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4-(Diphenylamino)benzaldehvde

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Key indicators: single-crystal X-ray study; T = 292 K; mean σ (C–C) = 0.004 Å; R factor = 0.056; wR factor = 0.153; data-to-parameter ratio = 15.2.

In the title compound, C₁₉H₁₅NO, the N atom adopts an approximately trigonal-planar geometry, lying 0.07 (1) Å from the plane defined by its three neighbouring C atoms. The two phenyl rings and the benzaldehyde group form dihedral angles of 53.0 (1)/47.2 (1) and 29.0 (1) $^{\circ}$, respectively, with this central plane.

Related literature

For details of the synthesis, see: Wang & Zhou (2000). For arylamines, see: Beller (1995); Wang et al. (2005); Yao et al. (2006).



Experimental

Crystal data

| $(7) Å^3$ |
|-----------|
| ., = |
| <i>.</i> |
| ion |
| 1 |
| |
| 0.04 mm |
| |
| i |

Data collection

Bruker SMART CCD area-detector diffractometer Absorption correction: multi-scan (SADABS; Bruker, 2000) $T_{\min} = 0.971, T_{\max} = 0.997$

Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.056$ $wR(F^2) = 0.153$ S = 0.912898 reflections

12673 measured reflections 2898 independent reflections 1393 reflections with $I > 2\sigma(I)$ $R_{\rm int} = 0.087$

191 parameters H-atom parameters constrained $\Delta \rho_{\rm max} = 0.14 \text{ e} \text{ Å}^{-3}$ $\Delta \rho_{\rm min} = -0.14 \text{ e} \text{ Å}^{-3}$

Data collection: SMART (Bruker, 2000); cell refinement: SAINT (Bruker, 2000); data reduction: SAINT; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: SHELXTL (Sheldrick, 2008); software used to prepare material for publication: SHELXTL.

Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: BI2326).

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supporting information

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4-(Diphenylamino)benzaldehyde

Hongli Wang, Wenyuan Xu, Bin Zhang, Wenjing Xiao and Hong Wu

S1. Comment

Arylamine derivatives are common intermediates in the synthesis of many compounds and polymers (Yao *et al.*, 2006; Beller, 1995). We became interested in using the Vilsmeier reaction to obtain the title compound, which is a good intermediate for several compounds (Wang *et al.*, 2005). In the crystal structure (Fig. 1), the bond lengths and angles are within normal ranges.

S2. Experimental

The title compound was synthesised according to the published procedure (Wang & Zhou, 2000) and recrystallized from chloroform.

S3. Refinement

All H atoms were placed in geometrically idealized positions with C—H = 0.93 Å and refined using a riding model, with $U_{iso}(H) = 1.2U_{eq}(C)$.



Figure 1

Molecular structure of the title compound showing displacement ellipsoids at 50% probability for non-H atoms.

4-(Diphenylamino)benzaldehyde

| Crystal data | |
|--|--|
| C ₁₉ H ₁₅ NO | F(000) = 576 |
| $M_r = 273.32$ | $D_{\rm x} = 1.223 {\rm Mg} {\rm m}^{-3}$ |
| Monoclinic, $P2_1/c$ | Mo <i>K</i> α radiation, $\lambda = 0.71073$ Å |
| Hall symbol: -P 2ybc | Cell parameters from 843 reflections |
| a = 12.1188 (8) Å | $\theta = 2.6 - 18.1^{\circ}$ |
| b = 11.4342 (8) Å | $\mu=0.08~\mathrm{mm^{-1}}$ |
| c = 10.9560 (7) Å | T = 292 K |
| $\beta = 102.082 \ (2)^{\circ}$ | Needle, colorless |
| $V = 1484.53 (17) Å^3$ | $0.40 \times 0.10 \times 0.04 \text{ mm}$ |
| Z = 4 | |
| Data collection | |
| Bruker SMART CCD area-detector | 12673 measured reflections |
| diffractometer | 2898 independent reflections |
| Radiation source: fine-focus sealed tube | 1393 reflections with $I > 2\sigma(I)$ |
| Graphite monochromator | $R_{\rm int} = 0.087$ |
| φ and ω scans | $\theta_{\rm max} = 26.0^{\circ}, \theta_{\rm min} = 1.7^{\circ}$ |
| Absorption correction: multi-scan | $h = -14 \rightarrow 14$ |
| (SADABS; Bruker, 2000) | $k = -14 \rightarrow 14$ |
| $T_{\min} = 0.971, \ T_{\max} = 0.997$ | $l = -13 \rightarrow 13$ |
| | |

