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# 1,1'-Bis(diisobutylphosphino)cobaltocenium hexafluoridophosphate

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Key indicators: single-crystal X-ray study; T = 298 K; mean  $\sigma$ (C–C) = 0.006 Å; R factor = 0.057; wR factor = 0.147; data-to-parameter ratio = 20.2.

In the title compound,  $[Co(C_{13}H_{22}P)_2]PF_6$ , the Co<sup>III</sup> atom is sandwiched between two (diisobutylphosphino)cyclopentadienenyl ligands. The two diisobutylphophine units are *trans* to each other with respect to the Co<sup>III</sup> metal center. The PF<sub>6</sub><sup>-</sup> anion links the cobaltocenium cations *via* weak C-H···F hydrogen bonds into a chain running along the *b* axis. The chains are further linked by C-H···F hydrogen bonds, forming a layer extending parallel to the (101) plane.

#### **Related literature**

For background to cobaltocene derivatives applied as catalysts, see: Mathews *et al.* (2000). For the structures of closely related compounds, see: Brasse *et al.* (2000); Hou *et al.* (2007).



#### **Experimental**

Crystal data  $[Co(C_{13}H_{22}P)_2]$ ·PF<sub>6</sub>  $M_r = 622.45$ Monoclinic,  $P2_1/n$  a = 16.7733 (3) Å b = 10.4660 (2) Å c = 18.5105 (4) Å  $\beta = 108.288$  (1)°

 $V = 3085.38 (10) \text{ Å}^{3}$  Z = 4Mo K\alpha radiation  $\mu = 0.76 \text{ mm}^{-1}$  T = 298 (2) K $0.40 \times 0.04 \times 0.02 \text{ mm}$   $R_{\rm int} = 0.083$ 

33818 measured reflections

6733 independent reflections

3878 reflections with  $I > 2\sigma(I)$ 

#### Data collection

Bruker SMART CCD area-detector diffractometer Absorption correction: multi-scan (SADABS; Sheldrick, 2004)  $T_{min} = 0.750, T_{max} = 0.985$ 

#### Refinement

$R[F^2 > 2\sigma(F^2)] = 0.056$	333 parameters
$wR(F^2) = 0.147$	H-atom parameters constrained
S = 0.97	$\Delta \rho_{\rm max} = 0.47 \text{ e } \text{\AA}^{-3}$
6733 reflections	$\Delta \rho_{\rm min} = -0.34 \text{ e } \text{\AA}^{-3}$

# Table 1

, °)

$D - H \cdots A$	D-H	$H \cdot \cdot \cdot A$	$D \cdots A$	$D - H \cdots A$
$C3-H3\cdots F5^{i}$	0.98	2.44	3.237 (5)	138
C15−H15···F4 <sup>i</sup>	0.98	2.39	3.278 (4)	150
C17−H17···F2	0.98	2.51	3.188 (5)	126
C18−H18···F6	0.98	2.41	3.305 (4)	152
$C19-H19B\cdots F2^{ii}$	0.97	2.54	3.494 (4)	167

Symmetry codes: (i) x, y - 1, z; (ii)  $-x + \frac{3}{2}, y - \frac{1}{2}, -z + \frac{1}{2}$ .

Data collection: *SMART* (Bruker, 2001); cell refinement: *SAINT* (Bruker, 2001); data reduction: *SAINT*; program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXS97* (Sheldrick, 2008); molecular graphics: *SHELXTL* (Sheldrick, 2008); software used to prepare material for publication: *SHELXTL*.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: IS2295).

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# supporting information

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# 1,1'-Bis(diisobutylphosphino)cobaltocenium hexafluoridophosphate

# Jian-Guo Hou, Ding-Biao Li and Man-Zhen Qiu

## S1. Comment

Cobaltocene derivatives have been applied as catalysts in cross-coupling reactions (Mathews *et al.*, 2000). As part of our investigations of new catalysts, we have focused our attention on cobaltocenium compounds. Some complexes, such as 1,1'-bis(diphenylphosphino)cobaltocenium tetrafluoridoborate, have been obtained and reported (Hou *et al.*, 2007). Herein, we report the structure of the title compound, (I) (Fig. 1). The molecular structure of the title complex consists of the  $[(\eta_5-(i-C_4H_9)_2PC_5H_4)_2C_0]^+$  cation and the PF<sub>6</sub><sup>-</sup> anion, which is very similar to the compounds 1,1'-bis(diphenyl-phosphino)cobaltocenium tetrafluoridoborate (Hou *et al.*, 2007) and 1,1'-bis(diphenylphosphino)cobaltocenium hexa-fluorophosphate with different substituents (Brasse *et al.*, 2000). The two (*i*-C<sub>4</sub>H<sub>9</sub>)<sub>2</sub>P substituents are *trans* to each other with respect to the Co<sup>III</sup> metal center, and the two substituted Cp rings staggered and are essentially parallel with a dihedral angle of 1.8 (2)°. The Co1…*Cg*1 and Co1…*Cg*2 distances are 1.6429 (15) and 1.6430 (3) Å, respectively, and the *Cg*1…Co1…*Cg*2 angle is 179.13 (8)° (*Cg*1 and *Cg*2 are the centroids of the two cyclopentadienyl) The hydrogen bonds of C—H…F play a key role of the stabilization of crystal structure of the title compound. As shown in Fig. 2, there are extensive nonclassical hydrogen bonds formed by C—H…F (Table 2). There are not only intramolecular but also intermolecular hydrogen bonds between the cation and anion, thus, two-dimensional layers extending parallel to the (101) plane were formed.

## **S2. Experimental**

The title compound was obtained by anion exchange of 1,1'-bis(di-isobutylphosphino)cobaltocenium chloride with ammonium hexaflurophosphate. Crystals appropriate for data collection were obtained by slow diffusion of hexane into a solution of the title compound in dichloromethane at 293 K.

## **S3. Refinement**

All H atoms were placed in geometrically idealized positions and constrained to ride on their parent atoms with C—H = 0.96-0.98 Å, and with  $U_{iso}(H) = 1.2U_{eq}(C)$  or  $1.5U_{eq}(methyl C)$ .



# Figure 1

The molecular structure of (I), showing ellipsoids at 30% probability level.



## Figure 2

The packing diagram of two-dimensional sheet with hydrogen bonds shown as dashed lines. H atoms not involved in the hydrogen bonds have been omitted for clarity.

#### 1,1'-Bis(diisobutylphosphino)cobaltocenium hexafluorophosphate

Crystal data

[Co(C<sub>13</sub>H<sub>22</sub>P)<sub>2</sub>]·PF<sub>6</sub>  $M_r = 622.45$ Monoclinic,  $P2_1/n$ Hall symbol: -P 2yn a = 16.7733 (3) Å b = 10.4660 (2) Å c = 18.5105 (4) Å  $\beta = 108.288$  (1)° V = 3085.38 (10) Å<sup>3</sup> Z = 4

#### Data collection

Bruker SMART CCD area-detector diffractometer Radiation source: fine-focus sealed tube Graphite monochromator  $\varphi$  and  $\omega$  scans Absorption correction: multi-scan (*SADABS*; Sheldrick, 2004)  $T_{\min} = 0.750, T_{\max} = 0.985$ 

#### Refinement

Refinement on  $F^2$ Least-squares matrix: full  $R[F^2 > 2\sigma(F^2)] = 0.056$  $wR(F^2) = 0.147$ S = 0.976733 reflections F(000) = 1304  $D_x = 1.340 \text{ Mg m}^{-3}$ Mo K $\alpha$  radiation,  $\lambda = 0.71073 \text{ Å}$ Cell parameters from 3150 reflections  $\theta = 2.3-19.9^{\circ}$   $\mu = 0.76 \text{ mm}^{-1}$  T = 298 KNeedle, yellow  $0.40 \times 0.04 \times 0.02 \text{ mm}$ 

33818 measured reflections 6733 independent reflections 3878 reflections with  $I > 2\sigma(I)$  $R_{int} = 0.083$  $\theta_{max} = 27.0^\circ, \theta_{min} = 1.4^\circ$  $h = -21 \rightarrow 21$  $k = -13 \rightarrow 13$  $l = -23 \rightarrow 22$ 

333 parameters0 restraintsPrimary atom site location: structure-invariant direct methodsSecondary atom site location: difference Fourier map

Hydrogen site location: inferred from	$w = 1/[\sigma^2(F_o^2) + (0.0731P)^2]$
neighbouring sites	where $P = (F_o^2 + 2F_c^2)/3$
H-atom parameters constrained	$(\Delta/\sigma)_{\rm max} = 0.001$
	$\Delta  ho_{ m max} = 0.47 \ { m e} \ { m \AA}^{-3}$
	$\Delta \rho_{\rm min} = -0.34 \text{ e } \text{\AA}^{-3}$

#### Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes. **Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	
Col	0.66580(3)	0.34637 (4)	0.07609 (2)	0.04054 (16)	
C1	0.6975 (2)	0.3487 (3)	-0.02171 (18)	0.0413 (8)	
C2	0.6752 (2)	0.2221 (3)	-0.00492 (18)	0.0480 (9)	
H2	0.7119	0.1470	0.0038	0.058*	
C3	0.5916 (2)	0.2239 (4)	-0.0027 (2)	0.0560 (10)	
H3	0.5608	0.1507	0.0081	0.067*	
C4	0.5606 (2)	0.3499 (4)	-0.01797 (19)	0.0542 (10)	
H4	0.5047	0.3794	-0.0193	0.065*	
C5	0.6254 (2)	0.4270 (3)	-0.02941 (18)	0.0468 (9)	
Н5	0.6215	0.5189	-0.0402	0.056*	
C6	0.7928 (2)	0.5658 (3)	-0.0360 (2)	0.0558 (10)	
H6A	0.7526	0.5870	-0.0849	0.067*	
H6B	0.7717	0.5993	0.0033	0.067*	
C7	0.8757 (3)	0.6294 (4)	-0.0295 (3)	0.0740 (13)	
H7	0.8998	0.5880	-0.0655	0.089*	
C8	0.9371 (3)	0.6159 (6)	0.0495 (3)	0.126 (2)	
H8A	0.9162	0.6608	0.0850	0.189*	
H8B	0.9904	0.6511	0.0507	0.189*	
H8C	0.9439	0.5271	0.0630	0.189*	
C9	0.8631 (3)	0.7712 (4)	-0.0501 (3)	0.1105 (19)	
H9A	0.8379	0.8127	-0.0164	0.166*	
H9B	0.8270	0.7798	-0.1016	0.166*	
H9C	0.9164	0.8099	-0.0451	0.166*	
C10	0.7851 (2)	0.3465 (4)	-0.1272 (2)	0.0562 (10)	
H10A	0.7344	0.3882	-0.1586	0.067*	
H10B	0.8316	0.3803	-0.1419	0.067*	
C11	0.7776 (3)	0.2041 (4)	-0.1449 (2)	0.0694 (12)	
H11	0.7300	0.1710	-0.1306	0.083*	
C12	0.7589 (3)	0.1826 (5)	-0.2301 (3)	0.1059 (18)	
H12A	0.8042	0.2160	-0.2458	0.159*	

