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# Di-*tert*-butyl 3,3'-(2,2'-bi-1*H*-imidazole-1,1'-diyl)dipropanoate

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Key indicators: single-crystal X-ray study; T = 295 K; mean  $\sigma$ (C–C) = 0.005 Å; R factor = 0.077; wR factor = 0.190; data-to-parameter ratio = 19.2.

In the title compound,  $C_{20}H_{20}N_4O_4$ , the complete molecule is generated by a crystallographic centre of symmetry. The conformation is stabilized by two intramolecular  $C-H\cdots N$  links.

#### **Related literature**

For the background to 2, 2'-biimidazole derivatives, see: Barnett *et al.* (1999, 2002); Liang *et al.* (2009); Zhang & Liang (2009); Zhang, Zhang, Ren *et al.* (2009); Zhang, Zhang, Xu *et al.* (2009). For the synthesis, see: Barnett *et al.* (1999).



#### **Experimental**

#### Crystal data

 $\begin{array}{l} C_{20}H_{30}N_4O_4\\ M_r=390.48\\ Monoclinic, P2_1/c\\ a=7.0321\ (14)\ \text{\AA}\\ b=17.484\ (4)\ \text{\AA}\\ c=8.9681\ (18)\ \text{\AA}\\ \beta=100.80\ (3)^\circ \end{array}$ 

 $V = 1083.1 \text{ (4) } \text{\AA}^{3}$  Z = 2Mo K\alpha radiation  $\mu = 0.08 \text{ mm}^{-1}$  T = 295 K $0.48 \times 0.42 \times 0.14 \text{ mm}$  9620 measured reflections

 $R_{\rm int} = 0.077$ 

2453 independent reflections

1474 reflections with  $I > 2\sigma(I)$ 

Data collection

Rigaku R-AXIS RAPID

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diffractometer
Absorption correction: multi-scan
(ABSCOR; Higashi, 1995)
T_{\min} = 0.960, T_{\max} = 0.988
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#### Refinement

$R[F^2 > 2\sigma(F^2)] = 0.077$	128 parameters
$vR(F^2) = 0.190$	H-atom parameters constrained
S = 1.02	$\Delta \rho_{\rm max} = 0.32 \text{ e } \text{\AA}^{-3}$
2453 reflections	$\Delta \rho_{\rm min} = -0.24 \text{ e} \text{ \AA}^{-3}$

#### Table 1

Hydrogen-bond geometry (Å, °).

 $D-H\cdots A$  D-H  $H\cdots A$   $D\cdots A$   $D-H\cdots A$  

 C10-H10B\cdots N2^i
 0.97
 2.46
 2.960 (3)
 111

Symmetry code: (i) -x + 1, -y + 1, -z + 1.

Data collection: *RAPID-AUTO* (Rigaku, 1998); cell refinement: *RAPID-AUTO*; data reduction: *CrystalStructure* (Rigaku/MSC, 2004); program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *SHELXTL* (Sheldrick, 2008); software used to prepare material for publication: *SHELXL97*.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: FB2148).

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# supporting information

Acta Cryst. (2009). E65, o1577 [doi:10.1107/S1600536809021369]

# Di-tert-butyl 3,3'-(2,2'-bi-1H-imidazole-1,1'-diyl)dipropanoate

## Ke Wang, Yue-Jiao Li, Ting-Ting Zhang and Hong-Ze Liang

### S1. Comment

Biimidazole is a potentially polydentate ligand, but its chemistry is less developed in comparison to the imidazole chemistry. The reason may be a limited solubility of biimidazole in common organic solvents. Although several new disubstituted 2,2'-biimidazoles have been recently synthesized (Barnett *et al.*, 1999; Barnett *et al.*, 2002), a few metal complexes based on biimidazole derivatives are reported (Zhang, Zhang, Ren *et al.*, 2009). In the course of our ongoing study, we have successfully synthesized a series of biimidazole derivatives with terminal carboxylic, hydroxyl, phosphino, imino groups which can be used as ligands in the coordination chemistry (Zhang & Liang, 2009; Zhang, Zhang, Xu *et al.*, 2009) and cross-coupling reactions (Liang *et al.*, 2009). These ligands exhibit rich coordination patterns and catalytic properties. Here we report the synthesis and the crystal structure of the title compound which is an intermediate of those above mentioned ligands. As shown in Fig. 1, the biimidazole ring atoms (C6, C7, C9, N1, N2 and their inversion-related partners) exhibit essentially coplanar mutual orientation [the dihedral angle is 0.00 (1)°], and the value of the torsion angle C9—N1—C10—C5 is -77.53 (30)°. In the crystal structure, there are weak C-H…N interactions (Tab. 1, Fig. 2).

#### **S2. Experimental**

The title compound was prepared according to a published procedure (Barnett *et al.*, 1999). 0.2 g (5 mmol) of NaOH was added to a suspension of 3 g (22.4 mmol) of 2,2'-biimidazole in 100 ml of DMF (dimethylformamide) at 80°C. The resulting mixture was stirred for 30 min. In the course of this time the mixture gradually turned into a clear pale yellow solution. 7.12 g (55.6 mmol) butyl acrylate in 10 ml of DMF was added dropwise in several minutes to the solution and the reaction was stirred at 80°C for 8 h until the heating was stopped. The DMF was removed *via* vacuum distillation in a hot oil bath at 100°C. The resulting black brown oil was dissolved in water (30 ml) and extracted with CH<sub>2</sub>Cl<sub>2</sub>. The organic layer was washed with water, and then evaporated under reduced pressure to yield a white product (7.4 g, 85%). The product was dissolved in 95% ethanol (30 ml) and cooled slowly in a refrigerator to afford colourless block crystals of average size 1.5 mm×1.2 mm×0.5 mm that were suitable for the X-ray analysis.

#### **S3. Refinement**

All the hydrogens were discernible in the difference electron density map. Nevertheless, the hydrogens were situated into the idealized positions. The C-H distances were constrained to 0.93, 0.96 and 0.97 Å for aryl, methylene and methyl hydrogens, respectively.  $U_{iso}(H) = 1.2 U_{eq}(C_{aryl}); U_{iso}(H) = 1.2 U_{eq}(C_{methylene}); U_{iso}(H) = 1.5 U_{eq}(C_{methyl}).$ 



## Figure 1

View of the title molecule with the displacement ellipsoids at the 45% probability level. The labelling of the non-H atoms is also given. The symmetry code (i):-x+1, -y+1, -z+1.



