the use of DNAZ in the preparation of a variety of solid energetic compounds, see: Ma *et al.* (2009*a,b,c*); Gao *et al.* (2009).



## Experimental

### Crystal data

| | |
|---|---|
| $C_9H_7N_5O_8$ | $V$ = 1206.3 (6) Å$^3$ |
| $M_r$ = 313.20 | $Z$ = 4 |
| Monoclinic, $P2_1/n$ | Mo $K\alpha$ radiation |
| $a$ = 8.113 (2) Å | $\mu$ = 0.15 mm$^{-1}$ |
| $b$ = 10.676 (3) Å | $T$ = 293 K |
| $c$ = 14.398 (4) Å | 0.31 × 0.26 × 0.20 mm |
| $\beta$ = 104.681 (4)° | |

### Data collection

| | |
|---|---|
| Bruker SMART APEX diffractometer | 2140 independent reflections |
| Absorption correction: none | 1670 reflections with $I > 2\sigma(I)$ |
| 5860 measured reflections | $R_{int}$ = 0.019 |

### Refinement

| | |
|---|---|
| $R[F^2 > 2\sigma(F^2)]$ = 0.038 | 199 parameters |
| $wR(F^2)$ = 0.118 | H-atom parameters constrained |
| $S$ = 1.20 | $\Delta\rho_{max}$ = 0.21 e Å$^{-3}$ |
| 2140 reflections | $\Delta\rho_{min}$ = −0.21 e Å$^{-3}$ |

Data collection: *SMART* (Bruker, 2003); cell refinement: *SAINT* (Bruker, 2003); data reduction: *SAINT*; program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *SHELXTL* (Sheldrick, 2008); software used to prepare material for publication: *SHELXTL*.

## References

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# supporting information

## 1-(2,4-Dinitrophenyl)-3,3-dinitroazetidine

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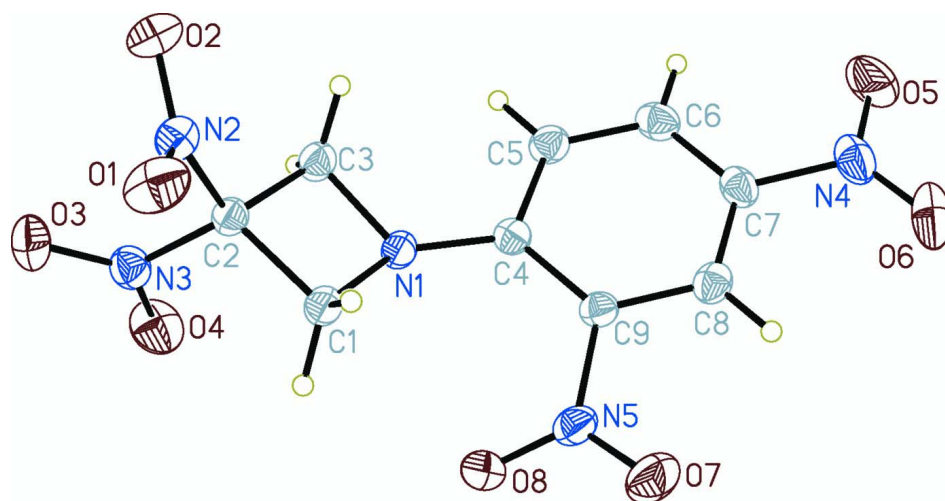
### S1. Comment

Highly nitrated small-ring heterocycles are good candidates for energetic materials because of the increased performance from the additional energy release upon opening of the strained ring system during decomposition (Frumkin *et al.*, 1999). Azetidine-based explosives, such as 1,3,3-trinitroazetidine (TNAZ) (Archibald *et al.*, 1990; Hiskey *et al.*, 1994*a*,*b*) demonstrate excellent performance partly because of the high strain associated with the four-membered ring. As one of the important derivates of TNAZ, 3,3-dinitroazetidine (DNAZ) (Hiskey *et al.*, 1992; Hiskey *et al.*, 1993) can prepare a variety of solid energetic compounds (Ma *et al.*, 2009*a*,*b*,*c*; Gao *et al.*, 2009). The title compound (I) is a DNAZ derivates. The dihedral angle between the azetidine ring and benzene ring is 26.1° and the planes of two nitryl of azetidine ring is 88.7°. There are no important intermolecular contacts in the crystal structure.