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(\hat{A}^2)$ 

H12B         0.7077         0.2256         -0.2573         0.159*           H12C         0.7530         0.0928         -0.2409         0.159*           C13         0.8552 (4)         0.1312 (4)         -0.1000 (3)         0.1079 (19)           H13A         0.8506         0.0440         -0.1170         0.162*           H13B         0.803         0.1337         -0.0469         0.162*           H13C         0.9039         0.1695         -0.1077         0.162*           C14         0.6338 (2)         0.3542 (3)         0.17449 (18)         0.0406 (8)           C15         0.7006 (2)         0.2654 (3)         0.18142 (18)         0.0470 (9)           H15         0.6689         0.1739         0.1921         0.056*           C16         0.7687 (2)         0.3305 (4)         0.15524 (19)         0.0574 (10)           H17         0.7821         0.5269         0.1402         0.699*           C17         0.7466 (2)         0.4751 (3)         0.1577 (18)         0.0493 (9)           H18         0.6323         0.5554         0.1492         0.599*           C19         0.5497 (2)         0.3333 (4)         0.2819 (19)         0.0528 (9)           L18					
H12C         0.7530         0.0928         -0.2409         0.159*           C13         0.8552 (4)         0.1312 (4)         -0.1000 (3)         0.1797 (19)           H13A         0.8603         0.1337         -0.0469         0.162*           H13B         0.8603         0.1337         -0.0469         0.162*           H13C         0.9039         0.1695         -0.1077         0.162*           C14         0.6338 (2)         0.3542 (3)         0.17149 (18)         0.0406 (8)           C15         0.7006 (2)         0.2654 (3)         0.18142 (18)         0.0407 (9)           H15         0.689         0.1739         0.1921         0.056* (10)           H16         0.8224         0.2923         0.1706         0.069* (10)           H17         0.7466 (2)         0.4595 (4)         0.15524 (19)         0.0574 (10)           H17         0.7466 (2)         0.3596 (3)         0.28119 (19)         0.528 (9)           C18         0.6640 (2)         0.3570         0.2819 (19)         0.528 (9)           H19A         0.508         0.3508         0.3120         0.663*           C20         0.5497 (3)         0.5532         0.3120         0.663*	H12B	0.7077	0.2256	-0.2573	0.159*
C13         0.8552 (4)         0.1312 (4)         -0.1000 (3)         0.1079 (19)           H13A         0.8506         0.0440         -0.1170         0.162*           H13B         0.8603         0.1337         -0.0469         0.162*           H13C         0.9039         0.1695         -0.1077         0.162*           C14         0.6338 (2)         0.3542 (3)         0.18142 (18)         0.0406 (8)           C15         0.7006 (2)         0.2654 (3)         0.18142 (18)         0.0470 (9)           H15         0.6989         0.1739         0.1921         0.056*           C17         0.7466 (2)         0.4595 (4)         0.15524 (19)         0.0574 (10)           H17         0.7821         0.5269         0.1450         0.069*           C18         0.6640 (2)         0.4751 (3)         0.15777 (18)         0.0493 (9)           H18         0.6323         0.5554         0.1492         0.059*           C19         0.5497 (2)         0.3896 (3)         0.28119 (19)         0.0528 (9)           H19A         0.5086         0.3520         0.3118         0.063*           C19         0.5497 (2)         0.5708         0.2477 (3)         0.114 (2)	H12C	0.7530	0.0928	-0.2409	0.159*
H13A0.85060.0440 $-0.1170$ 0.162*H13B0.86030.1337 $-0.0469$ 0.162*H13C0.90390.1695 $-0.1077$ 0.162*H13C0.69890.17390.19210.0567C140.6338 (2)0.3542 (3)0.17449 (18)0.0406 (8)C150.7006 (2)0.2654 (3)0.18142 (18)0.0470 (9)H150.69890.17390.19210.0576 (10)H160.82240.29230.17060.069*C170.7466 (2)0.4595 (4)0.15524 (19)0.0574 (10)H170.78210.52690.14500.069*C180.6640 (2)0.4751 (3)0.15777 (18)0.0493 (9)H180.63230.55540.14920.059*C190.5497 (2)0.3896 (3)0.28119 (19)0.528 (9)H19A0.50860.35200.30180.063*C200.5469 (3)0.5333 (4)0.2898 (2)0.0699 (12)H200.58770.57080.26800.084*C210.4615 (4)0.5887 (5)0.2477 (3)0.114 (2)H21A0.42080.55780.27020.171*H21B0.44550.56320.19530.171*H22B0.62880.54010.39930.138*H22C0.53480.55730.23730.138*H22C0.53480.53290.39730.138*H22B0.62880.54010.39930.138*H22B0.5477	C13	0.8552 (4)	0.1312 (4)	-0.1000(3)	0.1079 (19)
H13B         0.8603         0.1337         -0.0469         0.162*           H13C         0.9039         0.1695         -0.1077         0.152*           C14         0.6338 (2)         0.3542 (3)         0.17449 (18)         0.0406 (8)           C15         0.7006 (2)         0.2654 (3)         0.18142 (18)         0.0470 (9)           H15         0.6899         0.1739         0.1921         0.056* (10)           H16         0.8224         0.2923         0.1706         0.069*           C17         0.7466 (2)         0.4595 (4)         0.15524 (19)         0.0574 (10)           H17         0.7821         0.5269         0.1450         0.069*           C18         0.6640 (2)         0.4751 (3)         0.15777 (18)         0.0493 (9)           H18         0.6323         0.5554         0.1492         0.059*           C19         0.5497 (2)         0.3896 (3)         0.28119 (19)         0.0528 (9)           H19A         0.5086         0.3520         0.31018         0.063*           C20         0.5469 (3)         0.5333 (4)         0.2898 (2)         0.0699 (12)           H20         0.5877         0.5708         0.2680         0.084*	H13A	0.8506	0.0440	-0.1170	0.162*
H13C         0.9039         0.1695         -0.1077         0.162*           C14         0.6338 (2)         0.3542 (3)         0.17449 (18)         0.0406 (8)           C15         0.7006 (2)         0.2654 (3)         0.18142 (18)         0.0470 (9)           H15         0.6989         0.1739         0.1921         0.056*           C16         0.7687 (2)         0.3305 (4)         0.16930 (19)         0.0576 (10)           H16         0.8224         0.2923         0.1706         0.069*           C17         0.7466 (2)         0.4595 (4)         0.15524 (19)         0.0574 (10)           H17         0.7861 (2)         0.4751 (3)         0.15777 (18)         0.0493 (9)           H18         0.6323         0.5554         0.1492         0.059*           C19         0.5497 (2)         0.3896 (3)         0.28119 (19)         0.528 (9)           H19A         0.5086         0.3520         0.3018         0.663*           H19B         0.6046         0.3598         0.3120         0.063*           C20         0.5497 (1)         0.5708         0.2702         0.171*           L21A         0.4615 (4)         0.5887 (5)         0.2477 (3)         0.114 (2) <tr< td=""><td>H13B</td><td>0.8603</td><td>0.1337</td><td>-0.0469</td><td>0.162*</td></tr<>	H13B	0.8603	0.1337	-0.0469	0.162*
C14 $0.6338$ (2) $0.3542$ (3) $0.1749$ (18) $0.0406$ (8)C15 $0.7006$ (2) $0.2654$ (3) $0.18142$ (18) $0.0470$ (9)H15 $0.6989$ $0.1739$ $0.1921$ $0.056*$ C16 $0.7687$ (2) $0.3305$ (4) $0.16930$ (19) $0.0576$ (10)H16 $0.8224$ $0.2923$ $0.1706$ $0.069*$ C17 $0.7466$ (2) $0.4595$ (4) $0.15524$ (19) $0.0574$ (10)H17 $0.7821$ $0.5269$ $0.1450$ $0.069*$ C18 $0.66440$ (2) $0.4751$ (3) $0.15777$ (18) $0.0493$ (9)H18 $0.6323$ $0.5554$ $0.1492$ $0.0528$ (9)C19 $0.5497$ (2) $0.3896$ (3) $0.28119$ (19) $0.0528$ (9)H19A $0.5086$ $0.3520$ $0.3120$ $0.063*$ C20 $0.5469$ (3) $0.5333$ (4) $0.2898$ (2) $0.0699$ (12)H20 $0.5877$ $0.5708$ $0.2477$ (3) $0.114$ (2)H21A $0.4615$ (4) $0.5875$ $0.2702$ $0.171*$ H21B $0.4455$ $0.5632$ $0.1953$ $0.171*$ H21B $0.4455$ $0.5632$ $0.1953$ $0.171*$ H21B $0.4455$ $0.5632$ $0.1933$ $0.138*$ H22C $0.5738$ $0.5705$ (5) $0.3741$ (2) $0.0917$ (15)H22A $0.5717$ $0.6618$ $0.3786$ $0.138*$ H22B $0.6288$ $0.5401$ $0.3993$ $0.138*$ C23 $0.5366$ (2) $0.1557$ (3) $0.2033$ (2) $0.0605$ (1	H13C	0.9039	0.1695	-0.1077	0.162*
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C14	0.6338 (2)	0.3542 (3)	0.17449 (18)	0.0406 (8)
115 $0.6980$ $0.1739$ $0.1921$ $0.056^*$ C16 $0.7687(2)$ $0.3305(4)$ $0.16930(19)$ $0.0576(10)$ H16 $0.8224$ $0.2923$ $0.1706$ $0.069^*$ C17 $0.7466(2)$ $0.4595(4)$ $0.15524(19)$ $0.0574(10)$ H17 $0.786(2)$ $0.4595(4)$ $0.15524(19)$ $0.0574(10)$ H17 $0.786(2)$ $0.4459(4)$ $0.1450$ $0.069^*$ C18 $0.6640(2)$ $0.4751(3)$ $0.15777(18)$ $0.0493(9)$ H18 $0.6323$ $0.5554$ $0.1492$ $0.0528(9)$ H19A $0.5086$ $0.3520$ $0.3018$ $0.063^*$ H19B $0.6046$ $0.3598$ $0.3120$ $0.063^*$ L20 $0.5469(3)$ $0.5333(4)$ $0.2898(2)$ $0.0699(12)$ H20 $0.5877$ $0.5708$ $0.2680$ $0.884^*$ C21 $0.4615(4)$ $0.5887(5)$ $0.2477(3)$ $0.114(2)$ H21A $0.4208$ $0.5578$ $0.2702$ $0.171^*$ H21B $0.4455$ $0.5632$ $0.1953$ $0.171^*$ H22A $0.5717$ $0.6618$ $0.3786$ $0.138^*$ H22A $0.5717$ $0.6618$ $0.3786$ $0.138^*$ H22B $0.6288$ $0.5401$ $0.3993$ $0.138^*$ H22A $0.5407$ $0.1405$ $0.2154(3)$ $0.0708(12)$ H23B $0.5842$ $0.1405$ $0.2154(3)$ $0.0708(12)$ H23B $0.5842$ $0.1405$ $0.2154(3)$ $0.0708(12)$ H22A $0.4577$ <t< td=""><td>C15</td><td>0.7006 (2)</td><td>0.2654 (3)</td><td>0.18142 (18)</td><td>0.0470 (9)</td></t<>	C15	0.7006 (2)	0.2654 (3)	0.18142 (18)	0.0470 (9)