### Figure 2

A section of the title structure. The C-H…N hydrogen bonds (Tab. 1) are shown as dashed lines.

#### Di-tert-butyl 3,3'-(2,2'-bi-1H-imidazole-1,1'-diyl)dipropanoate

#### Crystal data

 $C_{20}H_{30}N_4O_4$   $M_r = 390.48$ Monoclinic,  $P2_1/c$ Hall symbol: -P 2ybc a = 7.0321 (14) Å b = 17.484 (4) Å c = 8.9681 (18) Å  $\beta = 100.80 (3)^\circ$   $V = 1083.1 (4) \text{ Å}^3$ Z = 2

#### Data collection

Rigaku R-AXIS RAPID	9620 measured reflections
diffractometer	2453 independent reflections
Radiation source: fine-focus sealed tube	1474 reflections with $I > 2\sigma(I)$
Graphite monochromator	$R_{\rm int} = 0.077$
Detector resolution: 0 pixels mm <sup>-1</sup>	$\theta_{\rm max} = 27.5^{\circ}, \ \theta_{\rm min} = 3.2^{\circ}$
$\omega$ scans	$h = -9 \rightarrow 9$
Absorption correction: multi-scan	$k = -22 \rightarrow 22$
(ABSCOR; Higashi, 1995)	$l = -11 \rightarrow 10$
$T_{\min} = 0.960, \ T_{\max} = 0.988$	
Refinement	
Refinement on $F^2$	Primary atom site location: structure-inva
Least-squares matrix: full	direct methods

F(000) = 420

 $\theta = 3.0-27.5^{\circ}$  $\mu = 0.08 \text{ mm}^{-1}$ 

Plate. colourless

 $0.48 \times 0.42 \times 0.14 \text{ mm}$ 

T = 295 K

 $D_{\rm x} = 1.197 {\rm Mg} {\rm m}^{-3}$ 

Mo *K* $\alpha$  radiation,  $\lambda = 0.71073$  Å

Cell parameters from 1478 reflections

ariant  $R[F^2 > 2\sigma(F^2)] = 0.077$ Secondary atom site location: difference Fourier  $wR(F^2) = 0.190$ man S = 1.02Hydrogen site location: difference Fourier map 2453 reflections H-atom parameters constrained 128 parameters  $w = 1/[\sigma^2(F_0^2) + (0.0718P)^2 + 0.3943P]$ 0 restraints where  $P = (F_o^2 + 2F_c^2)/3$ 59 constraints  $(\Delta/\sigma)_{\rm max} < 0.001$  $\Delta \rho_{\rm max} = 0.32 \text{ e } \text{\AA}^{-3}$  $\Delta \rho_{\rm min} = -0.24 \ {\rm e} \ {\rm \AA}^{-3}$ 

#### Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(Å^2)$ 

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	
N1	0.3460 (3)	0.51573 (11)	0.30746 (19)	0.0410 (5)	
N2	0.6689 (3)	0.51901 (13)	0.3698 (2)	0.0522 (6)	
C10	0.1400 (3)	0.50398 (14)	0.3101 (3)	0.0454 (6)	

H10A	0.0628	0.5297	0.2237	0.054*
H10B	0.1099	0.5268	0.4016	0.054*
O2	0.2468 (3)	0.32667 (12)	0.1854 (2)	0.0717 (6)
01	0.0366 (3)	0.40123 (12)	0.0365 (2)	0.0774 (7)
C9	0.5051 (3)	0.50815 (13)	0.4210 (2)	0.0415 (6)
C8	0.1171 (4)	0.38275 (15)	0.1612 (3)	0.0525 (6)
C7	0.6104 (4)	0.53329 (17)	0.2169 (3)	0.0568 (7)
H7A	0.6939	0.5428	0.1501	0.068*
C6	0.4159 (4)	0.53160 (15)	0.1774 (2)	0.0504 (6)
H6A	0.3431	0.5396	0.0809	0.061*
C5	0.0864 (4)	0.41992 (15)	0.3056 (3)	0.0520 (6)
H5A	0.1644	0.3940	0.3914	0.062*
H5B	-0.0484	0.4147	0.3144	0.062*
C4	0.2854 (6)	0.2868 (2)	0.0492 (4)	0.0905 (11)
H4A	0.3139	0.3238	-0.0242	0.109*
H4B	0.1724	0.2577	0.0027	0.109*
C3	0.4524 (6)	0.2349 (2)	0.0943 (5)	0.0958 (12)
H3A	0.4239	0.2005	0.1722	0.115*
H3B	0.4664	0.2039	0.0072	0.115*
C2	0.6387 (6)	0.2728 (2)	0.1520 (5)	0.1045 (13)
H2B	0.6290	0.3010	0.2434	0.125*
H2C	0.6653	0.3092	0.0770	0.125*
C1	0.8074 (6)	0.2163 (3)	0.1876 (7)	0.1289 (18)
H1A	0.9241	0.2435	0.2285	0.193*
H1B	0.8229	0.1904	0.0962	0.193*
H1C	0.7809	0.1795	0.2605	0.193*

Atomic displacement parameters  $(\mathring{A}^2)$ 

	$U^{11}$	$U^{22}$	$U^{33}$	$U^{12}$	$U^{13}$	$U^{23}$
N1	0.0380 (10)	0.0516 (11)	0.0319 (9)	0.0030 (9)	0.0030 (7)	0.0023 (8)
N2	0.0407 (11)	0.0834 (16)	0.0336 (10)	0.0013 (10)	0.0097 (8)	0.0031 (10)
C10	0.0364 (11)	0.0564 (15)	0.0413 (12)	0.0045 (11)	0.0017 (9)	0.0019 (10)
O2	0.0728 (13)	0.0805 (15)	0.0564 (12)	0.0151 (11)	-0.0018 (9)	-0.0074 (10)
01	0.0988 (16)	0.0791 (15)	0.0457 (11)	0.0097 (12)	-0.0087 (10)	0.0001 (9)
C9	0.0377 (11)	0.0553 (14)	0.0304 (11)	0.0037 (11)	0.0033 (8)	-0.0010 (9)
C8	0.0518 (14)	0.0532 (15)	0.0491 (15)	-0.0082 (12)	0.0006 (11)	0.0019 (11)
C7	0.0522 (15)	0.086 (2)	0.0343 (12)	-0.0015 (13)	0.0134 (10)	0.0047 (12)
C6	0.0539 (14)	0.0675 (17)	0.0289 (11)	0.0016 (12)	0.0051 (10)	0.0033 (11)
C5	0.0474 (13)	0.0629 (16)	0.0444 (13)	-0.0046 (12)	0.0054 (10)	0.0044 (12)
C4	0.100 (3)	0.098 (3)	0.069 (2)	0.020 (2)	0.0058 (18)	-0.0199 (19)
C3	0.097 (3)	0.095 (3)	0.098 (3)	-0.005 (2)	0.026 (2)	-0.021 (2)
C2	0.101 (3)	0.095 (3)	0.115 (3)	-0.006(2)	0.013 (2)	-0.001 (2)
C1	0.087 (3)	0.101 (3)	0.198 (5)	0.000 (2)	0.025 (3)	0.031 (3)