### S2. Experimental

A solution of DNAZ (0.2353 g, 1.6 mmol), 2,4-dinitrochlorobenzene (0.33 ml, 1.6 mmol), and $NaHCO_3$ (0.28 g, 3.2 mmol) in dichloromethane (30.0 ml) was stirred under reflux for 20 h. The reaction mixture was concentrated in vacuo, water (30 ml) was added, and the unstable mixture was extracted rapidly with dichloromethane (3 * 15 ml). The combined extracts were dried ($MgSO_4$,), the solvent was concentrated *in vacuo*, and ethanol (20 ml) was added, and the residue was filtrated to give the yellow compound in 30% yield. Crystals were obtained from dichloromethane, by slow evaporation at room temperature. Elemental analysis calculated for $C_9H_7N_5O_8$: C 34.61, N 22.36, H 2.253%; found: C 34.61, N 22.22, H 2.249%. IR (KBr, $cm^{-1}$): 3100.29, 1585.18, 1526.85, 1335.18, 1304.76, 869.25, 820.72.

### S3. Refinement

H atoms were placed at calculated idealized positions and refined using a riding model, with C—H distances in the range 0.93–0.97 Å.

**Figure 1**

The molecular structure of (I), showing the atom-numbering scheme. Displacement ellipsoids are drawn at the 30% probability level and H atoms are drawn as spheres of arbitrary radius.

**1-(2,4-Dinitrophenyl)-3,3-dinitroazetidine**

*Crystal data*

| | |
|---|---|
| $C_9H_7N_5O_8$ | $F(000) = 640$ |
| $M_r = 313.20$ | $D_x = 1.724$ Mg m$^{-3}$ |
| Monoclinic, $P2_1/n$ | Mo $K\alpha$ radiation, $\lambda = 0.71073$ Å |
| Hall symbol: -P 2yn | Cell parameters from 1904 reflections |
| $a = 8.113$ (2) Å | $\theta = 2.4$–26.0° |
| $b = 10.676$ (3) Å | $\mu = 0.15$ mm$^{-1}$ |
| $c = 14.398$ (4) Å | $T = 293$ K |
| $\beta = 104.681$ (4)° | Block, yellow |
| $V = 1206.3$ (6) Å$^3$ | $0.31 \times 0.26 \times 0.20$ mm |
| $Z = 4$ | |

*Data collection*

| | |
|---|---|
| Bruker APEXII diffractometer | 1670 reflections with $I > 2\sigma(I)$ |
| Radiation source: fine-focus sealed tube | $R_{int} = 0.019$ |
| Graphite monochromator | $\theta_{max} = 25.1°$, $\theta_{min} = 2.4°$ |
| $\varphi$ and $\omega$ scans | $h = -9 \rightarrow 9$ |
| 5860 measured reflections | $k = -11 \rightarrow 12$ |
| 2140 independent reflections | $l = -17 \rightarrow 17$ |

*Refinement*

| | |
|---|---|
| Refinement on $F^2$ | Secondary atom site location: difference Fourier map |
| Least-squares matrix: full | |
| $R[F^2 > 2\sigma(F^2)] = 0.038$ | Hydrogen site location: inferred from neighbouring sites |
| $wR(F^2) = 0.118$ | |
| $S = 1.20$ | H-atom parameters constrained |
| 2140 reflections | $w = 1/[\sigma^2(F_o^2) + (0.063P)^2 + 0.0921P]$ |
| 199 parameters | where $P = (F_o^2 + 2F_c^2)/3$ |
| 0 restraints | $(\Delta/\sigma)_{max} = 0.028$ |
| Primary atom site location: structure-invariant direct methods | $\Delta\rho_{max} = 0.21$ e Å$^{-3}$ |
| | $\Delta\rho_{min} = -0.21$ e Å$^{-3}$ |

*Special details*

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement**. Refinement of $F^2$ against ALL reflections. The weighted $R$-factor $wR$ and goodness of fit $S$ are based on $F^2$, conventional $R$-factors $R$ are based on $F$, with $F$ set to zero for negative $F^2$. The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating $R$-factors(gt) *etc*. and is not relevant to the choice of reflections for refinement. $R$-factors based on $F^2$ are statistically about twice as large as those based on $F$, and $R$- factors based on ALL data will be even larger.

*Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (Å$^2$)*

|  | *x* | *y* | *z* | $U_{iso}*/U_{eq}$ |
|---|---|---|---|---|
| O2 | 0.56725 (18) | 0.14099 (15) | 0.95776 (10) | 0.0576 (4) |
| N1 | 0.06769 (18) | 0.16834 (14) | 0.89752 (10) | 0.0360 (4) |
| C4 | −0.0303 (2) | 0.25527 (16) | 0.92696 (11) | 0.0324 (4) |
| O8 | −0.18514 (19) | 0.22095 (15) | 0.72839 (10) | 0.0566 (4) |
| N2 | 0.4618 (2) | 0.14859 (15) | 0.88135 (11) | 0.0419 (4) |
| C9 | −0.1501 (2) | 0.33688 (17) | 0.86745 (11) | 0.0334 (4) |
| N3 | 0.3038 (2) | −0.04265 (16) | 0.84420 (11) | 0.0435 (4) |
| N5 | −0.20374 (19) | 0.32296 (17) | 0.76316 (11) | 0.0429 (4) |
| C1 | 0.1375 (2) | 0.16202 (18) | 0.81278 (12) | 0.0376 (4) |
| H1A | 0.1660 | 0.2430 | 0.7906 | 0.045* |
| H1B | 0.0689 | 0.1131 | 0.7602 | 0.045* |
| C3 | 0.2168 (2) | 0.10713 (18) | 0.96128 (12) | 0.0384 (4) |
| H3B | 0.1908 | 0.0288 | 0.9886 | 0.046* |
| H3A | 0.2834 | 0.1618 | 1.0105 | 0.046* |
| N4 | −0.2936 (2) | 0.53426 (18) | 1.04331 (15) | 0.0556 (5) |
| C7 | −0.2070 (2) | 0.43720 (19) | 1.00353 (13) | 0.0411 (5) |
| O3 | 0.4390 (2) | −0.07976 (16) | 0.83333 (12) | 0.0679 (5) |
| C6 | −0.0999 (2) | 0.35558 (19) | 1.06406 (13) | 0.0441 (5) |
| H6 | −0.0866 | 0.3606 | 1.1300 | 0.053* |
| C2 | 0.2905 (2) | 0.09108 (16) | 0.87430 (12) | 0.0340 (4) |
| C8 | −0.2340 (2) | 0.42800 (18) | 0.90514 (13) | 0.0388 (4) |
| H8 | −0.3082 | 0.4828 | 0.8648 | 0.047* |
| O1 | 0.4830 (2) | 0.19814 (17) | 0.80972 (11) | 0.0655 (5) |
| O7 | −0.2721 (2) | 0.41195 (17) | 0.71504 (11) | 0.0671 (5) |
| O6 | −0.3804 (2) | 0.61021 (15) | 0.98923 (15) | 0.0718 (5) |
| O4 | 0.1762 (2) | −0.10369 (15) | 0.83337 (12) | 0.0678 (5) |
| C5 | −0.0131 (2) | 0.26685 (19) | 1.02664 (12) | 0.0407 (5) |
| H5 | 0.0596 | 0.2125 | 1.0683 | 0.049* |
| O5 | −0.2740 (3) | 0.5369 (2) | 1.13090 (13) | 0.0877 (7) |

*Atomic displacement parameters (Å$^2$)*

|  | $U^{11}$ | $U^{22}$ | $U^{33}$ | $U^{12}$ | $U^{13}$ | $U^{23}$ |
|---|---|---|---|---|---|---|
| O2 | 0.0396 (8) | 0.0687 (11) | 0.0560 (9) | −0.0018 (7) | −0.0034 (7) | 0.0035 (7) |
| N1 | 0.0336 (8) | 0.0430 (9) | 0.0315 (7) | 0.0082 (7) | 0.0083 (6) | 0.0019 (6) |
| C4 | 0.0289 (9) | 0.0349 (10) | 0.0344 (9) | −0.0039 (7) | 0.0098 (7) | −0.0011 (7) |