C160.7687 (2)0.3305 (4)0.16330 (19)0.0376 (10)H160.82240.29230.17060.069*C170.7466 (2)0.4595 (4)0.15524 (19)0.0574 (10)H170.78210.52690.14500.069*C180.6644 (2)0.4751 (3)0.15777 (18)0.0493 (9)H180.63230.55540.14920.059*C190.5497 (2)0.3896 (3)0.28119 (19)0.0628 (9)H19A0.50860.35200.30180.063*C200.5469 (3)0.5333 (4)0.2898 (2)0.0699 (12)H200.58770.57080.26800.084*C210.4615 (4)0.5887 (5)0.2477 (3)0.114 (2)H21A0.42050.55780.27020.171*H21B0.44550.56320.19530.171*H21B0.44550.56320.19530.171*H21C0.46400.68030.25100.171*H21B0.62880.54010.39930.138*H22B0.62880.54010.39930.138*H22B0.62880.54010.39930.138*H22C0.53480.53290.39730.138*H22B0.58420.14050.24840.073*C240.4590 (3)0.0970 (4)0.2154 (3)0.0708 (12)H23A0.58420.14050.24840.073*C250.3322 (3)0.1080 (5)0.1483 (3)0.115 (2)H25A0.39	H15	0.6989	0.1739	0.1921	0.056*
H160.29230.17060.069*C170.7466 (2)0.4595 (4)0.15524 (19)0.0574 (10)H170.78210.52690.14500.069*C180.6640 (2)0.4751 (3)0.15777 (18)0.0493 (9)H180.63230.55540.14920.059*C190.5497 (2)0.3896 (3)0.28119 (19)0.0528 (9)H19A0.50860.35200.30180.063*C200.5469 (3)0.5333 (4)0.2898 (2)0.0699 (12)H200.58770.57080.26800.084*C210.4615 (4)0.5887 (5)0.2477 (3)0.114 (2)H21A0.42080.55780.27020.171*H21B0.44550.56320.19530.171*H21B0.44550.56320.19530.171*H21C0.46400.68030.25100.171*H21C0.46400.68030.25100.138*H22B0.62880.54010.39930.138*H22C0.53480.53290.39730.138*H22C0.53480.53290.39730.138*H22B0.62880.40100.2154 (3)0.073*C240.4590 (3)0.0970 (4)0.2154 (3)0.073*C250.3822 (3)0.1080 (5)0.1483 (3)0.115 (2)H25B0.37110.19640.13520.172*H25B0.37110.19640.13520.172*H25B0.37110.19640.2538 </td <td>C16</td> <td>0.7687(2)</td> <td>0.3305 (4)</td> <td>0.16930 (19)</td> <td>0.0576 (10)</td>	C16	0.7687(2)	0.3305 (4)	0.16930 (19)	0.0576 (10)
1111111111111111 $(177)$ $(1746(2)$ $(0.4595(4)$ $(0.15524(19)$ $(0.574(10)$ $(117)$ $(0.7821)$ $(0.5269)$ $(0.1450)$ $(0.69*)$ $(118)$ $(0.640(2)$ $(0.4751(3))$ $(0.15777(18))$ $(0.0493(9))$ $(118)$ $(0.6323)$ $(0.5554)$ $(0.1492)$ $(0.59*)$ $(119)$ $(0.5497(2))$ $(0.3896(3))$ $(0.28119(19))$ $(0.528(9))$ $(119)$ $(0.5469(3))$ $(0.3598)$ $(0.3110)$ $(0.63*)$ $(120)$ $(0.5877)$ $(0.5788)$ $(0.2680)$ $(0.068*)$ $(220)$ $(0.5469(3))$ $(0.5333(4))$ $(0.2477(3))$ $(0.114(2))$ $(120)$ $(0.5877)$ $(0.578)$ $(0.2477(3))$ $(0.114(2))$ $(121)$ $(0.4455)$ $(0.5632)$ $(0.953)$ $(0.171*)$ $(121)$ $(0.4455)$ $(0.5632)$ $(0.953)$ $(0.171*)$ $(122)$ $(0.5730(3))$ $(0.5705(5))$ $(0.3741(2))$ $(0.917(15))$ $(122)$ $(0.5730(3))$ $(0.5705(5))$ $(0.3741(2))$ $(0.917(15))$ $(122)$ $(0.5348)$ $(0.5329)$ $(0.3773)$ $(0.138*)$ $(122)$ $(0.5348)$ $(0.5329)$ $(0.3773)$ $(0.138*)$ $(122)$ $(0.5348)$ $(0.557(3))$ $(0.2033(2))$ $(0.605(10))$ $(122)$ $(0.5348)$ $(0.557(3))$ $(0.233(2))$ $(0.605(10))$ $(122)$ $(0.5348)$ $(0.557(3))$ $(0.233(2))$ $(0.605(10))$ $(122)$ $(0.5346(2))$ $(0.1557(3))$ <t< td=""><td>H16</td><td>0.8224</td><td>0.2923</td><td>0.1706</td><td>0.069*</td></t<>	H16	0.8224	0.2923	0.1706	0.069*
C10.185 (C)0.115 (C)0.115 (C)0.0169H170.78210.52690.14500.069*C180.6640 (2)0.4751 (3)0.15777 (18)0.0493 (9)H180.63230.55540.14920.059*C190.5497 (2)0.3896 (3)0.28119 (19)0.0528 (9)H19A0.50860.35200.30180.063*H19B0.60460.35980.31200.063*C200.5469 (3)0.5333 (4)0.2898 (2)0.0699 (12)H200.58770.57080.26800.084*C210.4615 (4)0.5887 (5)0.2477 (3)0.114 (2)H21A0.42080.55780.27020.171*H21B0.44550.56320.19530.171*H21B0.44550.56320.19530.171*H21C0.46400.68030.25100.171*H22A0.57170.66180.37860.138*H22B0.62880.54010.39930.138*H22C0.53480.53290.39730.138*C230.5366 (2)0.1557 (3)0.2033 (2)0.0605 (10)H23A0.54770.11200.16120.073*H23B0.58420.14050.24840.073*C240.4590 (3)0.97140.2154 (3)0.115 (2)H25A0.39070.6320.16000.172*H25B0.37110.19640.13520.169*H26C0.4846-0.09100.190<	C17	0.7466(2)	0 4595 (4)	0 15524 (19)	0.0574 (10)
1110.1610.1510.1510.161C180.6640 (2)0.4751 (3)0.15777 (18)0.0493 (9)H180.63230.55540.14920.059*C190.5497 (2)0.3896 (3)0.28119 (19)0.0528 (9)H19A0.50860.35200.30180.063*C200.5469 (3)0.5333 (4)0.2898 (2)0.063*C210.4615 (4)0.5887 (5)0.2477 (3)0.114 (2)H21A0.42080.55780.27020.171*H21B0.44550.56320.19530.171*H21B0.44550.56320.19530.171*H21C0.46400.68030.25100.171*C220.5730 (3)0.5705 (5)0.3741 (2)0.0917 (15)H22A0.57170.66180.37860.138*H22B0.62880.54010.39930.138*H22B0.62880.54010.39930.138*H22B0.53440.53290.39730.138*H22B0.58420.14050.24840.073*C240.4590 (3)0.0970 (4)0.2154 (3)0.0708 (12)H23A0.54770.11200.16120.073*C250.3822 (3)0.1080 (5)0.1483 (3)0.115 (2)H25B0.37110.19640.13520.172*H25B0.37110.19640.25380.169*H25C0.33540.07140.16020.172*H25B0.37500.7355 (2)<	H17	0.7821	0.5269	0.1450	0.069*
C10         C101         C111         C101         C114         C101         C111         C111 <thc111< th="">         C111         C111         C</thc111<>	C18	0.6640(2)	0.320)	0.15777 (18)	0.009
Info $0.0525$ $0.0537$ $0.1712$ $0.0528$ $0.0528$ $0.0528$ $0.0528$ $0.0528$ $0.0528$ $0.063*$ H19A $0.5086$ $0.3520$ $0.3018$ $0.063^*$ $0.063^*$ H19B $0.6046$ $0.3598$ $0.3120$ $0.063^*$ C20 $0.5469$ $0.5377$ $0.5708$ $0.2680$ $0.084^*$ C21 $0.4615$ $(4)$ $0.5887$ $5.22887$ $0.2477$ $0.114$ H21A $0.4208$ $0.5578$ $0.2702$ $0.171^*$ H21B $0.4455$ $0.5632$ $0.1953$ $0.171^*$ H21C $0.4640$ $0.6803$ $0.2510$ $0.171^*$ H21C $0.4640$ $0.6803$ $0.2510$ $0.171^*$ H22A $0.5717$ $0.6618$ $0.3786$ $0.138^*$ H22B $0.6288$ $0.5401$ $0.3993$ $0.138^*$ H22B $0.6288$ $0.5401$ $0.3993$ $0.138^*$ H22C $0.5348$ $0.5329$ $0.3973$ $0.138^*$ H23B $0.5842$ $0.1405$ $0.2484$ $0.073^*$ H23B $0.5842$ $0.1405$ $0.2484$ $0.073^*$ H23B $0.5842$ $0.1405$ $0.2484$ $0.073^*$ H23B $0.3907$ $0.0632$ $0.1660$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^*$ H25B $0.3254$ $0.0714$ $0.1602$ $0.172^*$ H25B $0.5269$ $-0.0464$ <	H18	0.6323	0 5554	0.1492	0.059*
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C19	0.0323 0.5497 (2)	0.3896 (3)	0.28119 (19)	0.059
IIIIII0.50500.51200.50150.005H19B0.60460.35980.31200.063*C200.5469 (3)0.5333 (4)0.2898 (2)0.0699 (12)H200.58770.57080.2477 (3)0.114 (2)H21A0.4080.55780.27020.171*H21B0.44550.56320.19530.171*H21C0.46400.68030.25100.171*C220.5730 (3)0.5705 (5)0.3741 (2)0.0917 (15)H22A0.57170.66180.39930.138*H22B0.62880.54010.39930.138*H22C0.53480.53290.39730.138*C230.5366 (2)0.1557 (3)0.2033 (2)0.0605 (10)H23A0.54770.11200.16120.073*H23B0.58420.14050.24840.073*C240.4590 (3)0.0970 (4)0.2154 (3)0.0708 (12)H240.44820.14310.25750.085*C250.3822 (3)0.1080 (5)0.1483 (3)0.115 (2)H25A0.39070.06320.10600.172*H25B0.37110.19640.13520.172*H25C0.33540.07140.16020.172*H25B0.5269-0.04640.28320.169*H26A0.4304-0.07610.25380.169*H26B0.5269-0.04640.28320.169*F10.63466 (15)0.7385 (2)0.0350	H19A	0.5086	0.3520	0.20119 (19)	0.0528 (5)
1115 $0.5049$ $0.5333$ $0.5126$ $0.6059$ C20 $0.5469$ $0.5577$ $0.5708$ $0.2680$ $0.0699$ H20 $0.5877$ $0.5708$ $0.2680$ $0.084*$ C21 $0.4615$ $(4)$ $0.5887$ $0.2702$ $0.171*$ H21A $0.4208$ $0.5578$ $0.2702$ $0.171*$ H21B $0.4455$ $0.5632$ $0.1953$ $0.171*$ H21C $0.4640$ $0.6803$ $0.2510$ $0.171*$ C22 $0.5730$ $0.5705$ $0.3741$ $(2)$ $0.0917$ H22A $0.5717$ $0.6618$ $0.3786$ $0.138*$ H22B $0.6288$ $0.5401$ $0.3993$ $0.138*$ H22C $0.5348$ $0.5329$ $0.3973$ $0.138*$ C23 $0.5366$ $0.1557$ $0.2033$ $0.0073*$ H23B $0.5422$ $0.1405$ $0.2484$ $0.073*$ H23B $0.5842$ $0.1431$ $0.2575$ $0.088*$ C24 $0.4590$ $0.0970$ $0.2154$ $(3)$ $0.0708$ H24 $0.4482$ $0.1431$ $0.2575$ $0.088*$ C25 $0.3822$ $0.1080$ $0.1483$ $0.1172*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172*$ H25B $0.3711$ $0.1964$ $0.2332$ $0.169*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169*$ H26E $0.4304$ $-0.0761$ $0.2538$ $0.169*$ H26E $0.4846$ $-0.0910$ $0.1990$ $0.169*$ <	H19R	0.6046	0.3598	0.3120	0.003
$\begin{array}{ccccc} 0 & 0.549 & (1) & 0.535 & (1) & 0.535 & (2) & 0.5059 & (2) \\ H20 & 0.5877 & 0.5708 & 0.2680 & 0.084* \\ C21 & 0.4615 & (4) & 0.5887 & (5) & 0.2477 & (3) & 0.114 & (2) \\ H21A & 0.4208 & 0.5578 & 0.2702 & 0.171* \\ H21B & 0.4455 & 0.5632 & 0.1953 & 0.171* \\ H21C & 0.4640 & 0.6803 & 0.2510 & 0.171* \\ C22 & 0.5730 & (3) & 0.5705 & (5) & 0.3741 & (2) & 0.0917 & (15) \\ H22A & 0.5717 & 0.6618 & 0.3786 & 0.138* \\ H22B & 0.6288 & 0.5401 & 0.3993 & 0.138* \\ H22C & 0.5348 & 0.5329 & 0.3973 & 0.138* \\ C23 & 0.5366 & (2) & 0.1557 & (3) & 0.2033 & (2) & 0.0605 & (10) \\ H23A & 0.5477 & 0.1120 & 0.1612 & 0.073* \\ C24 & 0.4590 & (3) & 0.0970 & (4) & 0.2154 & (3) & 0.0708 & (12) \\ H24 & 0.4482 & 0.1431 & 0.2575 & 0.085* \\ C25 & 0.3822 & (3) & 0.1080 & (5) & 0.1483 & (3) & 0.115 & (2) \\ H25A & 0.3907 & 0.0632 & 0.1060 & 0.172* \\ H25B & 0.3711 & 0.1964 & 0.1352 & 0.172* \\ H25B & 0.3711 & 0.1964 & 0.1352 & 0.172* \\ H25B & 0.3711 & 0.1964 & 0.1352 & 0.172* \\ H26A & 0.4304 & -0.0761 & 0.2538 & 0.169* \\ H26A & 0.4304 & -0.0761 & 0.2538 & 0.169* \\ H26B & 0.5269 & -0.0464 & 0.2832 & 0.169* \\ H26A & 0.4304 & -0.0761 & 0.2538 & 0.169* \\ H26B & 0.5269 & -0.0464 & 0.2832 & 0.169* \\ H26B & 0.5269 & -0.0464 & 0.28$	C20	0.5469 (3)	0.5333(4)	0.3120 0.2808 (2)	0.005
1120 $0.577$ $0.5703$ $0.2405$ $0.2406$ C21 $0.4615$ (4) $0.5887$ (5) $0.2477$ (3) $0.114$ (2)H21A $0.4208$ $0.5578$ $0.2702$ $0.171*$ H21B $0.4455$ $0.5632$ $0.1953$ $0.171*$ H21C $0.4640$ $0.6803$ $0.2510$ $0.171*$ C22 $0.5730$ (3) $0.5705$ (5) $0.3741$ (2) $0.0917$ (15)H22A $0.5717$ $0.6618$ $0.3786$ $0.138*$ H22B $0.6288$ $0.5401$ $0.3993$ $0.138*$ C23 $0.5366$ (2) $0.1557$ (3) $0.2033$ (2) $0.6065$ (10)H23A $0.5477$ $0.1120$ $0.1612$ $0.073*$ H23B $0.5842$ $0.1405$ $0.2484$ $0.073*$ C24 $0.4590$ (3) $0.0970$ (4) $0.2154$ (3) $0.0708$ (12)H24 $0.4482$ $0.1431$ $0.2575$ $0.085*$ C25 $0.3822$ (3) $0.1080$ (5) $0.1483$ (3) $0.115$ (2)H25B $0.3711$ $0.1964$ $0.1352$ $0.172*$ H25B $0.3711$ $0.1964$ $0.2382$ $0.169*$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169*$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169*$ H26B $0.5269$ $-0.0464$ $0.28322$ $0.169*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169*$ F1 $0.63466$ (15) $0.7385$ (2) $0.1$	U20	0.5409 (5)	0.5555 (4)	0.2690 (2)	0.0099 (12)