Refinement

| Refinement on F^2 | Hydrogen site location: inferred from |
|--|---|
| Least-squares matrix: full | neighbouring sites |
| $R[F^2 > 2\sigma(F^2)] = 0.056$ | H-atom parameters constrained |
| $wR(F^2) = 0.153$ | $w = 1/[\sigma^2(F_o^2) + (0.0688P)^2]$ |
| S = 0.91 | where $P = (F_o^2 + 2F_c^2)/3$ |
| 2898 reflections | $(\Delta/\sigma)_{\rm max} < 0.001$ |
| 191 parameters | $\Delta \rho_{\rm max} = 0.14 \text{ e} \text{ Å}^{-3}$ |
| 0 restraints | $\Delta \rho_{\rm min} = -0.14 \text{ e} \text{ Å}^{-3}$ |
| Primary atom site location: structure-invariant direct methods | Extinction correction: <i>SHELXL97</i> (Sheldrick, 2008), $Fc^*=kFc[1+0.001xFc^2\lambda^3/sin(2\theta)]^{-1/4}$ |
| Secondary atom site location: difference Fourier map | Extinction coefficient: 0.007 (2) |

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (\hat{A}^2)

| | | | | TT + /TT | |
|-----|------------|--------------|-------------|----------------------------|--|
| | X | <i>y</i> | Ζ | $U_{\rm iso}^*/U_{\rm eq}$ | |
| C1 | 0.7834 (2) | 0.14287 (18) | 0.0025 (2) | 0.0483 (7) | |
| C2 | 0.6819 (2) | 0.09360 (19) | 0.0112 (3) | 0.0587 (8) | |
| H2 | 0.6307 | 0.1360 | 0.0460 | 0.070* | |
| C3 | 0.6555 (2) | -0.0192 (2) | -0.0318 (3) | 0.0624 (8) | |
| H3 | 0.5864 | -0.0520 | -0.0266 | 0.075* | |
| C4 | 0.7312 (3) | -0.0821 (2) | -0.0817 (3) | 0.0637 (8) | |
| H4 | 0.7136 | -0.1578 | -0.1102 | 0.076* | |
| C5 | 0.8329 (3) | -0.0340 (2) | -0.0896 (3) | 0.0659 (8) | |
| H5 | 0.8841 | -0.0771 | -0.1238 | 0.079* | |
| C6 | 0.8601 (2) | 0.0793 (2) | -0.0468(2) | 0.0574 (7) | |
| H6 | 0.9295 | 0.1116 | -0.0514 | 0.069* | |
| C7 | 0.9178 (2) | 0.27936 (18) | 0.1276 (2) | 0.0492 (7) | |
| C8 | 0.9540 (2) | 0.2101 (2) | 0.2309 (3) | 0.0645 (8) | |
| H8 | 0.9076 | 0.1514 | 0.2505 | 0.077* | |
| C9 | 1.0605 (3) | 0.2283 (3) | 0.3059 (3) | 0.0787 (9) | |
| H9 | 1.0850 | 0.1817 | 0.3759 | 0.094* | |
| C10 | 1.1294 (3) | 0.3147 (3) | 0.2769 (3) | 0.0790 (10) | |
| H10 | 1.2007 | 0.3263 | 0.3267 | 0.095* | |
| C11 | 1.0929 (3) | 0.3832 (2) | 0.1750 (3) | 0.0811 (10) | |
| H11 | 1.1392 | 0.4421 | 0.1555 | 0.097* | |
| C12 | 0.9878 (2) | 0.3656 (2) | 0.1008 (3) | 0.0639 (8) | |
| H12 | 0.9638 | 0.4128 | 0.0312 | 0.077* | |
| C13 | 0.7402 (2) | 0.35282 (17) | -0.0019 (2) | 0.0475 (6) | |