Geometric parameters (Å, °)

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$					
$\begin{split} & N1 - C6 & I.376 (3) & C5 - H5A & 0.9700 \\ & N1 - C10 & I.468 (3) & C5 - H5B & 0.9700 \\ & N2 - C7 & I.338 (3) & C4 - C3 & I.480 (5) \\ & N2 - C7 & I.378 (3) & C4 - H4A & 0.9700 \\ & C10 - C5 & I.516 (3) & C4 - H4B & 0.9700 \\ & C10 - H10A & 0.9700 & C3 - C2 & I.473 (5) \\ & C10 - H10B & 0.9700 & C3 - C2 & I.473 (5) \\ & C10 - H10B & 0.9700 & C3 - H3B & 0.9700 \\ & O2 - C4 & I.475 (4) & C2 - C1 & I.531 (5) \\ & O1 - C8 & I.199 (3) & C2 - H2B & 0.9700 \\ & C9 - C9 & I.460 (4) & C2 - H2B & 0.9700 \\ & C9 - C9 & I.460 (4) & C2 - H2B & 0.9700 \\ & C7 - C6 & I.347 (3) & C1 - H1B & 0.9600 \\ & C7 - C6 & I.347 (3) & C1 - H1B & 0.9600 \\ & C7 - H7A & 0.9300 & C1 - H1C & 0.9600 \\ & C7 - H7A & 0.9300 & C1 - H1C & 0.9600 \\ & C6 - N1 - C10 & 13.015 (19) & H5A - C5 - H5B & 108.0 \\ & C6 - N1 - C10 & 12.35 (18) & O2 - C4 - C3 & 108.9 (3) \\ & C9 - N2 - C7 & 104.6 (2) & O2 - C4 - H4A & 109.9 \\ & N1 - C10 - H10A & 109.2 & C3 - C4 - H4B & 109.9 \\ & N1 - C10 - H10A & 109.2 & C2 - C4 - H4B & 109.9 \\ & N1 - C10 - H10A & 109.2 & C2 - C3 - C4 & H15.3 (4) \\ & H10A - C10 - H10B & 109.2 & C2 - C3 - C4 & H3B & 108.4 \\ & C8 - O2 - C4 & 116.1 (2) & C4 - C3 - H3B & 108.4 \\ & C8 - O2 - C4 & 115.3 (4) \\ & H10A - C10 - H10B & 109.2 & C2 - C3 - H3B & 108.4 \\ & N2 - C9 - O9 & 124.5 (2) & C4 - C3 - H3B & 108.4 \\ & N2 - C9 - C9 & 124.5 (2) & C4 - C3 - H3B & 108.4 \\ & N2 - C9 - C9 & 124.5 (2) & C1 - C2 - C2 & 109.0 \\ & C6 - C7 - N1 & 111.5 19 (2) & C3 - C2 $	N1—C9	1.371 (3)	С6—Н6А	0.9300	
N1-C10       1.468 (3)       C3-H5B       0.9700         N2-C9       1.331 (3)       C4-C3       1.480 (5)         N2-C7       1.378 (3)       C4-H4A       0.9700         C10-L5       1.516 (3)       C4-H4B       0.9700         C10-H10A       0.9700       C3-C2       1.473 (5)         C10-H10B       0.9700       C3-H3A       0.9700         O2-C8       1.329 (3)       C3-H3B       0.9700         C2-C4       1.475 (4)       C2-C1       1.531 (5)         O1-C5       1.500 (4)       C1-H1A       0.9600         C7-C6       1.500 (4)       C1-H1B       0.9600         C7-C6       1.500 (4)       C1-H1B       0.9600         C7-H7A       0.9300       C1-H1B       0.9600         C7-H7A       0.9300       C1-H1C       0.9600         C7-H7A       0.9300       C1-H1C       0.9600         C9-N1-C10       13.15 (19)       H5A-C5-H5B       108.0         C9-N2-C7       104.6 (2)       0.2-C4-H4A       109.9         N1-C10-H10A       109.2       0.2-C4-H4A       109.9         N1-C10-H10A       109.2       C3-C4-H4B       108.3         C5-C10-H10A	N1—C6	1.376 (3)	С5—Н5А	0.9700	
N2-C9       1.331 (3)       C4-C3       1.480 (5)         N2-C7       1.378 (3)       C4-H4A       0.9700         C10-C5       1.516 (3)       C4-H4B       0.9700         C10-H10A       0.9700       C3-H3A       0.9700         C2-C8       1.329 (3)       C3-H3B       0.9700         O2-C8       1.329 (3)       C3-H3B       0.9700         O2-C4       1.475 (4)       C2-C1       1.531 (5)         O1-C8       1.199 (3)       C2-H2B       0.9700         C8-C5       1.500 (4)       C1-H1A       0.9600         C7-H7A       0.9300       C1-H1B       0.9600         C7-H7A       0.9300       C1-H1C       0.9600         C9-N1-C6       106.13 (18)       C10-C5-H5B       108.0         C6-N1-C10       130.15 (19)       H5A-C5-H5B       108.0         C6-N1-C10       123.53 (18)       O2-C4-C3       