| | | | | | | |
|---|---|---|---|---|---|---|
| O8 | 0.0486 (9) | 0.0709 (11) | 0.0446 (8) | 0.0096 (8) | 0.0012 (6) | −0.0167 (7) |
| N2 | 0.0366 (9) | 0.0427 (9) | 0.0457 (9) | 0.0007 (7) | 0.0092 (7) | 0.0018 (7) |
| C9 | 0.0295 (9) | 0.0389 (10) | 0.0311 (8) | −0.0015 (8) | 0.0062 (7) | −0.0005 (7) |
| N3 | 0.0490 (10) | 0.0384 (9) | 0.0433 (9) | 0.0025 (8) | 0.0123 (7) | −0.0007 (7) |
| N5 | 0.0306 (8) | 0.0574 (11) | 0.0387 (9) | 0.0037 (8) | 0.0050 (7) | 0.0027 (8) |
| C1 | 0.0342 (10) | 0.0451 (11) | 0.0338 (9) | 0.0067 (8) | 0.0089 (7) | 0.0017 (8) |
| C3 | 0.0375 (10) | 0.0404 (11) | 0.0364 (9) | 0.0059 (8) | 0.0075 (7) | 0.0039 (8) |
| N4 | 0.0443 (10) | 0.0497 (12) | 0.0779 (13) | −0.0058 (9) | 0.0253 (9) | −0.0222 (10) |
| C7 | 0.0352 (10) | 0.0414 (11) | 0.0497 (11) | −0.0052 (8) | 0.0164 (8) | −0.0131 (9) |
| O3 | 0.0609 (10) | 0.0625 (11) | 0.0811 (11) | 0.0189 (8) | 0.0196 (8) | −0.0179 (8) |
| C6 | 0.0430 (11) | 0.0556 (13) | 0.0356 (9) | −0.0058 (9) | 0.0135 (8) | −0.0069 (9) |
| C2 | 0.0320 (9) | 0.0330 (10) | 0.0359 (9) | 0.0019 (7) | 0.0068 (7) | 0.0003 (7) |
| C8 | 0.0309 (9) | 0.0364 (10) | 0.0483 (10) | −0.0013 (8) | 0.0086 (8) | 0.0015 (8) |
| O1 | 0.0474 (9) | 0.0908 (13) | 0.0596 (9) | −0.0145 (8) | 0.0159 (7) | 0.0171 (8) |
| O7 | 0.0700 (11) | 0.0777 (12) | 0.0478 (8) | 0.0224 (9) | 0.0043 (7) | 0.0165 (8) |
| O6 | 0.0689 (11) | 0.0460 (10) | 0.1116 (14) | 0.0094 (9) | 0.0432 (10) | −0.0049 (10) |
| O4 | 0.0725 (11) | 0.0498 (10) | 0.0845 (11) | −0.0217 (8) | 0.0263 (9) | −0.0118 (8) |
| C5 | 0.0397 (10) | 0.0480 (12) | 0.0339 (10) | 0.0030 (9) | 0.0083 (8) | 0.0032 (8) |
| O5 | 0.0877 (13) | 0.1094 (16) | 0.0693 (11) | 0.0103 (11) | 0.0260 (10) | −0.0450 (11) |

## Geometric parameters (Å, º)

| | | | |
|---|---|---|---|
| O2—N2 | 1.2133 (19) | C1—C2 | 1.530 (2) |
| N1—C4 | 1.358 (2) | C1—H1A | 0.9700 |
| N1—C1 | 1.471 (2) | C1—H1B | 0.9700 |
| N1—C3 | 1.473 (2) | C3—C2 | 1.528 (3) |
| C4—C5 | 1.412 (2) | C3—H3B | 0.9700 |
| C4—C9 | 1.420 (2) | C3—H3A | 0.9700 |
| O8—N5 | 1.224 (2) | N4—O6 | 1.217 (2) |
| N2—O1 | 1.209 (2) | N4—O5 | 1.231 (2) |
| N2—C2 | 1.499 (2) | N4—C7 | 1.449 (3) |
| C9—C8 | 1.375 (3) | C7—C6 | 1.375 (3) |
| C9—N5 | 1.461 (2) | C7—C8 | 1.381 (3) |
| N3—O4 | 1.199 (2) | C6—C5 | 1.370 (3) |
| N3—O3 | 1.213 (2) | C6—H6 | 0.9300 |
| N3—C2 | 1.504 (2) | C8—H8 | 0.9300 |
| N5—O7 | 1.223 (2) | C5—H5 | 0.9300 |
| | | | |
| C4—N1—C1 | 132.01 (15) | C2—C3—H3B | 113.9 |
| C4—N1—C3 | 124.20 (14) | N1—C3—H3A | 113.9 |
| C1—N1—C3 | 93.91 (13) | C2—C3—H3A | 113.9 |
| N1—C4—C5 | 117.53 (15) | H3B—C3—H3A | 111.1 |
| N1—C4—C9 | 126.61 (15) | O6—N4—O5 | 122.96 (19) |
| C5—C4—C9 | 115.86 (16) | O6—N4—C7 | 118.91 (19) |
| O1—N2—O2 | 125.62 (17) | O5—N4—C7 | 118.1 (2) |
| O1—N2—C2 | 116.82 (15) | C6—C7—C8 | 121.05 (18) |
| O2—N2—C2 | 117.57 (16) | C6—C7—N4 | 119.64 (18) |
| C8—C9—C4 | 121.83 (16) | C8—C7—N4 | 119.31 (18) |