| 0.6713 (2) | 0.34636 (19) | -0.1196 (3) | 0.0593 (7) |
|--------------|--|--|--|
| 0.6724 | 0.2797 | -0.1679 | 0.071* |
| 0.6009 (2) | 0.43842 (19) | -0.1657 (3) | 0.0612 (8) |
| 0.5539 | 0.4320 | -0.2442 | 0.073* |
| 0.5989 (2) | 0.53936 (19) | -0.0979 (3) | 0.0556 (7) |
| 0.6677 (2) | 0.5467 (2) | 0.0200 (3) | 0.0605 (8) |
| 0.6668 | 0.6142 | 0.0673 | 0.073* |
| 0.7375 (2) | 0.45501 (19) | 0.0682 (3) | 0.0577 (7) |
| 0.7830 | 0.4610 | 0.1476 | 0.069* |
| 0.5231 (2) | 0.6343 (2) | -0.1488 (3) | 0.0772 (9) |
| 0.4757 | 0.6210 | -0.2260 | 0.093* |
| 0.81100 (18) | 0.25939 (15) | 0.0479 (2) | 0.0567 (6) |
| 0.51528 (17) | 0.72793 (15) | -0.1018 (2) | 0.0929 (8) |
| | 0.6713 (2) 0.6724 0.6009 (2) 0.5539 0.5989 (2) 0.6677 (2) 0.6668 0.7375 (2) 0.7830 0.5231 (2) 0.4757 0.81100 (18) 0.51528 (17) | 0.0713 (2)0.34030 (19)0.67240.27970.6009 (2)0.43842 (19)0.55390.43200.5989 (2)0.53936 (19)0.6677 (2)0.5467 (2)0.66680.61420.7375 (2)0.45501 (19)0.78300.46100.5231 (2)0.6343 (2)0.47570.62100.81100 (18)0.25939 (15)0.51528 (17)0.72793 (15) | 0.0713(2) $0.34030(19)$ $-0.1190(3)$ 0.6724 0.2797 -0.1679 $0.6009(2)$ $0.43842(19)$ $-0.1657(3)$ 0.5539 0.4320 -0.2442 $0.5989(2)$ $0.53936(19)$ $-0.0979(3)$ $0.6677(2)$ $0.5467(2)$ $0.0200(3)$ 0.6668 0.6142 0.0673 $0.7375(2)$ $0.45501(19)$ $0.0682(3)$ 0.7830 0.4610 0.1476 $0.5231(2)$ $0.6343(2)$ $-0.1488(3)$ 0.4757 0.6210 -0.2260 $0.81100(18)$ $0.25939(15)$ $0.0479(2)$ $0.51528(17)$ $0.72793(15)$ $-0.1018(2)$ |

Atomic displacement parameters (\mathring{A}^2)

| | U^{11} | U^{22} | U^{33} | U^{12} | U^{13} | U^{23} |
|-----|-------------|-------------|-------------|--------------|--------------|--------------|
| C1 | 0.0461 (16) | 0.0370 (12) | 0.0592 (17) | 0.0004 (11) | 0.0050 (14) | 0.0024 (11) |
| C2 | 0.0541 (17) | 0.0434 (14) | 0.078 (2) | 0.0030 (12) | 0.0132 (15) | -0.0002 (13) |
| C3 | 0.0542 (18) | 0.0487 (15) | 0.080(2) | -0.0060 (13) | 0.0049 (17) | 0.0013 (13) |
| C4 | 0.070 (2) | 0.0444 (14) | 0.069 (2) | 0.0000 (15) | -0.0034 (17) | -0.0046 (13) |
| C5 | 0.077 (2) | 0.0587 (17) | 0.0599 (19) | 0.0171 (15) | 0.0085 (17) | -0.0094 (13) |
| C6 | 0.0515 (17) | 0.0579 (15) | 0.0632 (19) | -0.0006 (13) | 0.0126 (15) | 0.0002 (13) |
| C7 | 0.0497 (17) | 0.0421 (13) | 0.0533 (17) | -0.0006 (12) | 0.0052 (14) | -0.0027 (12) |
| C8 | 0.063 (2) | 0.0678 (17) | 0.063 (2) | 0.0082 (14) | 0.0146 (17) | 0.0088 (15) |
| C9 | 0.077 (3) | 0.102 (2) | 0.054 (2) | 0.030 (2) | 0.0059 (19) | -0.0009 (17) |
| C10 | 0.059 (2) | 0.091 (2) | 0.080 (3) | 0.0012 (19) | -0.001 (2) | -0.035 (2) |
| C11 | 0.068 (2) | 0.0638 (18) | 0.105 (3) | -0.0069 (16) | 0.004 (2) | -0.0098 (19) |
| C12 | 0.0566 (19) | 0.0577 (15) | 0.073 (2) | -0.0066 (14) | 0.0024 (16) | 0.0013 (14) |
| C13 | 0.0466 (16) | 0.0380 (12) | 0.0558 (17) | -0.0024 (11) | 0.0063 (14) | -0.0006 (11) |
| C14 | 0.0660 (19) | 0.0441 (14) | 0.0625 (19) | 0.0027 (12) | 0.0010 (16) | -0.0066 (12) |
| C15 | 0.0591 (18) | 0.0515 (15) | 0.0662 (19) | 0.0039 (13) | -0.0025 (15) | 0.0006 (13) |
| C16 | 0.0484 (17) | 0.0430 (14) | 0.073 (2) | 0.0013 (11) | 0.0066 (16) | 0.0000 (13) |
| C17 | 0.0591 (18) | 0.0417 (14) | 0.081 (2) | -0.0023 (13) | 0.0158 (17) | -0.0126 (13) |
| C18 | 0.0561 (18) | 0.0489 (14) | 0.0638 (19) | 0.0003 (12) | 0.0027 (15) | -0.0047 (13) |
| C19 | 0.077 (2) | 0.0477 (16) | 0.103 (3) | 0.0085 (15) | 0.0115 (19) | 0.0079 (16) |
| N1 | 0.0526 (14) | 0.0375 (10) | 0.0714 (16) | 0.0000 (9) | -0.0067 (12) | 0.0017 (10) |
| O1 | 0.0878 (16) | 0.0471 (11) | 0.143 (2) | 0.0126 (10) | 0.0210 (15) | -0.0011 (11) |
| | | | | | | |