108.9 (3)         C9-N1-C5       112.1 (2)       C3-C4-H4A       109.9         N1-C10-H10A       109.2       C2-C3-C4       H33         N1-C10-H10A       109.2       C2-C3-C4       H34         N1-C10-H10A       109.2       C2-C3-H3A       108.4         C5-C10-H10B<	N1-C10	1.468 (3)	С5—Н5В	0.9700	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	N2—C9	1.331 (3)	C4—C3	1.480 (5)	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	N2—C7	1.378 (3)	C4—H4A	0.9700	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C10—C5	1.516 (3)	C4—H4B	0.9700	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C10—H10A	0.9700	C3—C2	1.473 (5)	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C10—H10B	0.9700	С3—НЗА	0.9700	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O2—C8	1.329 (3)	С3—Н3В	0.9700	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O2—C4	1.475 (4)	C2—C1	1.531 (5)	
C9-C9'1.460 (4)C2-H2C0.9700C8-C51.500 (4)C1-H1A0.9600C7-C61.347 (3)C1-H1B0.9600C7-H7A0.9300C1-H1C0.9600C9-N1-C6106.13 (18)C10-C5-H5B109.3C9-N1-C10130.15 (19)H5A-C5-H5B108.0C6-N1-C10123.53 (18)O2-C4-C3108.9 (3)C9-N2-C7104.6 (2)O2-C4-H4A109.9N1-C10-C5112.1 (2)C3-C4-H4A109.9N1-C10-H10A109.2C3-C4-H4B109.9SC5-C10-H10A109.2C3-C4-H4B109.9N1-C10-H10B109.2C3-C4-H4B108.3C5-C10-H10B109.2C2-C3-C4115.3 (4)H10A-C10-H10B109.2C2-C3-H3A108.4C8-O2-C4116.1 (2)C4-C3-H3B108.4N2-C9-N1111.59 (19)C2-C3-H3B108.4N2-C9-C9'124.5 (2)C4-C3-H3B108.4N1-C9-C9123.9 (2)H3A-C2-H3B108.4N1-C9-C9123.9 (2)H3A-C2-H3B109.0O1-C8-C5124.7 (3)C3-C2-C1112.7 (4)O1-C8-C5124.7 (3)C3-C2-H2B109.0C6-C7-N2110.9 (2)C3-C2-H2C109.0C6-C7-N2110.9 (2)C3-C2-H2C109.0C6-C7-N4124.5H2B-C2-H2C107.8C7-C6-N1106.7 (2)C2-C1-H1IB109.5C8-C5-C10111.6 (2)C2-C1-H1IB109.5C8-C5-H5A109.3H1A-C1-H1C	O1—C8	1.199 (3)	C2—H2B	0.9700	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C9—C9 <sup>i</sup>	1.460 (4)	C2—H2C	0.9700	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C8—C5	1.500 (4)	C1—H1A	0.9600	
C7-H7A0.9300C1-H1C0.9600C9-N1-C6106.13 (18)C10-C5-H5B109.3C9-N1-C10130.15 (19)H5A-C5-H5B108.0C6-N1-C10123.53 (18)O2-C4-C3108.9 (3)C9-N2-C7104.6 (2)O2-C4-H4A109.9N1-C10-C5112.1 (2)C3-C4-H4A109.9N1-C10-H10A109.2O2-C4-H4B109.9SC-C10-H10A109.2C3-C4-H4B109.9N1-C10-H10B109.2C3-C4-H4B108.3C5-C10-H10B109.2C2-C3-C4115.3 (4)H10A-C10-H10B107.9C2-C3-H3A108.4C8-O2-C4116.1 (2)C4-C3-H3B108.4N2-C9-N111.59 (19)C2-C3-H3B108.4N2-C9-N111.59 (19)C2-C3-H3B108.4N2-C9-C9'123.9 (2)H3A-C3-H3B107.5O1-C8-C5124.7 (3)C3-C2-H2B109.0C6-C7-N2112.6 (2)C1-C2-H2B109.0C6-C7-N210.9 (2)C3-C2-H2C109.0C6-C7-H7A124.5C1-C2-H2C109.0C6-C7-H7A124.5H2B-C2-H2C107.8C7-C6-N1106.7 (2)C2-C1-H1A109.5C7-C6-N1106.7 (2)C2-C1-H1B109.5N1-C6-H6A126.6HA-C1-H1B109.5N1-C6-H6A126.6HA-C1-H1B109.5C7-C6-N5A109.3H1A-C1-H1C109.5C8-C5-H5A109.3H1A-C1-H1C109.5C8-C5-H5A109.3H1A-C1-H1C109.5 </td <td>С7—С6</td> <td>1.347 (3)</td> <td>C1—H1B</td> <td>0.9600</td> <td></td>	С7—С6	1.347 (3)	C1—H1B	0.9600	
C9-N1-C6106.13 (18)C10-C5-H5B109.3C9-N1-C10130.15 (19)H5A-C5-H5B108.0C6-N1-C10123.53 (18)O2-C4-C3108.9 (3)C9-N2-C7104.6 (2)O2-C4-H4A109.9N1-C10-C5112.1 (2)C3-C4-H4B109.9N1-C10-H10A109.2O2-C4-H4B109.9SC-C10-H10A109.2C3-C4-H4B109.9N1-C10-H10B109.2C2-C3-C4115.3 (4)H10A-C10-H10B109.2C2-C3-H3A108.4C5-C10-H10B107.9C2-C3-H3A108.4C8-O2-C4116.1 (2)C4-C3-H3B108.4N2-C9-N1111.59 (19)C2-C3-H3B108.4N1-C9-C9i123.9 (2)H3A-C3-H3B108.4N1-C9-C9i123.9 (2)H3A-C3-H3B108.4N1-C9-C9i123.9 (2)H3A-C3-H3B109.0O2-C8-C5124.7 (3)C3-C2-H2B109.0O2-C8-C5112.6 (2)C1-C2-H2B109.0C6-C7-N2110.9 (2)C3-C2-H2C109.0C6-C7-N4124.5H2B-C2-H2C107.8C7-C6-N1106.7 (2)C2-C1-H1A109.5C7-C6-N1106.7 (2)C2-C1-H1B109.5N1-C6-H6A126.6H1A-C1-H1B109.5N1-C6-H6A126.6H1A-C1-H1B109.5C8-C5-H5A109.3H1A-C1-H1C109.5C8-C5-H5A109.3H1A-C1-H1C109.5C8-C5-H5A109.3H1A-C1-H1C109.5	C7—H7A	0.9300	C1—H1C	0.9600	
