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(E)-3-(2-Chloro-3,3,3-trifluoroprop-1-enyl)-2,2-dimethyl-*N*,*N*-diphenylcyclopropanecarboxamide

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Key indicators: single-crystal X-ray study; T = 294 K; mean σ (C–C) = 0.003 Å; disorder in main residue; R factor = 0.041; wR factor = 0.119; data-to-parameter ratio = 14.7.

The title compound, $C_{21}H_{19}ClF_3NO$, was synthesized from 3-[(*E*)-2-chloro-3,3,3-trifluoroprop-1-enyl]-2,2-dimethylcyclopropanecarboxylic acid and diphenylamine. The propenyl and carboxamide substituents lie on the same side of the cyclopropane ring plane, with the two methyl substituents on either side of the plane. The phenyl rings of the carboxamide are inclined at an angle of 84.6 (3)° to one another. The F atoms are disordered over two positions; the site occupancy factors are *ca* 0.6 and 0.4.

Related literature

For the preparation of the title compound, see: Liu *et al.* (2006). For the insecticidal properties of related compounds, see: Punja (1981).



) ssMark

Experimental

Crystal data

C₂₁H₁₉ClF₃NO $M_r = 393.82$ Monoclinic, P_{2_1}/n a = 9.247 (6) Å b = 21.443 (14) Å c = 10.025 (7) Å $\beta = 99.068$ (11)°

Data collection

Bruker SMART CCD area-detector diffractometer Absorption correction: multi-scan (*SADABS*; Bruker, 1997) $T_{\rm min} = 0.951, T_{\rm max} = 0.960$

Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.042$ $wR(F^2) = 0.119$ S = 1.004030 reflections 274 parameters $V = 1963 (2) Å^{3}$ Z = 4 Mo K\alpha radiation $\mu = 0.23 \text{ mm}^{-1}$ T = 294 (2) K 0.22 \times 0.20 \times 0.18 mm

11179 measured reflections 4030 independent reflections 2379 reflections with $I > 2\sigma(I)$ $R_{\text{int}} = 0.034$

Data collection: *SMART* (Bruker, 1997); cell refinement: *SAINT* (Bruker, 1997); data reduction: *SAINT*; program(s) used to solve structure: *SHELXS97* (Sheldrick, 1997); program(s) used to refine structure: *SHELXL97* (Sheldrick, 1997); molecular graphics: *SHELXTL* (Bruker, 1997); software used to prepare material for publication: *SHELXTL*

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: SJ2421).

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supporting information

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(*E*)-3-(2-Chloro-3,3,3-trifluoroprop-1-enyl)-2,2-dimethyl-*N*,*N*-diphenylcyclo-propanecarboxamide

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S1. Comment

3-((*E*)-2-Chloro-3,3,3-trifluoroprop-1-enyl)-2,2-dimethyl cyclopropanecarboxylic acid is a very important intermediate in the preparation of tefluthrinan a useful insecticide controlling a wide range of soil insect pests in maize, sugar beet, and other crops (Punja, 1981). Diphenylamine is also a structure which has bioactivity. We reasoned that a structure containing both of these bioactive components may show enhanced insecticidal activity and prepared the title compound (I), whose structure is reported here Fig. 1.

The the propenyl and carboxamide substituents lie on the same side of the cyclopropane ring plane, with the two methyl substituents on either side of the plane. The benzene rings of the carboxamide are inclined at $95.4 (3)^{\circ}$ to one another. The crystal packing of (I) is shown in Fig. 2.

S2. Experimental

The title compound was prepared according to the method of Liu *et al.* (2006). The product was recrystallized from methanol and ethyl acetate (5:1, v/v) over 3 days at ambient temperature, giving colourless single crystals of (I).

S3. Refinement

H atoms were positioned geometrically with C—H = 0.93-0.98 Å and refined using riding model with $U_{iso}(H) = 1.2$ Ueq(carrier). The fluorine atoms of the trifluoromethyl group were disordered over two conformations. The occupancy factor for the major component refined to 0.56 (3).



Figure 1

The molecular structure of (I), drawn with 30% probability ellipsoids. H atoms are drawn as spheres of arbitrary radius.



Figure 2

The crystal structure of (I), viewed along the *a* axis.