Geometric parameters (Å, °)

| C1—C2 | 1.375 (3) | C10—C11 | 1.359 (4) | |
|-------|-----------|---------|-----------|--|
| C1—C6 | 1.376 (3) | C10—H10 | 0.930 | |
| C1—N1 | 1.437 (3) | C11—C12 | 1.375 (3) | |
| C2—C3 | 1.387 (3) | C11—H11 | 0.930 | |
| С2—Н2 | 0.930 | C12—H12 | 0.930 | |
| C3—C4 | 1.366 (4) | C13—C14 | 1.383 (3) | |
| С3—Н3 | 0.930 | C13—C18 | 1.402 (3) | |
| | | | | |

| C4—C5 | 1.369 (4) | C13—N1 | 1.407 (3) |
|---------------------------------|----------------------|----------------------------|-------------------|
| C4—H4 | 0.930 | C14—C15 | 1.382 (3) |
| C5—C6 | 1.394 (3) | C14—H14 | 0.930 |
| С5—Н5 | 0.930 | C15—C16 | 1.376 (3) |
| С6—Н6 | 0.930 | C15H15 | 0.930 |
| C7 $C12$ | 1 372 (3) | | 1.385(4) |
| C_{1}^{2} | 1.372(3) 1.275(2) | $C_{10} = C_{10}$ | 1.385(4) |
| C7C8 | 1.373(3) | | 1.430(3) |
| | 1.421 (3) | | 1.381 (3) |
| C8-C9 | 1.392 (4) | | 0.930 |
| С8—Н8 | 0.930 | C18—H18 | 0.930 |
| C9—C10 | 1.373 (4) | C19—O1 | 1.200 (3) |
| С9—Н9 | 0.930 | С19—Н19 | 0.930 |
| C2—C1—C6 | 119.9 (2) | C10-C11-C12 | 120.2 (3) |
| C2-C1-N1 | 120.2 (2) | C10-C11-H11 | 119.9 |
| C6-C1-N1 | 119.9 (2) | C12—C11—H11 | 119.9 |
| C1 - C2 - C3 | 120.2(2) | C7-C12-C11 | 121 1 (3) |
| C1 - C2 - H2 | 119.9 | C7-C12-H12 | 119 5 |
| $C_3 - C_2 - H_2$ | 110.0 | C_{11} C_{12} H_{12} | 119.5 |
| C_{1} C_{2} C_{2} | 110.0 (3) | C_{14} C_{12} C_{18} | 119.5 118.4(2) |
| $C_{4} = C_{3} = C_{2}$ | 119.9 (3) | C14 - C13 - C18 | 110.4(2) |
| $C_4 = C_3 = H_3$ | 120.0 | C14 - C13 - N1 | 121.4(2) |
| C2—C3—H3 | 120.0 | C18—C13—N1 | 120.2 (2) |
| C3_C4_C5 | 120.2 (2) | 015-014-013 | 120.4 (2) |
| C3—C4—H4 | 119.9 | C15—C14—H14 | 119.8 |
| C5—C4—H4 | 119.9 | C13—C14—H14 | 119.8 |
| C4—C5—C6 | 120.3 (3) | C16—C15—C14 | 121.4 (3) |
| C4—C5—H5 | 119.9 | C16—C15—H15 | 119.3 |
| С6—С5—Н5 | 119.9 | C14—C15—H15 | 119.3 |
| C1—C6—C5 | 119.5 (2) | C15—C16—C17 | 118.6 (2) |
| С1—С6—Н6 | 120.3 | C15—C16—C19 | 120.0 (3) |