C9-N1-C10101.15 (19)H5A-C5-H5B108.0C6-N1-C10123.53 (18) $02-C4-C3$ 108.9 (3)C9-N2-C7104.6 (2) $02-C4-H4A$ 109.9N1-C10-C5112.1 (2)C3-C4-H4A109.9N1-C10-H10A109.2 $02-C4-H4B$ 109.9C5-C10-H10A109.2C3-C4-H4B109.9N1-C10-H10B109.2H4A-C4-H4B108.3C5-C10-H10B109.2C2-C3-C4115.3 (4)H10A-C10-H10B107.9C2-C3-H3A108.4C8-02-C4116.1 (2)C4-C3-H3B108.4N2-C9-N1111.59 (19)C2-C3-H3B108.4N1-C9-C9 <sup>6</sup> 124.5 (2)C4-C3-H3B107.5O1-C8-O2122.7 (3)C3-C2-C1112.7 (4)O1-C8-C5124.7 (3)C3-C2-H2B109.0C2-C8-C5112.6 (2)C1-C2-H2B109.0C6-C7-N2110.9 (2)C3-C2-H2C109.0C6-C7-N4124.5H2-C2-H2C107.8C7-C6-N1106.7 (2)C2-C1-H1A109.5C7-C6-H6A126.6C2-C1-H1B109.5N1-C6-H6A126.6H1A-C1-H1B109.5N1-C6-H5A109.3H1A-C1-H1C109.5C7-C5-H5A109.3H1A-C1-H1C109.5	C9N1C6	106 13 (18)	C10_C5_H5B	109 3	
C5N1C10130.15 (17)110.17C4C5100.5C6N1C10123.53 (18) $O2-C4-C3$ 108.9 (3)C9N2-C7104.6 (2) $O2-C4-C4$ 109.9N1-C10-C5112.1 (2)C3-C4-H4A109.9SC10-H10A109.2 $O2-C4$ -H4B109.9C5-C10-H10A109.2C3-C4-H4B108.3C5-C10-H10B109.2C2-C3-C4115.3 (4)H10A-C10-H10B107.9C2-C3-H3A108.4C8-O2-C4116.1 (2)C4-C3-H3A108.4N2-C9-N1111.59 (19)C2-C3-H3B108.4N2-C9-C9'124.5 (2)C4-C3-H3B108.4N1-C9-C9'123.9 (2)H3A-C3-H3B108.4N1-C9-C9'124.5 (2)C4-C3-H3B109.0O2-C8-C5124.7 (3)C3-C2-C1112.7 (4)O1-C8-C5124.7 (3)C3-C2-H2B109.0O2-C8-C5112.6 (2)C1-C2-H2C109.0C6-C7-H7A124.5C1-C2-H2C109.0C6-C7-H7A124.5H2B-C2-H2C107.8C7-C6-H6A126.6C2-C1-H1B109.5N1-C6-H6A126.6C2-C1-H1B109.5N1-C6-H6A126.6H1A-C1-H1B109.5C8-C5-C10111.6 (2)C2-C1-H1C109.5C8-C5-H5A109.3H1A-C1-H1C109.5C8-C5-H5A109.3H1B-C1-H1C109.5	C9-N1-C10	130 15 (19)	H5A-C5-H5B	108.0	
$CO = N2 - C7$ $102.05 (12)$ $O2 - C4 - H4A$ $109.9$ $N1 - C10 - C5$ $112.1 (2)$ $C3 - C4 - H4A$ $109.9$ $N1 - C10 - H10A$ $109.2$ $O2 - C4 - H4B$ $109.9$ $C5 - C10 - H10A$ $109.2$ $C3 - C4 - H4B$ $109.9$ $N1 - C10 - H10B$ $109.2$ $C3 - C4 - H4B$ $108.3$ $C5 - C10 - H10B$ $109.2$ $C2 - C3 - C4$ $115.3 (4)$ $H10A - C10 - H10B$ $109.2$ $C2 - C3 - H3A$ $108.4$ $C8 - O2 - C4$ $116.1 (2)$ $C4 - C3 - H3A$ $108.4$ $N2 - C9 - N1$ $111.59 (19)$ $C2 - C3 - H3B$ $108.4$ $N2 - C9 - C9^{i}$ $124.5 (2)$ $C4 - C3 - H3B$ $108.4$ $N2 - C9 - C9^{i}$ $123.9 (2)$ $H3A - C3 - H3B$ $108.4$ $N1 - C9 - C9^{i}$ $123.9 (2)$ $H3A - C3 - H3B$ $109.0$ $O2 - C8 - C5$ $124.7 (3)$ $C3 - C2 - H2B$ $109.0$ $O2 - C8 - C5$ $112.6 (2)$ $C1 - C2 - H2B$ $109.0$ $C6 - C7 - N2$ $110.9 (2)$ $C3 - C2 - H2C$ $109.0$ $C6 - C7 - H7A$ $124.5$ $C1 - C2 - H2C$ $109.0$ $C6 - C7 - H7A$ $124.5$ $H2B - C2 - H2C$ $107.8$ $C7 - C6 - N1$ $106.7 (2)$ $C2 - C1 - H1B$ $109.5$ $N1 - C6 - H6A$ $126.6$ $H1A - C1 - H1B$ $109.5$ $N1 - C6 - H6A$ $126.6$ $H1A - C1 - H1C$ $109.5$ $C8 - C5 - H5A$ $109.3$ $H1B - C1 - H1C$ $109.5$ $C8 - C5 - H5B$ $109.3$ $H1B - C1 - H1C$ $109.5$ <td>C6-N1-C10</td> <td>123 53 (18)</td> <td><math>0^{2}-C^{4}-C^{3}</math></td> <td>108.9(3)</td> <td></td>	C6-N1-C10	123 53 (18)	$0^{2}-C^{4}-C^{3}$	108.9(3)	