C210.4015 (4)0.5367 (5) $0.2477(2)$ $0.114(2)$ H21A0.42080.55780.2702 $0.171^*$ H21B0.44550.5632 $0.1953$ $0.171^*$ H21C0.46400.6803 $0.2510$ $0.171^*$ C220.5730 (3)0.5705 (5) $0.3741 (2)$ $0.0917 (15)$ H22A0.57170.6618 $0.3786$ $0.138^*$ H22B0.6288 $0.5401$ $0.3993$ $0.138^*$ H22C0.5348 $0.5329$ $0.3973$ $0.138^*$ C230.5366 (2) $0.1557 (3)$ $0.2033 (2)$ $0.0605 (10)$ H23A $0.5477$ $0.1120$ $0.1612$ $0.073^*$ C24 $0.4590 (3)$ $0.0970 (4)$ $0.2154 (3)$ $0.0708 (12)$ H24 $0.4482$ $0.1431$ $0.2575$ $0.085^*$ C25 $0.3822 (3)$ $0.1080 (5)$ $0.1483 (3)$ $0.115 (2)$ H25A $0.3907$ $0.0632$ $0.1060$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.2538$ $0.169^*$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ F1 $0.63466 (15)$ $0.7385 (2)$ $0.03501 (14)$ $0.0871 (8)$ F2 $0.75008 (15)$ $0.7617 (2)$ $0.13489 (16)$ $0.0973 (8)$ F4 $0.70793 (18)$ $0.9559 (2)$	C21	0.3877 0.4615 (4)	0.5708	0.2080 0.2477(3)	0.084
1121A $0.4208$ $0.573$ $0.2702$ $0.171$ H21B $0.4455$ $0.5632$ $0.1953$ $0.171^*$ H21C $0.4640$ $0.6803$ $0.2510$ $0.171^*$ C22 $0.5730$ (3) $0.5705$ (5) $0.3741$ (2) $0.0917$ (15)H22A $0.5717$ $0.6618$ $0.3786$ $0.138^*$ H22B $0.6288$ $0.5401$ $0.3993$ $0.138^*$ H22C $0.5348$ $0.5329$ $0.3973$ $0.138^*$ C23 $0.5366$ (2) $0.1557$ (3) $0.2033$ (2) $0.0605$ (10)H23A $0.5477$ $0.1120$ $0.1612$ $0.073^*$ C24 $0.4590$ (3) $0.0970$ (4) $0.2154$ (3) $0.0708$ (12)H24 $0.4482$ $0.1431$ $0.2575$ $0.085^*$ C25 $0.3822$ (3) $0.1080$ (5) $0.1483$ (3) $0.115$ (2)H25A $0.3907$ $0.0632$ $0.1060$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^*$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172^*$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^*$ F1 $0.63466$ (15) $0.7385$ (2) $0.3510$ (14) $0.0871$ (8)F2 $0.7093$ (18) $0.9559$ (2) $0.15705$ (15) $0.1059$ (10)F3 $0.7173$ (17) $0.9112$ (3) $0.4222$ (16) $0.973$ (8)F4 $0$		0.4013 (4)	0.5887 (5)	0.2477 (3)	0.114(2) 0.171*
H21B $0.4435$ $0.3032$ $0.1935$ $0.171^{+}$ H21C $0.4640$ $0.6803$ $0.2510$ $0.171^{+}$ C22 $0.5730 (3)$ $0.5705 (5)$ $0.3741 (2)$ $0.0917 (15)$ H22A $0.5717$ $0.6618$ $0.3786$ $0.138^{*}$ H22B $0.6288$ $0.5401$ $0.3993$ $0.138^{*}$ H22C $0.5348$ $0.5329$ $0.3973$ $0.138^{*}$ C23 $0.5366 (2)$ $0.1557 (3)$ $0.2033 (2)$ $0.0605 (10)$ H23A $0.5477$ $0.1120$ $0.1612$ $0.073^{*}$ C24 $0.4590 (3)$ $0.0970 (4)$ $0.2154 (3)$ $0.0708 (12)$ H24 $0.4482$ $0.1431$ $0.2575$ $0.085^{*}$ C25 $0.3822 (3)$ $0.1080 (5)$ $0.1483 (3)$ $0.115 (2)$ H25A $0.3907$ $0.0632$ $0.1060$ $0.172^{*}$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^{*}$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172^{*}$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172^{*}$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^{*}$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^{*}$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^{*}$ F1 $0.63466 (15)$ $0.7385 (2)$ $0.35501 (14)$ $0.0953 (9)$ F2 $0.75008 (15)$ $0.7617 (2)$ $0.13489 (16)$ $0.0973 (8)$ F4 $0.70793 (18)$ $0.9559 (2)$ $0.15705 (15)$ $0.1059 ($		0.4208	0.5578	0.2702	0.171*
H21C $0.4040$ $0.0803$ $0.210$ $0.171^{\circ}$ C22 $0.5730$ (3) $0.5705$ (5) $0.3741$ (2) $0.0917$ (15)H22A $0.5717$ $0.6618$ $0.3786$ $0.138^{\ast}$ H22B $0.6288$ $0.5401$ $0.3993$ $0.138^{\ast}$ C23 $0.5366$ (2) $0.1557$ (3) $0.2033$ (2) $0.0605$ (10)H23A $0.5477$ $0.1120$ $0.1612$ $0.073^{\ast}$ C24 $0.4590$ (3) $0.0970$ (4) $0.2154$ (3) $0.0708$ (12)H24 $0.4482$ $0.1431$ $0.2575$ $0.085^{\ast}$ C25 $0.3822$ (3) $0.1080$ (5) $0.1483$ (3) $0.115$ (2)H25A $0.3907$ $0.0632$ $0.1060$ $0.172^{\ast}$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^{\ast}$ H25C $0.3354$ $0.0714$ $0.2402$ (4) $0.113$ (2)H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^{\ast}$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^{\ast}$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^{\ast}$ F1 $0.63466$ (15) $0.7385$ (2) $0.03501$ (14) $0.0871$ (8)F2 $0.7508$ (15) $0.7617$ (2) $0.13489$ (16) $0.0953$ (9)F3 $0.71730$ (17) $0.9112$ (3) $0.44222$ (16) $0.0973$ (8)F4 $0.70793$ (18) $0.9559$ (2) $0.15705$ (15) $0.1059$ (10)F5 $0.59126$ (16) $0.9334$ (2) $0.5722$ (17) $0.1051$ (9)F6 $0.62383$ (18) $0.784$		0.4433	0.5052	0.1933	$0.171^{\circ}$
1222 $0.3730$ $0.3705$ $0.3705$ $0.3741$ $(2)$ $0.0917$ $(13)$ $122A$ $0.5717$ $0.6618$ $0.3786$ $0.138*$ $122B$ $0.6288$ $0.5401$ $0.3993$ $0.138*$ $122C$ $0.5348$ $0.5329$ $0.3973$ $0.138*$ $122C$ $0.5348$ $0.5329$ $0.3973$ $0.138*$ $122C$ $0.5366$ $0.1557$ $0.2033$ $0.2033$ $(2)$ $123A$ $0.5477$ $0.1120$ $0.1612$ $0.073*$ $123B$ $0.5842$ $0.1405$ $0.2484$ $0.073*$ $124$ $0.44990$ $(3)$ $0.0970$ $(4)$ $0.2154$ $(3)$ $124$ $0.4482$ $0.1431$ $0.2575$ $0.085*$ $C25$ $0.3822$ $(3)$ $0.1080$ $(5)$ $0.1483$ $(3)$ $1125B$ $0.3711$ $0.1964$ $0.1352$ $0.172*$ $125B$ $0.3711$ $0.1964$ $0.1352$ $0.172*$ $125B$ $0.3711$ $0.1964$ $0.1352$ $0.172*$ $125C$ $0.3544$ $0.0714$ $0.1602$ $0.172*$ $126A$ $0.4304$ $-0.0761$ $0.2538$ $0.169*$ $126B$ $0.5269$ $-0.0464$ $0.2832$ $0.169*$ $126C$ $0.4846$ $-0.0910$ $0.1990$ $0.169*$ $126C$ $0.4846$ $-0.0910$ $0.1990$ $0.169*$ $126$ $0.71730$ $0.7172$ $0.13489$ $(6)$ $0.9973$ $12$ $0.7508$ $0.7617$ $(2)$	П21С С22	0.4040	0.0803	0.2310 0.2741(2)	$0.1/1^{\circ}$
H22A0.51170.606180.57860.138*H22B0.62880.54010.39930.138*H22C0.53480.53290.39730.138*C230.5366 (2)0.1557 (3)0.2033 (2)0.0605 (10)H23A0.54770.11200.16120.073*H23B0.58420.14050.24840.073*C240.4590 (3)0.0970 (4)0.2154 (3)0.0708 (12)H240.44820.14310.25750.085*C250.3822 (3)0.1080 (5)0.1483 (3)0.115 (2)H25B0.37110.19640.13520.172*H25C0.33540.07140.16020.172*H26A0.4304-0.07610.25380.169*H26B0.5269-0.04640.28320.169*H26B0.5269-0.04640.28320.169*H26C0.4846-0.09100.19900.169*F10.63466 (15)0.7385 (2)0.03501 (14)0.0871 (8)F20.75008 (15)0.7617 (2)0.13489 (16)0.0953 (9)F30.71730 (17)0.9112 (3)0.04222 (16)0.0973 (8)F40.70793 (18)0.9559 (2)0.15705 (15)0.1059 (10)F50.59126 (16)0.9334 (2)0.05722 (17)0.1051 (9)F60.62383 (18)0.7849 (3)0.14848 (15)0.0981 (8)P10.80124 (6)0.39039 (9)-0.02673 (5)0.0469 (3)		0.5750 (5)	0.3703(3)	0.3741 (2)	0.0917(13)
H22B0.62880.54010.39930.138*H22C0.53480.53290.39730.138*C230.5366 (2)0.1557 (3)0.2033 (2)0.0605 (10)H23A0.54770.11200.16120.073*H23B0.58420.14050.24840.073*C240.4590 (3)0.0970 (4)0.2154 (3)0.0708 (12)H240.44820.14310.25750.085*C250.3822 (3)0.1080 (5)0.1483 (3)0.115 (2)H25B0.37110.19640.13520.172*H25C0.33540.07140.16020.172*C260.4769 (3)-0.0421 (4)0.2402 (4)0.113 (2)H26A0.4304-0.07610.25380.169*H26B0.5269-0.04640.28320.169*H26C0.4846-0.09100.19900.169*F10.63466 (15)0.7385 (2)0.03501 (14)0.0871 (8)F20.75008 (15)0.7617 (2)0.13489 (16)0.0953 (9)F30.71730 (17)0.9112 (3)0.04222 (16)0.0973 (8)F40.70793 (18)0.9559 (2)0.15705 (15)0.1059 (10)F50.59126 (16)0.9334 (2)0.05722 (17)0.1051 (9)F60.62383 (18)0.7849 (3)0.14848 (15)0.0981 (8)P10.80124 (6)0.39039 (9)-0.02673 (5)0.0469 (3)	H22A	0.5/1/	0.6618	0.3786	0.138*
H22C $0.5348$ $0.5329$ $0.3973$ $0.138^*$ C23 $0.5366$ (2) $0.1557$ (3) $0.2033$ (2) $0.0605$ (10)H23A $0.5477$ $0.1120$ $0.1612$ $0.073^*$ H23B $0.5842$ $0.1405$ $0.2484$ $0.073^*$ C24 $0.4590$ (3) $0.0970$ (4) $0.2154$ (3) $0.0708$ (12)H24 $0.4482$ $0.1431$ $0.2575$ $0.085^*$ C25 $0.3822$ (3) $0.1080$ (5) $0.1483$ (3) $0.115$ (2)H25A $0.3907$ $0.0632$ $0.1060$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^*$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172^*$ C26 $0.4769$ (3) $-0.0421$ (4) $0.2402$ (4) $0.113$ (2)H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^*$ F1 $0.63466$ (15) $0.7385$ (2) $0.03501$ (14) $0.0871$ (8)F2 $0.75008$ (15) $0.7617$ (2) $0.13489$ (16) $0.0953$ (9)F3 $0.71730$ (17) $0.9112$ (3) $0.04222$ (16) $0.0973$ (8)F4 $0.70793$ (18) $0.9559$ (2) $0.15705$ (15) $0.1059$ (10)F5 $0.59126$ (16) $0.9334$ (2) $0.05722$ (17) $0.1051$ (9)F6 $0.62383$ (18) $0.7849$ (3) $0.14848$ (15) $0.0981$ (8)P1 $0.80124$ (6) $0.39039$ (9)<	H22B	0.6288	0.5401	0.3993	0.138*
$C23$ $0.3366(2)$ $0.1557(3)$ $0.2033(2)$ $0.0005(10)$ H23A $0.5477$ $0.1120$ $0.1612$ $0.073^*$ H23B $0.5842$ $0.1405$ $0.2484$ $0.073^*$ C24 $0.4590(3)$ $0.0970(4)$ $0.2154(3)$ $0.0708(12)$ H24 $0.4482$ $0.1431$ $0.2575$ $0.085^*$ C25 $0.3822(3)$ $0.1080(5)$ $0.1483(3)$ $0.115(2)$ H25A $0.3907$ $0.0632$ $0.1060$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^*$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172^*$ C26 $0.4769(3)$ $-0.0421(4)$ $0.2402(4)$ $0.113(2)$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^*$ F1 $0.63466(15)$ $0.7385(2)$ $0.03501(14)$ $0.0871(8)$ F2 $0.75008(15)$ $0.7617(2)$ $0.13489(16)$ $0.0953(9)$ F3 $0.71730(17)$ $0.9112(3)$ $0.4222(16)$ $0.0973(8)$ F4 $0.70793(18)$ $0.9559(2)$ $0.15705(15)$ $0.1059(10)$ F5 $0.59126(16)$ $0.9334(2)$ $0.05722(17)$ $0.1051(9)$ F6 $0.62383(18)$ $0.7849(3)$ $0.14848(15)$ $0.0981(8)$ P1 $0.80124(6)$ $0.39039(9)$ $-0.02673(5)$ $0.0469(3)$	H22C	0.5348	0.5329	0.3973	0.138*