| С5—С6—Н6 | 120.3 | C17—C16—C19 | 121.3 (2) |
| C12—C7—C8 | 119.0 (3) | C18—C17—C16 | 120.7 (2) |
| C12—C7—N1 | 120.6 (2) | С18—С17—Н17 | 119.6 |
| C8—C7—N1 | 120.4 (2) | С16—С17—Н17 | 119.6 |
| C7 - C8 - C9 | 119.8 (3) | C17 - C18 - C13 | 1204(3) |
| C7 - C8 - H8 | 120.1 | C17 - C18 - H18 | 119.8 |
| C_{1} C_{2} C_{3} H_{3} | 120.1 | C_{13} C_{18} H_{18} | 110.8 |
| $C_{2} = C_{3} = C_{10}$ | 120.1 120.2(2) | C_{13} C_{10} C_{16} | 119.0 126.0(2) |
| $C_{10} = C_{2} = C_{3}$ | 120.2 (3) | 01 - 010 - 010 | 120.9 (3) |
| $C_{10} - C_{9} - H_{9}$ | 119.9 | OI = CI = HI9 | 110.5 |
| C8-C9-H9 | 119.9 | C10—C19—H19 | 110.5 |
| | 119.7 (3) | C13— $N1$ — $C7$ | 121.32 (18) |
| C11—C10—H10 | 120.1 | | 119.4 (2) |
| С9—С10—Н10 | 120.1 | C7—N1—C1 | 118.55 (18) |
| C6—C1—C2—C3 | -1.3 (4) | C14—C15—C16—C19 | -179.6 (3) |
| N1—C1—C2—C3 | -179.5 (2) | C15—C16—C17—C18 | 0.5 (4) |
| C1—C2—C3—C4 | 0.7 (4) | C19—C16—C17—C18 | 178.7 (2) |
| C2—C3—C4—C5 | -0.2 (4) | C16—C17—C18—C13 | 0.3 (4) |

| C3—C4—C5—C6 | 0.1 (4) | C14—C13—C18—C17 | -0.2 (4) |
|-----------------|------------|-----------------|------------|
| C2-C1-C6-C5 | 1.2 (4) | N1-C13-C18-C17 | -179.6 (2) |
| N1-C1-C6-C5 | 179.5 (2) | C15—C16—C19—O1 | -177.5 (3) |
| C4—C5—C6—C1 | -0.7 (4) | C17—C16—C19—O1 | 4.4 (5) |
| С12—С7—С8—С9 | -0.1 (4) | C14—C13—N1—C7 | 146.1 (2) |
| N1—C7—C8—C9 | 177.9 (2) | C18—C13—N1—C7 | -34.5 (4) |
| C7—C8—C9—C10 | -0.2 (4) | C14—C13—N1—C1 | -23.9 (4) |
| C8—C9—C10—C11 | 0.5 (4) | C18—C13—N1—C1 | 155.4 (2) |
| C9—C10—C11—C12 | -0.5 (5) | C12—C7—N1—C13 | -42.9 (4) |
| C8—C7—C12—C11 | 0.1 (4) | C8—C7—N1—C13 | 139.1 (2) |
| N1—C7—C12—C11 | -177.9 (2) | C12—C7—N1—C1 | 127.3 (2) |
| C10-C11-C12-C7 | 0.2 (4) | C8—C7—N1—C1 | -50.7 (3) |
| C18—C13—C14—C15 | -0.6 (4) | C2-C1-N1-C13 | -58.8 (3) |
| N1—C13—C14—C15 | 178.8 (2) | C6-C1-N1-C13 | 123.0 (3) |
| C13—C14—C15—C16 | 1.4 (4) | C2-C1-N1-C7 | 130.9 (3) |
| C14—C15—C16—C17 | -1.4 (4) | C6—C1—N1—C7 | -47.4 (3) |
| | | | |