ConstructionConstructionConstructionConstructionN1-C10-C5112.1 (2)C3-C4-H4A109.9N1-C10-H10A109.2C2-C4-H4B109.9C5-C10-H10A109.2C3-C4-H4B109.9N1-C10-H10B109.2C2-C3-C4115.3 (4)H10A-C10-H10B107.9C2-C3-H3A108.4C8-02-C4116.1 (2)C4-C3-H3A108.4C8-02-C4116.1 (2)C4-C3-H3B108.4N2-C9-N1111.59 (19)C2-C3-H3B108.4N1-C9-C9i123.9 (2)H3A-C3-H3B108.4N1-C9-C9i123.9 (2)H3A-C3-H3B107.5O1-C8-O2122.7 (3)C3-C2-C1112.7 (4)O1-C8-C5124.7 (3)C3-C2-H2B109.0O2-C8-C5110.9 (2)C3-C2-H2C109.0C6-C7-N2110.9 (2)C3-C2-H2C109.0C6-C7-H7A124.5C1-C2-H2C109.0N2-C7-H7A124.5H2B-C2-H2C107.8C7-C6-H6A126.6C2-C1-H1A109.5N1-C6-H6A126.6C2-C1-H1B109.5N1-C6-H6A126.6H1A-C1-H1B109.5C8-C5-C10111.6 (2)C2-C1-H1C109.5C8-C5-H5A109.3H1A-C1-H1C109.5C8-C5-H5B109.3H1B-C1-H1C109.5	C9 - N2 - C7	125.55(10) 104 6 (2)	$\Omega^2$ $C^4$ $H^4A$	109.9	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$N_1 - C_{10} - C_5$	104.0(2) 112 1 (2)	$C_{3}$ $C_{4}$ $H_{4A}$	109.9	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	N1 - C10 - H10A	109.2	$\Omega^2 - C4 - H4B$	109.9	
$C10 - H101$ $107.2$ $C10 - H101$ $109.2$ $H4A - C4 - H4B$ $108.3$ $C5 - C10 - H10B$ $109.2$ $C2 - C3 - C4$ $115.3$ (4) $H10A - C10 - H10B$ $107.9$ $C2 - C3 - H3A$ $108.4$ $C8 - O2 - C4$ $116.1$ (2) $C4 - C3 - H3A$ $108.4$ $N2 - C9 - N1$ $111.59$ (19) $C2 - C3 - H3B$ $108.4$ $N2 - C9 - C9^i$ $124.5$ (2) $C4 - C3 - H3B$ $108.4$ $N1 - C9 - C9^i$ $123.9$ (2) $H3A - C3 - H3B$ $108.4$ $N1 - C9 - C9^i$ $123.9$ (2) $H3A - C3 - H3B$ $107.5$ $O1 - C8 - O2$ $122.7$ (3) $C3 - C2 - C1$ $112.7$ (4) $O1 - C8 - C5$ $124.7$ (3) $C3 - C2 - H2B$ $109.0$ $O2 - C8 - C5$ $112.6$ (2) $C1 - C2 - H2B$ $109.0$ $O2 - C8 - C5$ $112.6$ (2) $C1 - C2 - H2B$ $109.0$ $C6 - C7 - N2$ $110.9$ (2) $C3 - C2 - H2C$ $109.0$ $C6 - C7 - H7A$ $124.5$ $H2B - C2 - H2C$ $109.0$ $N2 - C7 - H7A$ $124.5$ $H2B - C2 - H2C$ $109.0$ $N - C6 - H6A$ $126.6$ $C1 - C1 - H1B$ $109.5$ $C7 - C6 - M1$ $106.7$ (2) $C2 - C1 - H1B$ $109.5$ $N - C6 - H6A$ $126.6$ $H1A - C1 - H1B$ $109.5$ $N - C6 - H6A$ $126.6$ $H1A - C1 - H1B$ $109.5$ $C8 - C5 - H5A$ $109.3$ $H1B - C1 - H1C$ $109.5$ $C8 - C5 - H5B$ $109.3$ $H1B - C1 - H1C$ $109.5$	$C_{5}$ $C_{10}$ $H_{10A}$	109.2	C3 - C4 - H4B	109.9	
$R_1 = C_1S_1 = R_1R_1S_1 = R_1R_2S_1 = R_1R_2S_1$	N1 - C10 - H10B	109.2	H4A - C4 - H4B	108.3	
Constrained103.2C2C3C1113.5H10A $-C10$ H10B107.9C2C3H3A108.4C8 $-O2$ C4116.1(2)C4C3H3A108.4N2 $-C9$ N1111.59(19)C2C3H3B108.4N2 $-C9$ C9124.5(2)C4C3H3B108.4N1 $-C9$ C9123.9(2)H3AH3AC3H3B107.5O1 $-C8$ C2122.7(3)C3C2C2C1112.7(4)O1 $-C8$ C5124.7(3)C3C2H2B109.002C3C2H3AC3C3C3C3C3C2H3AC3C3C3C3C3C2C4C3H3BH3 </td <td><math>C_{5}</math> <math>C_{10}</math> <math>H_{10B}</math></td> <td>109.2</td> <td><math>C^2 - C^3 - C^4</math></td> <td>115 3 (4)</td> <td></td>	$C_{5}$ $C_{10}$ $H_{10B}$	109.2	$C^2 - C^3 - C^4$	115 3 (4)	
Initial101.7101.7101.7101.7 $C8-O2-C4$ 116.1 (2) $C4-C3-H3A$ 108.4 $N2-C9-N1$ 111.59 (19) $C2-C3-H3B$ 108.4 $N2-C9-C9^i$ 124.5 (2) $C4-C3-H3B$ 108.4 $N1-C9-C9^i$ 123.9 (2)H3A-C3-H3B107.5 $O1-C8-O2$ 122.7 (3) $C3-C2-C1$ 112.7 (4) $O1-C8-C5$ 124.7 (3) $C3-C2-H2B$ 109.0 $O2-C8-C5$ 112.6 (2) $C1-C2-H2B$ 109.0 $C6-C7-N2$ 110.9 (2) $C3-C2-H2C$ 109.0 $C6-C7-H7A$ 124.5 $C1-C2-H2C$ 109.0 $N2-C7-H7A$ 124.5 $H2B-C2-H2C$ 107.8 $C7-C6-N1$ 106.7 (2) $C2-C1-H1A$ 109.5 $C7-C6-H6A$ 126.6 $C2-C1-H1B$ 109.5 $N1-C6-H6A$ 126.6 $H1A-C1-H1B$ 109.5 $N1-C6-H6A$ 126.6 $H1A-C1-H1C$ 109.5 $C8-C5-H5A$ 109.3 $H1B-C1-H1C$ 109.5 $C8-C5-H5B$ 109.3 $H1B-C1-H1C$ 109.5	$H_{10A}$ $-C_{10}$ $H_{10B}$	107.9	C2 - C3 - H3A	108.4	