H23A $0.5477$ $0.1120$ $0.1612$ $0.073^*$ H23B $0.5842$ $0.1405$ $0.2484$ $0.073^*$ C24 $0.4590$ (3) $0.0970$ (4) $0.2154$ (3) $0.0708$ (12)H24 $0.4482$ $0.1431$ $0.2575$ $0.085^*$ C25 $0.3822$ (3) $0.1080$ (5) $0.1483$ (3) $0.115$ (2)H25A $0.3907$ $0.0632$ $0.1060$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^*$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172^*$ C26 $0.4769$ (3) $-0.0421$ (4) $0.2402$ (4) $0.113$ (2)H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^*$ F1 $0.63466$ (15) $0.7385$ (2) $0.03501$ (14) $0.0871$ (8)F2 $0.75008$ (15) $0.7617$ (2) $0.13489$ (16) $0.0953$ (9)F3 $0.71730$ (17) $0.9112$ (3) $0.4222$ (16) $0.0973$ (8)F4 $0.70793$ (18) $0.9559$ (2) $0.15705$ (15) $0.1059$ (10)F5 $0.59126$ (16) $0.9334$ (2) $0.05722$ (17) $0.1051$ (9)F6 $0.62383$ (18) $0.7849$ (3) $0.14848$ (15) $0.0981$ (8)P1 $0.80124$ (6) $0.39039$ (9) $-0.02673$ (5) $0.0469$ (3)	C23	0.5366 (2)	0.1557 (3)	0.2033 (2)	0.0605 (10)
H23B $0.5842$ $0.1405$ $0.2484$ $0.073^*$ C24 $0.4590 (3)$ $0.0970 (4)$ $0.2154 (3)$ $0.0708 (12)$ H24 $0.4482$ $0.1431$ $0.2575$ $0.085^*$ C25 $0.3822 (3)$ $0.1080 (5)$ $0.1483 (3)$ $0.115 (2)$ H25A $0.3907$ $0.0632$ $0.1060$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^*$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172^*$ C26 $0.4769 (3)$ $-0.0421 (4)$ $0.2402 (4)$ $0.113 (2)$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^*$ F1 $0.63466 (15)$ $0.7385 (2)$ $0.03501 (14)$ $0.0871 (8)$ F2 $0.75008 (15)$ $0.7617 (2)$ $0.13489 (16)$ $0.0953 (9)$ F3 $0.71730 (17)$ $0.9112 (3)$ $0.4222 (16)$ $0.0973 (8)$ F4 $0.70793 (18)$ $0.9559 (2)$ $0.15705 (15)$ $0.1059 (10)$ F5 $0.59126 (16)$ $0.9334 (2)$ $0.05722 (17)$ $0.1051 (9)$ F6 $0.62383 (18)$ $0.7849 (3)$ $0.14848 (15)$ $0.0981 (8)$ P1 $0.80124 (6)$ $0.39039 (9)$ $-0.02673 (5)$ $0.0469 (3)$	H23A	0.5477	0.1120	0.1612	0.073*
C24 $0.4590 (3)$ $0.0970 (4)$ $0.2154 (3)$ $0.0708 (12)$ H24 $0.4482$ $0.1431$ $0.2575$ $0.085*$ C25 $0.3822 (3)$ $0.1080 (5)$ $0.1483 (3)$ $0.115 (2)$ H25A $0.3907$ $0.0632$ $0.1060$ $0.172*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172*$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172*$ C26 $0.4769 (3)$ $-0.0421 (4)$ $0.2402 (4)$ $0.113 (2)$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169*$ F1 $0.63466 (15)$ $0.7385 (2)$ $0.03501 (14)$ $0.0871 (8)$ F2 $0.75008 (15)$ $0.7617 (2)$ $0.13489 (16)$ $0.0953 (9)$ F3 $0.71730 (17)$ $0.9112 (3)$ $0.4222 (16)$ $0.0973 (8)$ F4 $0.70793 (18)$ $0.9559 (2)$ $0.15705 (15)$ $0.1059 (10)$ F5 $0.59126 (16)$ $0.9334 (2)$ $0.05722 (17)$ $0.1051 (9)$ F6 $0.62383 (18)$ $0.7849 (3)$ $0.14848 (15)$ $0.0981 (8)$ P1 $0.80124 (6)$ $0.39039 (9)$ $-0.02673 (5)$ $0.0469 (3)$	H23B	0.5842	0.1405	0.2484	0.073*
H24 $0.4482$ $0.1431$ $0.2575$ $0.085^*$ C25 $0.3822 (3)$ $0.1080 (5)$ $0.1483 (3)$ $0.115 (2)$ H25A $0.3907$ $0.0632$ $0.1060$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^*$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172^*$ C26 $0.4769 (3)$ $-0.0421 (4)$ $0.2402 (4)$ $0.113 (2)$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^*$ F1 $0.63466 (15)$ $0.7385 (2)$ $0.03501 (14)$ $0.0871 (8)$ F2 $0.75008 (15)$ $0.7617 (2)$ $0.13489 (16)$ $0.0953 (9)$ F3 $0.71730 (17)$ $0.9112 (3)$ $0.04222 (16)$ $0.0973 (8)$ F4 $0.70793 (18)$ $0.9559 (2)$ $0.15705 (15)$ $0.1059 (10)$ F5 $0.59126 (16)$ $0.9334 (2)$ $0.05722 (17)$ $0.1051 (9)$ F6 $0.62383 (18)$ $0.7849 (3)$ $0.14848 (15)$ $0.0981 (8)$ P1 $0.80124 (6)$ $0.39039 (9)$ $-0.02673 (5)$ $0.0469 (3)$	C24	0.4590 (3)	0.0970 (4)	0.2154 (3)	0.0708 (12)
C25 $0.3822 (3)$ $0.1080 (5)$ $0.1483 (3)$ $0.115 (2)$ H25A $0.3907$ $0.0632$ $0.1060$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^*$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172^*$ C26 $0.4769 (3)$ $-0.0421 (4)$ $0.2402 (4)$ $0.113 (2)$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^*$ F1 $0.63466 (15)$ $0.7385 (2)$ $0.03501 (14)$ $0.0871 (8)$ F2 $0.75008 (15)$ $0.7617 (2)$ $0.13489 (16)$ $0.0953 (9)$ F3 $0.71730 (17)$ $0.9112 (3)$ $0.4222 (16)$ $0.0973 (8)$ F4 $0.70793 (18)$ $0.9559 (2)$ $0.15705 (15)$ $0.1059 (10)$ F5 $0.59126 (16)$ $0.9334 (2)$ $0.05722 (17)$ $0.1051 (9)$ F6 $0.62383 (18)$ $0.7849 (3)$ $0.14848 (15)$ $0.0981 (8)$ P1 $0.80124 (6)$ $0.39039 (9)$ $-0.02673 (5)$ $0.0469 (3)$	H24	0.4482	0.1431	0.2575	0.085*
H25A $0.3907$ $0.0632$ $0.1060$ $0.172^*$ H25B $0.3711$ $0.1964$ $0.1352$ $0.172^*$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172^*$ C26 $0.4769(3)$ $-0.0421(4)$ $0.2402(4)$ $0.113(2)$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^*$ F1 $0.63466(15)$ $0.7385(2)$ $0.03501(14)$ $0.0871(8)$ F2 $0.75008(15)$ $0.7617(2)$ $0.13489(16)$ $0.0953(9)$ F3 $0.71730(17)$ $0.9112(3)$ $0.04222(16)$ $0.0973(8)$ F4 $0.70793(18)$ $0.9559(2)$ $0.15705(15)$ $0.1059(10)$ F5 $0.59126(16)$ $0.9334(2)$ $0.05722(17)$ $0.1051(9)$ F6 $0.62383(18)$ $0.7849(3)$ $0.14848(15)$ $0.0981(8)$ P1 $0.80124(6)$ $0.39039(9)$ $-0.02673(5)$ $0.0469(3)$	C25	0.3822 (3)	0.1080 (5)	0.1483 (3)	0.115 (2)
H25B $0.3711$ $0.1964$ $0.1352$ $0.172*$ H25C $0.3354$ $0.0714$ $0.1602$ $0.172*$ C26 $0.4769(3)$ $-0.0421(4)$ $0.2402(4)$ $0.113(2)$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169*$ F1 $0.63466(15)$ $0.7385(2)$ $0.03501(14)$ $0.0871(8)$ F2 $0.75008(15)$ $0.7617(2)$ $0.13489(16)$ $0.0953(9)$ F3 $0.71730(17)$ $0.9112(3)$ $0.04222(16)$ $0.0973(8)$ F4 $0.70793(18)$ $0.9559(2)$ $0.15705(15)$ $0.1059(10)$ F5 $0.59126(16)$ $0.9334(2)$ $0.05722(17)$ $0.1051(9)$ F6 $0.62383(18)$ $0.7849(3)$ $0.14848(15)$ $0.0981(8)$ P1 $0.80124(6)$ $0.39039(9)$ $-0.02673(5)$ $0.0469(3)$	H25A	0.3907	0.0632	0.1060	0.172*
H25C $0.3354$ $0.0714$ $0.1602$ $0.172^*$ C26 $0.4769 (3)$ $-0.0421 (4)$ $0.2402 (4)$ $0.113 (2)$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^*$ F1 $0.63466 (15)$ $0.7385 (2)$ $0.03501 (14)$ $0.0871 (8)$ F2 $0.75008 (15)$ $0.7617 (2)$ $0.13489 (16)$ $0.0953 (9)$ F3 $0.71730 (17)$ $0.9112 (3)$ $0.04222 (16)$ $0.0973 (8)$ F4 $0.70793 (18)$ $0.9559 (2)$ $0.15705 (15)$ $0.1059 (10)$ F5 $0.59126 (16)$ $0.9334 (2)$ $0.05722 (17)$ $0.1051 (9)$ F6 $0.62383 (18)$ $0.7849 (3)$ $0.14848 (15)$ $0.0981 (8)$ P1 $0.80124 (6)$ $0.39039 (9)$ $-0.02673 (5)$ $0.0469 (3)$	H25B	0.3711	0.1964	0.1352	0.172*
C26 $0.4769 (3)$ $-0.0421 (4)$ $0.2402 (4)$ $0.113 (2)$ H26A $0.4304$ $-0.0761$ $0.2538$ $0.169*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169*$ F1 $0.63466 (15)$ $0.7385 (2)$ $0.03501 (14)$ $0.0871 (8)$ F2 $0.75008 (15)$ $0.7617 (2)$ $0.13489 (16)$ $0.0953 (9)$ F3 $0.71730 (17)$ $0.9112 (3)$ $0.04222 (16)$ $0.0973 (8)$ F4 $0.70793 (18)$ $0.9559 (2)$ $0.15705 (15)$ $0.1059 (10)$ F5 $0.59126 (16)$ $0.9334 (2)$ $0.05722 (17)$ $0.1051 (9)$ F6 $0.62383 (18)$ $0.7849 (3)$ $0.14848 (15)$ $0.0981 (8)$ P1 $0.80124 (6)$ $0.39039 (9)$ $-0.02673 (5)$ $0.0469 (3)$	H25C	0.3354	0.0714	0.1602	0.172*
H26A $0.4304$ $-0.0761$ $0.2538$ $0.169^*$ H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^*$ F1 $0.63466 (15)$ $0.7385 (2)$ $0.03501 (14)$ $0.0871 (8)$ F2 $0.75008 (15)$ $0.7617 (2)$ $0.13489 (16)$ $0.0953 (9)$ F3 $0.71730 (17)$ $0.9112 (3)$ $0.04222 (16)$ $0.0973 (8)$ F4 $0.70793 (18)$ $0.9559 (2)$ $0.15705 (15)$ $0.1059 (10)$ F5 $0.59126 (16)$ $0.9334 (2)$ $0.05722 (17)$ $0.1051 (9)$ F6 $0.62383 (18)$ $0.7849 (3)$ $0.14848 (15)$ $0.0981 (8)$ P1 $0.80124 (6)$ $0.39039 (9)$ $-0.02673 (5)$ $0.0469 (3)$	C26	0.4769 (3)	-0.0421 (4)	0.2402 (4)	0.113 (2)
H26B $0.5269$ $-0.0464$ $0.2832$ $0.169^*$ H26C $0.4846$ $-0.0910$ $0.1990$ $0.169^*$ F1 $0.63466 (15)$ $0.7385 (2)$ $0.03501 (14)$ $0.0871 (8)$ F2 $0.75008 (15)$ $0.7617 (2)$ $0.13489 (16)$ $0.0953 (9)$ F3 $0.71730 (17)$ $0.9112 (3)$ $0.04222 (16)$ $0.0973 (8)$ F4 $0.70793 (18)$ $0.9559 (2)$ $0.15705 (15)$ $0.1059 (10)$ F5 $0.59126 (16)$ $0.9334 (2)$ $0.05722 (17)$ $0.1051 (9)$ F6 $0.62383 (18)$ $0.7849 (3)$ $0.14848 (15)$ $0.0981 (8)$ P1 $0.80124 (6)$ $0.39039 (9)$ $-0.02673 (5)$ $0.0469 (3)$	H26A	0.4304	-0.0761	0.2538	0.169*
H26C $0.4846$ $-0.0910$ $0.1990$ $0.169*$ F1 $0.63466 (15)$ $0.7385 (2)$ $0.03501 (14)$ $0.0871 (8)$ F2 $0.75008 (15)$ $0.7617 (2)$ $0.13489 (16)$ $0.0953 (9)$ F3 $0.71730 (17)$ $0.9112 (3)$ $0.04222 (16)$ $0.0973 (8)$ F4 $0.70793 (18)$ $0.9559 (2)$ $0.15705 (15)$ $0.1059 (10)$ F5 $0.59126 (16)$ $0.9334 (2)$ $0.05722 (17)$ $0.1051 (9)$ F6 $0.62383 (18)$ $0.7849 (3)$ $0.14848 (15)$ $0.0981 (8)$ P1 $0.80124 (6)$ $0.39039 (9)$ $-0.02673 (5)$ $0.0469 (3)$	H26B	0.5269	-0.0464	0.2832	0.169*
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	H26C	0.4846	-0.0910	0.1990	0.169*
F20.75008 (15)0.7617 (2)0.13489 (16)0.0953 (9)F30.71730 (17)0.9112 (3)0.04222 (16)0.0973 (8)F40.70793 (18)0.9559 (2)0.15705 (15)0.1059 (10)F50.59126 (16)0.9334 (2)0.05722 (17)0.1051 (9)F60.62383 (18)0.7849 (3)0.14848 (15)0.0981 (8)P10.80124 (6)0.39039 (9)-0.02673 (5)0.0469 (3)	F1	0.63466 (15)	0.7385 (2)	0.03501 (14)	0.0871 (8)
F30.71730 (17)0.9112 (3)0.04222 (16)0.0973 (8)F40.70793 (18)0.9559 (2)0.15705 (15)0.1059 (10)F50.59126 (16)0.9334 (2)0.05722 (17)0.1051 (9)F60.62383 (18)0.7849 (3)0.14848 (15)0.0981 (8)P10.80124 (6)0.39039 (9)-0.02673 (5)0.0469 (3)	F2	0.75008 (15)	0.7617 (2)	0.13489 (16)	0.0953 (9)
F40.70793 (18)0.9559 (2)0.15705 (15)0.1059 (10)F50.59126 (16)0.9334 (2)0.05722 (17)0.1051 (9)F60.62383 (18)0.7849 (3)0.14848 (15)0.0981 (8)P10.80124 (6)0.39039 (9)-0.02673 (5)0.0469 (3)	F3	0.71730 (17)	0.9112 (3)	0.04222 (16)	0.0973 (8)
F50.59126 (16)0.9334 (2)0.05722 (17)0.1051 (9)F60.62383 (18)0.7849 (3)0.14848 (15)0.0981 (8)P10.80124 (6)0.39039 (9)-0.02673 (5)0.0469 (3)	F4	0.70793 (18)	0.9559 (2)	0.15705 (15)	0.1059 (10)
F60.62383 (18)0.7849 (3)0.14848 (15)0.0981 (8)P10.80124 (6)0.39039 (9)-0.02673 (5)0.0469 (3)	F5	0.59126 (16)	0.9334 (2)	0.05722 (17)	0.1051 (9)
P1 0.80124 (6) 0.39039 (9) -0.02673 (5) 0.0469 (3)	F6	0.62383 (18)	0.7849 (3)	0.14848 (15)	0.0981 (8)
	P1	0.80124 (6)	0.39039 (9)	-0.02673 (5)	0.0469 (3)