| | | | |
|---|---|---|---|
| C8—C9—N5 | 115.41 (15) | C5—C6—C7 | 119.63 (17) |
| C4—C9—N5 | 122.54 (16) | C5—C6—H6 | 120.2 |
| O4—N3—O3 | 125.76 (19) | C7—C6—H6 | 120.2 |
| O4—N3—C2 | 115.52 (16) | N2—C2—N3 | 105.99 (14) |
| O3—N3—C2 | 118.72 (17) | N2—C2—C3 | 116.55 (14) |
| O7—N5—O8 | 123.01 (16) | N3—C2—C3 | 114.47 (15) |
| O7—N5—C9 | 118.51 (17) | N2—C2—C1 | 116.00 (15) |
| O8—N5—C9 | 118.39 (15) | N3—C2—C1 | 114.20 (14) |
| N1—C1—C2 | 88.22 (12) | C3—C2—C1 | 89.46 (13) |
| N1—C1—H1A | 113.9 | C9—C8—C7 | 119.30 (17) |
| C2—C1—H1A | 113.9 | C9—C8—H8 | 120.3 |
| N1—C1—H1B | 113.9 | C7—C8—H8 | 120.4 |
| C2—C1—H1B | 113.9 | C6—C5—C4 | 122.15 (17) |
| H1A—C1—H1B | 111.1 | C6—C5—H5 | 118.9 |
| N1—C3—C2 | 88.23 (12) | C4—C5—H5 | 118.9 |
| N1—C3—H3B | 113.9 | | |
| | | | |
| C1—N1—C4—C5 | −151.31 (18) | O1—N2—C2—C3 | −140.71 (18) |
| C3—N1—C4—C5 | −15.0 (3) | O2—N2—C2—C3 | 39.7 (2) |
| C1—N1—C4—C9 | 28.7 (3) | O1—N2—C2—C1 | −37.3 (2) |
| C3—N1—C4—C9 | 165.05 (17) | O2—N2—C2—C1 | 143.13 (16) |
| N1—C4—C9—C8 | −175.18 (17) | O4—N3—C2—N2 | −178.93 (15) |
| C5—C4—C9—C8 | 4.9 (3) | O3—N3—C2—N2 | 1.3 (2) |
| N1—C4—C9—N5 | 10.4 (3) | O4—N3—C2—C3 | 51.2 (2) |
| C5—C4—C9—N5 | −169.55 (16) | O3—N3—C2—C3 | −128.56 (18) |
| C8—C9—N5—O7 | 23.2 (2) | O4—N3—C2—C1 | −50.0 (2) |
| C4—C9—N5—O7 | −162.06 (18) | O3—N3—C2—C1 | 130.29 (18) |
| C8—C9—N5—O8 | −153.55 (17) | N1—C3—C2—N2 | 122.10 (16) |
| C4—C9—N5—O8 | 21.2 (2) | N1—C3—C2—N3 | −113.44 (15) |
| C4—N1—C1—C2 | 148.25 (19) | N1—C3—C2—C1 | 3.06 (14) |
| C3—N1—C1—C2 | 3.19 (14) | N1—C1—C2—N2 | −122.59 (15) |
| C4—N1—C3—C2 | −152.23 (17) | N1—C1—C2—N3 | 113.68 (16) |
| C1—N1—C3—C2 | −3.19 (14) | N1—C1—C2—C3 | −3.07 (14) |
| O6—N4—C7—C6 | 175.89 (19) | C4—C9—C8—C7 | −2.9 (3) |
| O5—N4—C7—C6 | −3.2 (3) | N5—C9—C8—C7 | 171.93 (16) |
| O6—N4—C7—C8 | −4.3 (3) | C6—C7—C8—C9 | −1.1 (3) |
| O5—N4—C7—C8 | 176.56 (19) | N4—C7—C8—C9 | 179.16 (17) |
| C8—C7—C6—C5 | 2.7 (3) | C7—C6—C5—C4 | −0.4 (3) |
| N4—C7—C6—C5 | −177.53 (18) | N1—C4—C5—C6 | 176.83 (18) |
| O1—N2—C2—N3 | 90.61 (19) | C9—C4—C5—C6 | −3.2 (3) |
| O2—N2—C2—N3 | −88.97 (19) | | |