$N2-C9-N1$ $111.59 (19)$ $C2-C3-H3B$ $108.4$ $N2-C9-C9^i$ $124.5 (2)$ $C4-C3-H3B$ $108.4$ $N1-C9-C9^i$ $123.9 (2)$ $H3A-C3-H3B$ $107.5$ $O1-C8-O2$ $122.7 (3)$ $C3-C2-C1$ $112.7 (4)$ $O1-C8-C5$ $124.7 (3)$ $C3-C2-H2B$ $109.0$ $O2-C8-C5$ $112.6 (2)$ $C1-C2-H2B$ $109.0$ $C6-C7-N2$ $110.9 (2)$ $C3-C2-H2C$ $109.0$ $C6-C7-H7A$ $124.5$ $C1-C2-H2C$ $109.0$ $N2-C7-H7A$ $124.5$ $H2B-C2-H2C$ $109.0$ $N2-C7-H7A$ $124.5$ $H2B-C2-H2C$ $109.0$ $N2-C7-H7A$ $126.6$ $C2-C1-H1A$ $109.5$ $C7-C6-H6A$ $126.6$ $C2-C1-H1B$ $109.5$ $N1-C6-H6A$ $126.6$ $H1A-C1-H1B$ $109.5$ $N1-C6-H6A$ $126.6$ $H1A-C1-H1C$ $109.5$ $C8-C5-C10$ $111.6 (2)$ $C2-C1-H1C$ $109.5$ $C10-C5-H5A$ $109.3$ $H1A-C1-H1C$ $109.5$ $C8-C5-H5B$ $109.3$ $H1B-C1-H1C$ $109.5$	C8 - 02 - C4	116.1 (2)	C4 - C3 - H3A	108.4	
N2-C9-C9i124.5 (2)C4-C3-H3B108.4N1-C9-C9i123.9 (2)H3A-C3-H3B107.5O1-C8-O2122.7 (3)C3-C2-C1112.7 (4)O1-C8-C5124.7 (3)C3-C2-H2B109.0O2-C8-C5112.6 (2)C1-C2-H2B109.0C6-C7-N2110.9 (2)C3-C2-H2C109.0C6-C7-H7A124.5C1-C2-H2C109.0N2-C7-H7A124.5H2B-C2-H2C107.8C7-C6-N1106.7 (2)C2-C1-H1A109.5C7-C6-H6A126.6C2-C1-H1B109.5N1-C6-H6A126.6H1A-C1-H1B109.5N1-C6-H6A126.6H1A-C1-H1C109.5C8-C5-C10111.6 (2)C2-C1-H1C109.5C10-C5-H5A109.3H1B-C1-H1C109.5C8-C5-H5B109.3H1B-C1-H1C109.5	N2-C9-N1	111 59 (19)	$C^2$ — $C^3$ — $H^3B$	108.4	
$N1-C9-C9^i$ $123.9 (2)$ $H3A-C3-H3B$ $107.5$ $O1-C8-O2$ $122.7 (3)$ $C3-C2-C1$ $112.7 (4)$ $O1-C8-C5$ $124.7 (3)$ $C3-C2-H2B$ $109.0$ $O2-C8-C5$ $112.6 (2)$ $C1-C2-H2B$ $109.0$ $C6-C7-N2$ $110.9 (2)$ $C3-C2-H2C$ $109.0$ $C6-C7-H7A$ $124.5$ $C1-C2-H2C$ $109.0$ $N2-C7-H7A$ $124.5$ $C1-C2-H2C$ $109.0$ $N2-C7-H7A$ $124.5$ $126.6$ $12-C2-H2C$ $107.8$ $C7-C6-H6A$ $126.6$ $C2-C1-H1A$ $109.5$ $N1-C6-H6A$ $126.6$ $C2-C1-H1B$ $109.5$ $N1-C6-H6A$ $126.6$ $H1A-C1-H1B$ $109.5$ $N1-C6-H5A$ $109.3$ $H1A-C1-H1C$ $109.5$ $C8-C5-H5A$ $109.3$ $H1B-C1-H1C$ $109.5$ $C8-C5-H5B$ $109.3$ $H1B-C1-H1C$ $109.5$	$N2-C9-C9^{i}$	124.5 (2)	C4-C3-H3B	108.4	
11205 + 05 $1205 + 05$ $1205 + 05$ $1217 + 05 + 105$ $1017 + 05 + 105$ $01-C8-O2$ $122.7 (3)$ $C3-C2-C1$ $112.7 (4)$ $01-C8-C5$ $124.7 (3)$ $C3-C2-H2B$ $109.0$ $02-C8-C5$ $112.6 (2)$ $C1-C2-H2B$ $109.0$ $C6-C7-N2$ $110.9 (2)$ $C3-C2-H2C$ $109.0$ $C6-C7-H7A$ $124.5$ $C1-C2-H2C$ $109.0$ $N2-C7-H7A$ $124.5$ $H2B-C2-H2C$ $107.8$ $C7-C6-N1$ $106.7 (2)$ $C2-C1-H1A$ $109.5$ $C7-C6-H6A$ $126.6$ $C2-C1-H1B$ $109.5$ $N1-C6-H6A$ $126.6$ $H1A-C1-H1B$ $109.5$ $N1-C6-H6A$ $126.6$ $H1A-C1-H1B$ $109.5$ $C8-C5-C10$ $111.6 (2)$ $C2-C1-H1C$ $109.5$ $C10-C5-H5A$ $109.3$ $H1A-C1-H1C$ $109.5$ $C8-C5-H5B$ $109.3$ $H1B-C1-H1C$ $109.5$	$N1 - C9 - C9^i$	123.9(2)	H3A—C3—H3B	107.5	
O1-C8-C5 $124.7 (3)$ $C3-C2-H2B$ $109.0$ $O2-C8-C5$ $112.6 (2)$ $C1-C2-H2B$ $109.0$ $C6-C7-N2$ $110.9 (2)$ $C3-C2-H2C$ $109.0$ $C6-C7-H7A$ $124.5$ $C1-C2-H2C$ $109.0$ $N2-C7-H7A$ $124.5$ $H2B-C2-H2C$ $107.8$ $C7-C6-N1$ $106.7 (2)$ $C2-C1-H1A$ $109.5$ $C7-C6-H6A$ $126.6$ $C2-C1-H1B$ $109.5$ $N1-C6-H6A$ $126.6$ $C2-C1-H1B$ $109.5$ $C8-C5-C10$ $111.6 (2)$ $C2-C1-H1C$ $109.5$ $C10-C5-H5A$ $109.3$ $H1A-C1-H1C$ $109.5$ $C8-C5-H5B$ $109.3$ $H1B-C1-H1C$ $109.5$	01-C8-02	122.7 (3)	C3 - C2 - C1	112.7 (4)	
O2-C8-C5       112.6 (2)       C1-C2-H2B       109.0         C6-C7-N2       110.9 (2)       C3-C2-H2C       109.0         C6-C7-H7A       124.5       C1-C2-H2C       109.0         N2-C7-H7A       124.5       H2B-C2-H2C       107.8         C7-C6-N1       106.7 (2)       C2-C1-H1A       109.5         C7-C6-H6A       126.6       C2-C1-H1B       109.5         N1-C6-H6A       126.6       H1A-C1-H1B       109.5         C8-C5-C10       111.6 (2)       C2-C1-H1C       109.5         C8-C5-H5A       109.3       H1A-C1-H1C       109.5         C10-C5-H5A       109.3       H1B-C1-H1C       109.5	01 - C8 - C5	124.7(3)	C3 - C2 - H2B	109.0	