# supporting information

P2	0.52962 (6)	0.32919 (9)	0.18315 (5)	0.0476 (3)
P3	0.67083 (6)	0.84835 (9)	0.09545 (6)	0.0561 (3)

Atomic displacement parameters  $(Å^2)$ 

	$U^{11}$	$U^{22}$	$U^{33}$	$U^{12}$	$U^{13}$	U <sup>23</sup>
Col	0.0484 (3)	0.0352 (3)	0.0388 (3)	-0.0031 (2)	0.0149 (2)	-0.0013 (2)
C1	0.0513 (19)	0.0361 (19)	0.0372 (17)	-0.0008 (16)	0.0150 (15)	-0.0037 (15)
C2	0.069 (2)	0.033 (2)	0.044 (2)	-0.0023 (17)	0.0203 (17)	-0.0092 (16)
C3	0.066 (2)	0.052 (3)	0.052 (2)	-0.0226 (19)	0.0213 (19)	-0.0142 (19)
C4	0.048 (2)	0.063 (3)	0.045 (2)	-0.0019 (19)	0.0064 (16)	-0.0064 (19)
C5	0.053 (2)	0.044 (2)	0.0401 (19)	0.0021 (17)	0.0109 (16)	0.0053 (16)
C6	0.061 (2)	0.043 (2)	0.067 (2)	-0.0035 (18)	0.0257 (19)	0.0008 (18)
C7	0.078 (3)	0.057 (3)	0.094 (3)	-0.019 (2)	0.036 (3)	-0.011 (2)
C8	0.089 (4)	0.107 (4)	0.150 (5)	-0.031 (3)	-0.008 (4)	-0.014 (4)
C9	0.123 (4)	0.060 (3)	0.148 (5)	-0.031 (3)	0.041 (4)	0.010 (3)
C10	0.066 (2)	0.062 (3)	0.047 (2)	-0.0002 (19)	0.0268 (18)	0.0003 (19)
C11	0.083 (3)	0.068 (3)	0.072 (3)	-0.021 (2)	0.046 (2)	-0.022 (2)
C12	0.129 (4)	0.121 (5)	0.081 (4)	-0.029 (4)	0.051 (3)	-0.042 (3)
C13	0.163 (5)	0.062 (3)	0.101 (4)	0.027 (3)	0.046 (4)	-0.014 (3)
C14	0.055 (2)	0.0317 (19)	0.0366 (18)	0.0033 (15)	0.0173 (15)	-0.0004 (15)
C15	0.060 (2)	0.043 (2)	0.0408 (19)	0.0072 (17)	0.0193 (17)	0.0054 (16)
C16	0.051 (2)	0.076 (3)	0.043 (2)	0.005 (2)	0.0113 (17)	0.001 (2)
C17	0.067 (3)	0.065 (3)	0.041 (2)	-0.022 (2)	0.0178 (18)	-0.0124 (19)
C18	0.074 (3)	0.034 (2)	0.041 (2)	-0.0064 (17)	0.0211 (18)	-0.0087 (16)
C19	0.063 (2)	0.052 (2)	0.047 (2)	0.0069 (18)	0.0228 (18)	0.0029 (17)
C20	0.094 (3)	0.054 (3)	0.072 (3)	-0.013 (2)	0.041 (2)	-0.013 (2)
C21	0.167 (5)	0.066 (3)	0.091 (4)	0.056 (4)	0.015 (4)	-0.008 (3)
C22	0.105 (4)	0.093 (4)	0.078 (3)	-0.014 (3)	0.030 (3)	-0.035 (3)
C23	0.075 (3)	0.040 (2)	0.074 (3)	-0.0032 (19)	0.034 (2)	0.004 (2)
C24	0.077 (3)	0.052 (3)	0.087 (3)	-0.014 (2)	0.030 (2)	0.004 (2)
C25	0.087 (4)	0.119 (5)	0.116 (4)	-0.041 (3)	0.001 (3)	0.011 (4)
C26	0.109 (4)	0.053 (3)	0.186 (6)	-0.014 (3)	0.061 (4)	0.024 (3)
F1	0.0994 (18)	0.0704 (17)	0.0828 (17)	-0.0229 (14)	0.0160 (14)	-0.0294 (14)
F2	0.0789 (16)	0.0622 (16)	0.120 (2)	0.0124 (13)	-0.0038 (15)	0.0095 (15)
F3	0.105 (2)	0.089 (2)	0.103 (2)	-0.0209 (16)	0.0388 (16)	0.0105 (16)
F4	0.142 (3)	0.0577 (16)	0.096 (2)	-0.0114 (16)	0.0059 (17)	-0.0290 (15)
F5	0.0843 (18)	0.0725 (18)	0.139 (2)	0.0210 (14)	0.0074 (17)	0.0211 (17)
F6	0.128 (2)	0.0788 (19)	0.105 (2)	0.0015 (17)	0.0616 (18)	0.0080 (16)
P1	0.0508 (5)	0.0438 (6)	0.0477 (5)	-0.0007 (4)	0.0179 (4)	-0.0006 (4)
P2	0.0546 (5)	0.0429 (6)	0.0472 (5)	0.0024 (4)	0.0188 (4)	0.0008 (4)
P3	0.0628 (6)	0.0361 (6)	0.0614 (6)	-0.0009 (5)	0.0081 (5)	-0.0028 (5)

## Geometric parameters (Å, °)

Co1—C16	2.028 (3)	C13—H13B	0.9600
Co1—C2	2.028 (3)	C13—H13C	0.9600
Co1—C18	2.033 (3)	C14—C15	1.430 (4)

Co1—C17	2.034 (3)	C14—C18	1.433 (4)
Col—C15	2.036 (3)	C14—P2	1.823 (3)
Co1—C5	2.038 (3)	C15—C16	1.407 (5)
Co1—C1	2.041 (3)	C15—H15	0.9800
Co1—C3	2.045 (3)	C16—C17	1.403 (5)
Co1—C4	2,053(3)	C16—H16	0.9800
Co1-C14	2.055(3)	C17-C18	1410(5)
C1-C5	1 431 (5)	C17—H17	0.9800
C1-C2	1.131(3) 1.437(4)	C18—H18	0.9800
C1P1	1.437(4) 1 824 (3)	$C_{10}$ $C_{20}$	1.515(5)
$C_2 C_3$	1.024(5)	$C_{19}$ $C_{20}$	1.515(3)
C2 H2	0.0800	$C_{10}$ $H_{10A}$	0.0700
$C_2 = C_1$	1,412,(5)	C10 H10P	0.9700
$C_{3}$	1.413(3)	C19—R19B	0.9700
	0.9800	C20—C21	1.515(0)
	1.421 (5)	C20—C22	1.532 (5)
C4—H4	0.9800	C20—H20	0.9800
C5—H5	0.9800	C21—H2IA	0.9600
C6—C7	1.513 (5)	C21—H21B	0.9600
C6—P1	1.845 (4)	C21—H21C	0.9600
С6—Н6А	0.9700	C22—H22A	0.9600
С6—Н6В	0.9700	C22—H22B	0.9600
C7—C8	1.508 (6)	C22—H22C	0.9600
С7—С9	1.530 (6)	C23—C24	1.519 (5)
С7—Н7	0.9800	C23—P2	1.850 (4)
C8—H8A	0.9600	С23—Н23А	0.9700
C8—H8B	0.9600	С23—Н23В	0.9700
C8—H8C	0.9600	C24—C25	1.487 (6)
С9—Н9А	0.9600	C24—C26	1.527 (6)
С9—Н9В	0.9600	C24—H24	0.9800
С9—Н9С	0.9600	С25—Н25А	0.9600
C10—C11	1.523 (5)	С25—Н25В	0.9600
C10—P1	1.851 (4)	С25—Н25С	0.9600
C10—H10A	0.9700	C26—H26A	0.9600
C10—H10B	0.9700	C26—H26B	0.9600
C11—C13	1.512 (6)	C26—H26C	0.9600
C11—C12	1.526 (5)	F1—P3	1.586 (2)
C11—H11	0.9800	F2—P3	1.585 (2)
C12—H12A	0.9600	F3—P3	1.579 (3)
C12—H12B	0.9600	F4—P3	1.584(2)
C12 H12D	0.9600	F5P3	1.567(2)
C13_H13A	0.9600	F6—P3	1.576(2) 1.585(3)
CIJ-IIIJA	0.9000	10-15	1.565 (5)
C16—Co1—C2	109.48 (15)	C11—C12—H12A	109.5
C16—Co1—C18	68.21 (15)	C11—C12—H12B	109.5
C2—Co1—C18	176.26 (14)	H12A—C12—H12B	109.5
C16—Co1—C17	40.40 (14)	C11—C12—H12C	109.5
C2—Co1—C17	135.80 (16)	H12A—C12—H12C	109.5
C18—Co1—C17	40.57 (14)	H12B—C12—H12C	109.5
	× /		