C6 - C7 - N2 $110.9 (2)$ $C3 - C2 - H2C$ $109.0$ $C6 - C7 - H7A$ $124.5$ $C1 - C2 - H2C$ $109.0$ $N2 - C7 - H7A$ $124.5$ $H2B - C2 - H2C$ $107.8$ $C7 - C6 - N1$ $106.7 (2)$ $C2 - C1 - H1A$ $109.5$ $C7 - C6 - H6A$ $126.6$ $C2 - C1 - H1B$ $109.5$ $N1 - C6 - H6A$ $126.6$ $H1A - C1 - H1B$ $109.5$ $C8 - C5 - C10$ $111.6 (2)$ $C2 - C1 - H1C$ $109.5$ $C8 - C5 - H5A$ $109.3$ $H1A - C1 - H1C$ $109.5$ $C10 - C5 - H5A$ $109.3$ $H1B - C1 - H1C$ $109.5$ $C8 - C5 - H5B$ $109.3$ $H1B - C1 - H1C$ $109.5$	$0^{2}-C^{8}-C^{5}$	12.6(2)	C1 - C2 - H2B	109.0	
C6       C7       H7A       124.5       C1       C2       H2C       109.0         N2       C7       H7A       124.5       H2B       C2       H2C       107.8         C7       C6       H1       106.7 (2)       C2       C1       H1B       109.5         C7       C6       H6A       126.6       C2       C1       H1B       109.5         N1       C6       H6A       126.6       H1A       C1       H1B       109.5         N1       C6       H1A       C1       H1B       109.5       C3       C4       C4 <t< td=""><td>C6-C7-N2</td><td>110.9 (2)</td><td>C3 - C2 - H2C</td><td>109.0</td><td></td></t<>	C6-C7-N2	110.9 (2)	C3 - C2 - H2C	109.0	
N2—C7—H7A       124.5       H2B—C2—H2C       107.8         C7—C6—N1       106.7 (2)       C2—C1—H1A       109.5         C7—C6—H6A       126.6       C2—C1—H1B       109.5         N1—C6—H6A       126.6       H1A—C1—H1B       109.5         C8—C5—C10       111.6 (2)       C2—C1—H1C       109.5         C10—C5—H5A       109.3       H1A—C1—H1C       109.5         C8—C5—H5B       109.3       H1B—C1—H1C       109.5	C6—C7—H7A	124.5	C1 - C2 - H2C	109.0	
C7—C6—N1       106.7 (2)       C2—C1—H1A       109.5         C7—C6—H6A       126.6       C2—C1—H1B       109.5         N1—C6—H6A       126.6       H1A—C1—H1B       109.5         C8—C5—C10       111.6 (2)       C2—C1—H1C       109.5         C8—C5—H5A       109.3       H1A—C1—H1C       109.5         C10—C5—H5A       109.3       H1B—C1—H1C       109.5         C8—C5—H5B       109.3       C10—C1—H1C       C109.5	N2—C7—H7A	124.5	$H_2B$ — $C_2$ — $H_2C$	107.8	
C7—C6—H6A       126.6       C2—C1—H1B       109.5         N1—C6—H6A       126.6       H1A—C1—H1B       109.5         C8—C5—C10       111.6 (2)       C2—C1—H1C       109.5         C8—C5—H5A       109.3       H1A—C1—H1C       109.5         C10—C5—H5A       109.3       H1B—C1—H1C       109.5         C8—C5—H5B       109.3       C10—C1—H1C       109.5	C7-C6-N1	106.7 (2)	C2-C1-H1A	109.5	
N1—C6—H6A       126.6       H1A—C1—H1B       109.5         C8—C5—C10       111.6 (2)       C2—C1—H1C       109.5         C8—C5—H5A       109.3       H1A—C1—H1C       109.5         C10—C5—H5A       109.3       H1B—C1—H1C       109.5         C8—C5—H5B       109.3       C10—C1—H1C       109.5	C7—C6—H6A	126.6	C2 - C1 - H1B	109.5	
C8—C5—C10       111.6 (2)       C2—C1—H1C       109.5         C8—C5—H5A       109.3       H1A—C1—H1C       109.5         C10—C5—H5A       109.3       H1B—C1—H1C       109.5         C8—C5—H5B       109.3       H1B—C1—H1C       109.5	N1—C6—H6A	126.6	H1A—C1—H1B	109.5	
C8—C5—H5A     109.3     H1A—C1—H1C     109.5       C10—C5—H5A     109.3     H1B—C1—H1C     109.5       C8—C5—H5B     109.3     H1B—C1—H1C     109.5	C8—C5—C10	111.6 (2)	C2—C1—H1C	109.5	
C10—C5—H5A 109.3 H1B—C1—H1C 109.5 C8—C5—H5B 109.3	C8—C5—H5A	109.3	H1A—C1—H1C	109.5	
C8—C5—H5B 109.3	C10—C5—H5A	109.3	H1B—C1—H1C	109.5	
	C8—C5—H5B	109.3			

Symmetry code: (i) -x+1, -y+1, -z+1.

# Hydrogen-bond geometry (Å, °)

D—H···A	<i>D</i> —Н	H···A	D····A	D—H…A
C10—H10 <i>B</i> ····N2 <sup>i</sup>	0.97	2.46	2.960 (3)	111

Symmetry code: (i) -x+1, -y+1, -z+1.