C16—Co1—C15	40.50 (13)	C11—C13—H13A	109.5
C2—Co1—C15	112.05 (14)	C11—C13—H13B	109.5
C18—Co1—C15	68.31 (14)	H13A—C13—H13B	109.5
C17—Co1—C15	68.08 (15)	C11—C13—H13C	109.5
C16—Co1—C5	141.94 (15)	H13A—C13—H13C	109.5
C2—Co1—C5	68.72 (14)	H13B—C13—H13C	109.5
C18—Co1—C5	111.10 (14)	C15—C14—C18	105.9 (3)
C17—Co1—C5	113.26 (15)	C15—C14—P2	130.1 (3)
C15—Co1—C5	177.38 (13)	C18—C14—P2	124.0 (3)
$C_{16} = C_{01} = C_{1}$	111.52 (14)	$C_{15}$ $C_{14}$ $C_{01}$	68.81 (18)
$C^2$ — $C_01$ — $C_1$	41 36 (12)	C18 - C14 - Co1	68 62 (18)
C18 - Co1 - C1	136 13 (13)	$P^2 - C_1 4 - C_0 1$	12659(17)
$C_{17} - C_{01} - C_{1}$	109 39 (14)	$C_{16}$ $C_{15}$ $C_{14}$	120.39(17) 108.8(3)
$C_{15} = C_{01} = C_{1}$	141.09(13)	$C_{16}$ $C_{15}$ $C_{14}$	69 44 (19)
$C_{2}$	41.07 (13)	$C_{14}$ $C_{15}$ $C_{01}$	70 28 (18)
$C_{16}$ $C_{21}$ $C_{3}$	136.00(16)	$C_{14} = C_{15} = C_{01}$	125.6
$C_1^2 = C_2^1 = C_3^2$	130.09 (10)	$C_{10} = C_{15} = H_{15}$	125.6
$C_2 = C_0 = C_3$	40.00(14) 142.01(15)	Col C15 H15	125.0
$C_{18} = C_{01} = C_{3}$	145.01(15) 175.80(16)	Сог—Ст3—Н13	123.0
C17 - C01 - C3	1/5.89 (16)	C17 - C16 - C13	108.4 (3)
$C_{15} = C_{01} = C_{3}$	110.4/(15)	C1/-C16-C01	70.0 (2)
$C_{3}$	68.35 (15)		/0.07 (19)
	69.14 (13)	C17—C16—H16	125.8
C16—Co1—C4	176.30 (16)	С15—С16—Н16	125.8
C2—Co1—C4	68.30 (14)	Co1—C16—H16	125.8
C18—Co1—C4	114.16 (15)	C16—C17—C18	108.1 (3)
C17—Co1—C4	143.21 (16)	C16—C17—Co1	69.6 (2)
C15—Co1—C4	136.99 (15)	C18—C17—Co1	69.65 (19)
C5—Co1—C4	40.65 (13)	C16—C17—H17	126.0
C1—Co1—C4	68.97 (14)	C18—C17—H17	126.0
C3—Co1—C4	40.35 (14)	Co1—C17—H17	126.0
C16—Co1—C14	68.80 (14)	C17—C18—C14	108.8 (3)
C2—Co1—C14	141.54 (13)	C17-C18-Co1	69.8 (2)
C18—Co1—C14	41.02 (12)	C14-C18-Co1	70.36 (18)
C17—Co1—C14	68.82 (14)	C17—C18—H18	125.6
C15—Co1—C14	40.91 (12)	C14—C18—H18	125.6
C5—Co1—C14	137.02 (13)	Co1-C18-H18	125.6
C1—Co1—C14	177.04 (13)	C20—C19—P2	116.2 (3)
C3—Co1—C14	112.82 (14)	С20—С19—Н19А	108.2
C4—Co1—C14	110.91 (14)	Р2—С19—Н19А	108.2
C5—C1—C2	106.3 (3)	С20—С19—Н19В	108.2
C5-C1-P1	130.4 (3)	P2-C19-H19B	108.2
C2-C1-P1	123.3 (3)	H19A—C19—H19B	107.4
C5-C1-Co1	69.38 (19)	C19-C20-C21	112.4 (4)
$C_2 - C_1 - C_0 I$	68 86 (18)	$C_{19} = C_{20} = C_{22}$	112.1(1) 110.6(4)
P1 - C1 - Co1	124 48 (16)	$C_{21}$ $C_{20}$ $C_{22}$ $C_{22}$	110.4 (4)
$C_{3}$ $-C_{2}$ $-C_{1}$	108 7 (3)	C19 - C20 - H20	107.8
$C_{3}$ $-C_{2}$ $-C_{01}$	70 3 (2)	$C_{21}$ $C_{20}$ $H_{20}$	107.8
C1 - C2 - Co1	69.78 (18)	$C_{22} = C_{20} = H_{20}$	107.8
	07.70(10)	$\bigcirc 22$ $\bigcirc 220$ 1120	10/.0

С3С2Н2	125.6	C20_C21_H21A	109 5
$C_{1} = C_{2} = H_{2}$	125.6	$C_{20}$ $C_{21}$ $H_{21R}$	109.5
$C_1 = C_2 = H_2$	125.6	$L_{20}$ $L_{21}$ $L$	109.5
$C_0 = C_2 = C_2$	123.0 108.2 (2)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	109.5
$C_{4} = C_{3} = C_{2}$	100.2(3)		109.5
$C_4 = C_3 = C_0 I$	(0.10(19))	$H_2 IA = C_2 I = H_2 IC$	109.5
$C_2 = C_3 = C_0 I$	09.00 (19)	$H_2IB = C_2I = H_2IC$	109.5
C4 - C3 - H3	125.9	C20—C22—H22A	109.5
C2—C3—H3	125.9	C20—C22—H22B	109.5
Col—C3—H3	125.9	H22A—C22—H22B	109.5
C3—C4—C5	108.0 (3)	C20—C22—H22C	109.5
C3—C4—Co1	69.49 (19)	H22A—C22—H22C	109.5
C5—C4—Co1	69.10 (18)	H22B—C22—H22C	109.5
C3—C4—H4	126.0	C24—C23—P2	115.0 (3)
C5—C4—H4	126.0	C24—C23—H23A	108.5
Co1—C4—H4	126.0	P2—C23—H23A	108.5
C4—C5—C1	108.7 (3)	C24—C23—H23B	108.5
C4—C5—Co1	70.25 (19)	Р2—С23—Н23В	108.5
C1C5Co1	69.55 (18)	H23A—C23—H23B	107.5
С4—С5—Н5	125.6	C25—C24—C23	113.7 (4)
C1—C5—H5	125.6	C25—C24—C26	111.2 (4)
Co1—C5—H5	125.6	C23—C24—C26	109.4 (4)
C7—C6—P1	112.9 (3)	C25—C24—H24	107.4
C7—C6—H6A	109.0	C23—C24—H24	107.4
P1—C6—H6A	109.0	C26—C24—H24	107.4
C7—C6—H6B	109.0	$C_{24}$ $C_{25}$ $H_{25A}$	109.5
P1—C6—H6B	109.0	$C_{24}$ $C_{25}$ $H_{25R}$	109.5
Н6АС6Н6В	107.8	$H_{25}^{-}$ $H_{$	109.5
$C_8 C_7 C_6$	111 5 (4)	$C_{24}$ $C_{25}$ $H_{25}$ $H_{25}$	109.5
$C_{8} = C_{7} = C_{9}$	111.3(4) 109.4(4)	$H_{25}^{-1}$	109.5
$C_{6} = C_{7} = C_{9}$	109.4(4)	$H_{25}^{-} = C_{25}^{-} = H_{25}^{-} = H_{25}^{-} C_{25}^{-} = H_{25}^{-} C_$	109.5
$C_0 = C_7 = U_7$	10.0 (4)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	109.5
$C_{0} = C_{1} = H_{1}$	108.4	$C_{24}$ $C_{20}$ $H_{20}$ $H$	109.5
	108.4	C24—C20—H26B	109.5
C9—C/—H/	108.4	$H_{20}A - C_{20} - H_{20}B$	109.5
C/C8H8A	109.5	C24—C26—H26C	109.5
С/—С8—Н8В	109.5	H26A—C26—H26C	109.5
H8A—C8—H8B	109.5	H26B—C26—H26C	109.5
С7—С8—Н8С	109.5	C1—P1—C6	101.32 (16)
H8A—C8—H8C	109.5	C1—P1—C10	98.64 (16)
H8B—C8—H8C	109.5	C6—P1—C10	99.83 (17)
С7—С9—Н9А	109.5	C14—P2—C23	99.00 (16)
С7—С9—Н9В	109.5	C14—P2—C19	98.79 (16)
H9A—C9—H9B	109.5	C23—P2—C19	99.08 (18)
С7—С9—Н9С	109.5	F5—P3—F3	89.92 (16)
Н9А—С9—Н9С	109.5	F5—P3—F4	90.45 (15)
Н9В—С9—Н9С	109.5	F3—P3—F4	89.63 (15)
C11—C10—P1	115.8 (3)	F5—P3—F6	89.95 (16)
C11-C10-H10A	108.3	F3—P3—F6	179.69 (17)
P1-C10-H10A	108.3	F4—P3—F6	90.65 (16)

C11—C10—H10B	108.3	F5—P3—F2	178.99 (18)
P1-C10-H10B	108.3	F3—P3—F2	91.09 (16)
H10A—C10—H10B	107.4	F4—P3—F2	89.53 (14)
C13—C11—C10	112.2 (4)	F6—P3—F2	89.04 (16)
C13—C11—C12	110.9 (4)	F5—P3—F1	90.58 (15)
C10-C11-C12	110.1 (4)	F3—P3—F1	90.94 (15)
C13—C11—H11	107.8	F4—P3—F1	178.83 (16)
C10—C11—H11	107.8	F6—P3—F1	88.78 (14)
C12—C11—H11	107.8	F2—P3—F1	89 44 (14)
	107.0	12 13 11	0,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
C16—Co1—C1—C5	-146.7(2)	C15—Co1—C14—C18	117.8 (3)
C2—Co1—C1—C5	117.9 (3)	C5-Co1-C14-C18	-64.6(3)
C18—Co1—C1—C5	-66.2 (3)	C3—Co1—C14—C18	-146.8(2)
$C_{17} - C_{01} - C_{1} - C_{5}$	-103.5(2)	C4-C01-C14-C18	-103.2(2)
$C_{15} - C_{01} - C_{1} - C_{5}$	177.7 (2)	$C_{16} - C_{01} - C_{14} - P_{2}$	-162.0(3)
$C_{3}$ — $C_{0}$ ]— $C_{1}$ — $C_{5}$	80.6 (2)	$C_{2}$ $C_{01}$ $C_{14}$ $P_{2}$	-671(3)
C4-Co1-C1-C5	37 2 (2)	$C_{18}$ $C_{01}$ $C_{14}$ $P_{2}$	1172(3)
$C_{16} - C_{01} - C_{1} - C_{2}$	95 4 (2)	$C_{17}$ $C_{01}$ $C_{14}$ $P_{2}$	1545(3)
$C_{18} = C_{01} = C_{12} = C_{22}$	175.9(2)	$C_{15}$ $C_{01}$ $C_{14}$ $P_{2}$	-1250(3)
$C_{17}^{-10} = C_{11}^{-10} = C_{12}^{-10}$	175.5(2) 138.6(2)	$C_{2} = C_{2} = C_{1} = C_{1} = C_{1} = C_{2}$	526(3)
C15-C01-C1-C2	59 8 (3)	$C_3 = C_0 = C_1 + C_1 + C_2$	-29.6(3)
$C_{13} = C_{11} = C_{11} = C_{22}$	-117.9(3)	$C_{4}$ Col Cl4 P2	29.0(3)
$C_{3} = C_{01} = C_{1} = C_{2}$	-27.2(2)	$C_{1}^{+-}C_{1$	14.0(2)
$C_{3} = C_{1} = C_{1} = C_{2}$	-90.6(2)	$P_{2} = C_{14} = C_{15} = C_{16}$	0.0(4)
$C_{4} = C_{1} = C_{1} = C_{2}$	-30.0(2)	$r_2 - c_{14} - c_{15} - c_{16}$	1/9.3(2)
$C_{10} = C_{11} = C_{11} = P_{11}$	-21.2(3)	$C_{12} = C_{14} = C_{15} = C_{16}$	58.9 (2)
$C_2 = C_0 = C_1 = P_1$	-110.0(3)	C18 - C14 - C15 - C01	-38.9(2)
C18 - C01 - C1 - P1	59.3 (3)	P2-C14-C15-C01	120.6(3)
CI/-CoI-CI-PI	22.0 (3)	$C_2 = C_0 = C_1 $	94.6 (2)
	-56.8(3)		-81.4 (2)
C5—Co1—C1—P1	125.5 (3)		-37.5(2)
C3—Co1—C1—P1	-153.9 (3)	CI_CoI_CI5_CI6	56.5 (3)
C4—Co1—C1—P1	162.8 (2)	C3—Co1—C15—C16	138.3 (2)
C5-C1-C2-C3	0.2 (4)	C4—Co1—C15—C16	175.9 (2)
P1—C1—C2—C3	177.9 (2)	C14—Co1—C15—C16	-120.1(3)
Co1—C1—C2—C3	59.7 (2)	C16—Co1—C15—C14	120.1 (3)
C5—C1—C2—Co1	-59.6 (2)	C2—Co1—C15—C14	-145.4 (2)
P1C1C01	118.2 (2)	C18—Co1—C15—C14	38.66 (19)
C16—Co1—C2—C3	139.5 (2)	C17—Co1—C15—C14	82.5 (2)
C17—Co1—C2—C3	176.9 (2)	C1—Co1—C15—C14	176.6 (2)
C15—Co1—C2—C3	96.2 (2)	C3—Co1—C15—C14	-101.6 (2)
C5—Co1—C2—C3	-81.1 (2)	C4—Co1—C15—C14	-64.0 (3)
C1—Co1—C2—C3	-119.7 (3)	C14—C15—C16—C17	0.4 (4)
C4—Co1—C2—C3	-37.3 (2)	Co1-C15-C16-C17	59.8 (2)
C14—Co1—C2—C3	59.4 (3)	C14-C15-C16-Co1	-59.4 (2)
C16—Co1—C2—C1	-100.8 (2)	C2-Co1-C16-C17	139.3 (2)
C17—Co1—C2—C1	-63.4 (3)	C18—Co1—C16—C17	-37.6 (2)
C15—Co1—C2—C1	-144.14 (19)	C15—Co1—C16—C17	-119.3 (3)
C5—Co1—C2—C1	38.55 (19)	C5—Co1—C16—C17	59.2 (3)

$C_{3}-C_{0}1-C_{2}-C_{1}$	1197(3)	C1 - C01 - C16 - C17	95.0(2)
$C_1 C_2 C_1$	82 4 (2)	$C_1 = C_1 C_1 C_1 C_1 C_1 C_1 C_1 C_1 C_1 C_1$	176.8(2)
$C_1 = C_1 = C_2 = C_1$	170.00(10)	$C_{14}$ $C_{01}$ $C_{16}$ $C_{17}$	-81.8(2)
$C_1 = C_2 = C_1$	179.09(19)	$C^2$ $C^{-1}$ $C^{-16}$ $C^{-15}$	-1015(2)
$C_1 = C_2 = C_3 = C_4$	0.0(4)	$C_2 = C_0 = C_1 $	-101.3(2)
C01 - C2 - C3 - C4	59.4 (2)	C13 - C01 - C10 - C13	81.7(2)
CI = C2 = C3 = C01	-59.4 (2)		119.3 (3)
C16-C01-C3-C4	1/8.5 (2)	$C_{5}$ — $C_{0}$ ]— $C_{16}$ — $C_{15}$	1/8.5 (2)
C2—Co1—C3—C4	-119.6 (3)	CI_CoI_CI6_CI5	-145.7 (2)
C18—Co1—C3—C4	59.2 (3)	C3—Co1—C16—C15	-63.9 (3)
C15—Co1—C3—C4	140.0 (2)	C14—Co1—C16—C15	37.4 (2)
C5—Co1—C3—C4	-37.5 (2)	C15—C16—C17—C18	-0.6 (4)
C1—Co1—C3—C4	-81.7 (2)	Co1-C16-C17-C18	59.2 (2)
C14—Co1—C3—C4	95.9 (2)	C15-C16-C17-Co1	-59.8 (2)
C16—Co1—C3—C2	-61.9 (3)	C2-Co1-C17-C16	-62.0(3)
C18—Co1—C3—C2	178.8 (2)	C18—Co1—C17—C16	119.4 (3)
C15—Co1—C3—C2	-100.4(2)	C15—Co1—C17—C16	37.6 (2)
C5—Co1—C3—C2	82.1 (2)	C5-Co1-C17-C16	-144.8(2)
C1—Co1—C3—C2	37.9 (2)	C1—Co1—C17—C16	-100.7(2)
C4—Co1—C3—C2	119.6 (3)	C4—Co1—C17—C16	178.7 (2)
$C_{14} - C_{01} - C_{3} - C_{2}$	-1445(2)	$C_{14} - C_{01} - C_{17} - C_{16}$	81.8 (2)
$C_{2} - C_{3} - C_{4} - C_{5}$	-0.2(4)	$C_{16} - C_{01} - C_{17} - C_{18}$	-1194(3)
$C_{01} - C_{3} - C_{4} - C_{5}$	58 5 (2)	$C^{2}$ $C^{1}$ $C^{17}$ $C^{18}$	178.6(2)
$C^{2}-C^{3}-C^{4}-C^{1}$	-58.7(2)	$C_{15}$ $C_{01}$ $C_{17}$ $C_{18}$	-81.8(2)
$C_2 = C_3 = C_4 = C_0^2$	37.6(2)	$C_{13} = C_{11} = C_{17} = C_{18}$	05.8(2)
$C_2 = C_0 = C_4 = C_3$	57.0(2) -145.5(2)	$C_{3}$ $C_{01}$ $C_{17}$ $C_{18}$	33.8(2)
$C_{10} = C_{01} = C_{4} = C_{3}$	-143.3(2)	C1 = C01 = C17 = C18	139.8(2)
C1/-C01-C4-C3	1/0.7(2)	C4 - C01 - C17 - C18	59.5 (3)
C15-C01-C4-C3	-62.0(3)	C14 - C01 - C17 - C18	-3/./(2)
$C_{5}$ — $C_{0}$ ]— $C_{4}$ — $C_{3}$	119.7 (3)	C16—C17—C18—C14	0.6 (4)
CI-CoI-C4-C3	82.1 (2)	Col—C17—C18—C14	59.7 (2)
C14—Co1—C4—C3	-101.0 (2)	C16—C17—C18—Co1	-59.1 (2)
C2—Co1—C4—C5	-82.2 (2)	C15—C14—C18—C17	-0.4(4)
C18—Co1—C4—C5	94.8 (2)	P2-C14-C18-C17	-179.9 (2)
C17—Co1—C4—C5	57.0 (3)	Co1-C14-C18-C17	-59.4 (2)
C15—Co1—C4—C5	178.3 (2)	C15-C14-C18-Co1	59.0 (2)
C1—Co1—C4—C5	-37.6 (2)	P2-C14-C18-Co1	-120.5 (2)
C3—Co1—C4—C5	-119.7 (3)	C16—Co1—C18—C17	37.4 (2)
C14—Co1—C4—C5	139.2 (2)	C15—Co1—C18—C17	81.2 (2)
C3—C4—C5—C1	0.3 (4)	C5-Co1-C18-C17	-101.6(2)
Co1—C4—C5—C1	59.1 (2)	C1—Co1—C18—C17	-61.4(3)
C3—C4—C5—Co1	-58.8 (2)	C3—Co1—C18—C17	176.8 (3)
C2—C1—C5—C4	-0.3(4)	C4—Co1—C18—C17	-145.6(2)
P1-C1-C5-C4	-177.8(2)	$C_{14} - C_{01} - C_{18} - C_{17}$	1197(3)
$C_01 - C_1 - C_5 - C_4$	-59 5 (2)	$C_{16} - C_{01} - C_{18} - C_{14}$	-823(2)
$C_{2}$ $C_{1}$ $C_{5}$ $C_{01}$	59 2 (2)	C17 - C01 - C18 - C14	-1197(3)
P1 - C1 - C5 - Co1	-1183(3)	$C_{15}$ $C_{01}$ $C_{18}$ $C_{14}$	-38.56(10)
$C_{16} C_{01} C_{5} C_{4}$	110.3(3) 1759(2)	$C_{13} = C_{13} = C_{10} = C_{14}$	129 70 (19)
$C_{10} - C_{01} - C_{3} - C_{4}$	1/3.0(2)	$C_{1} = C_{1} = C_{10} = C_{14}$	130.70(19)
$C_2 = C_0 = C_3 = C_4$	01.1(2)	$C_1 = C_0 = C_1 $	1/0.02 (18)
C18 - C01 - C5 - C4	-103.0(2)	C3—C01—C18—C14	57.0(3)

C17—Co1—C5—C4	-146.9 (2)	C4-Co1-C18-C14	94.6 (2)
C1—Co1—C5—C4	119.9 (3)	P2-C19-C20-C21	61.7 (5)
C3—Co1—C5—C4	37.2 (2)	P2-C19-C20-C22	-174.4 (3)
C14—Co1—C5—C4	-63.5 (3)	P2-C23-C24-C25	61.3 (5)
C16—Co1—C5—C1	56.0 (3)	P2-C23-C24-C26	-173.6 (3)
C2—Co1—C5—C1	-38.82 (19)	C5-C1-P1-C6	4.9 (3)
C18—Co1—C5—C1	137.2 (2)	C2-C1-P1-C6	-172.2 (3)
C17—Co1—C5—C1	93.2 (2)	Co1—C1—P1—C6	-86.4 (2)
C3—Co1—C5—C1	-82.7 (2)	C5-C1-P1-C10	-97.0 (3)
C4—Co1—C5—C1	-119.9 (3)	C2-C1-P1-C10	85.8 (3)
C14—Co1—C5—C1	176.62 (19)	Co1—C1—P1—C10	171.7 (2)
P1-C6-C7-C8	-67.0 (5)	C7—C6—P1—C1	171.4 (3)
P1-C6-C7-C9	171.0 (3)	C7—C6—P1—C10	-87.7 (3)
P1-C10-C11-C13	-59.7 (5)	C11-C10-P1-C1	-70.1 (3)
P1-C10-C11-C12	176.3 (3)	C11—C10—P1—C6	-173.2 (3)
C16—Co1—C14—C15	-37.1 (2)	C15—C14—P2—C23	-0.1 (3)
C2—Co1—C14—C15	57.9 (3)	C18—C14—P2—C23	179.4 (3)
C18—Co1—C14—C15	-117.8 (3)	Co1-C14-P2-C23	92.0 (2)
C17—Co1—C14—C15	-80.5 (2)	C15-C14-P2-C19	100.6 (3)
C5—Co1—C14—C15	177.6 (2)	C18—C14—P2—C19	-79.9 (3)
C3—Co1—C14—C15	95.4 (2)	Co1-C14-P2-C19	-167.2 (2)
C4—Co1—C14—C15	139.0 (2)	C24—C23—P2—C14	179.3 (3)
C16—Co1—C14—C18	80.7 (2)	C24—C23—P2—C19	78.8 (3)
C2-Co1-C14-C18	175.7 (2)	C20—C19—P2—C14	81.0 (3)
C17—Co1—C14—C18	37.3 (2)	C20—C19—P2—C23	-178.3 (3)

# Hydrogen-bond geometry (Å, °)

D—H···A	D—H	H…A	D···A	D—H···A
C3—H3…F5 <sup>i</sup>	0.98	2.44	3.237 (5)	138
C15— $H15$ ···F4 <sup>i</sup>	0.98	2.39	3.278 (4)	150
C17—H17…F2	0.98	2.51	3.188 (5)	126
C18—H18…F6	0.98	2.41	3.305 (4)	152
C19—H19 <i>B</i> …F2 <sup>ii</sup>	0.97	2.54	3.494 (4)	167

Symmetry codes: (i) *x*, *y*–1, *z*; (ii) –*x*+3/2, *y*–1/2, –*z*+1/2.