(E)-3-(2-Chloro-3,3,3-trifluoroprop-1-enyl)-2,2-dimethyl-N,N- diphenylcyclopropanecarboxamide

Crystal data

C₂₁H₁₉ClF₃NO $M_r = 393.82$ Monoclinic, $P2_1/n$ Hall symbol: -P 2yn a = 9.247 (6) Å b = 21.443 (14) Å c = 10.025 (7) Å $\beta = 99.068$ (11)° V = 1963 (2) Å³ Z = 4

Data collection

Bruker SMART CCD area-detector diffractometer Radiation source: fine-focus sealed tube Graphite monochromator φ and ω scans Absorption correction: multi-scan (*SADABS*; Bruker, 1997) $T_{\min} = 0.951, T_{\max} = 0.960$

Refinement

Refinement on F^2 Least-squares matrix: full $R[F^2 > 2\sigma(F^2)] = 0.042$ $wR(F^2) = 0.119$ S = 1.004030 reflections F(000) = 816 $D_x = 1.333 \text{ Mg m}^{-3}$ Mo K\alpha radiation, $\lambda = 0.71073 \text{ Å}$ Cell parameters from 2995 reflections $\theta = 2.2-24.7^{\circ}$ $\mu = 0.23 \text{ mm}^{-1}$ T = 294 KPrism, colourles $0.22 \times 0.20 \times 0.18 \text{ mm}$

11179 measured reflections 4030 independent reflections 2379 reflections with $I > 2\sigma(I)$ $R_{int} = 0.034$ $\theta_{max} = 26.5^{\circ}, \theta_{min} = 1.9^{\circ}$ $h = -11 \rightarrow 10$ $k = -20 \rightarrow 26$ $l = -12 \rightarrow 11$

274 parameters60 restraintsPrimary atom site location: structure-invariant direct methodsSecondary atom site location: difference Fourier map

Hydrogen site location: inferred from	$w = 1/[\sigma^2(F_o^2) + (0.0477P)^2 + 0.4369P]$
neighbouring sites	where $P = (F_o^2 + 2F_c^2)/3$
H-atom parameters constrained	$(\Delta/\sigma)_{\rm max} = 0.001$
	$\Delta \rho_{\rm max} = 0.30 \text{ e} \text{ Å}^{-3}$
	$\Delta \rho_{\rm min} = -0.32 \text{ e} \text{ Å}^{-3}$

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes. **Refinement**. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	Occ. (<1)
Cl1	0.52632 (8)	0.07861 (4)	0.13621 (8)	0.0975 (3)	
F1	0.732 (2)	0.0017 (7)	0.0236 (16)	0.111 (4)	0.44 (3)
F2	0.9287 (12)	0.0254 (10)	0.1498 (12)	0.096 (3)	0.44 (3)
F3	0.823 (2)	0.0915 (7)	0.0041 (15)	0.122 (3)	0.44 (3)
F1′	0.7705 (16)	-0.0077 (4)	0.0400 (14)	0.103 (3)	0.56 (3)
F2′	0.9394 (7)	0.0532 (8)	0.1380 (10)	0.094 (2)	0.56 (3)
F3′	0.7669 (19)	0.0895 (6)	-0.0073 (10)	0.123 (3)	0.56 (3)
01	1.00435 (15)	0.11409 (7)	0.53022 (16)	0.0659 (4)	
N1	0.96418 (16)	0.19188 (7)	0.67253 (17)	0.0483 (4)	
C1	0.7965 (3)	0.04904 (14)	0.0946 (3)	0.0799 (8)	
C2	0.7085 (2)	0.06733 (10)	0.1994 (2)	0.0600 (6)	
C3	0.7634 (2)	0.07596 (10)	0.3275 (2)	0.0560 (5)	
H3	0.8630	0.0683	0.3528	0.067*	
C4	0.6825 (2)	0.09642 (9)	0.4335 (2)	0.0542 (5)	
H4	0.5822	0.1103	0.4003	0.065*	
C5	0.7013 (2)	0.06512 (9)	0.5698 (2)	0.0535 (5)	
C6	0.7573 (2)	0.13142 (9)	0.5584 (2)	0.0544 (5)	
H6	0.6969	0.1637	0.5914	0.065*	
C7	0.8048 (3)	0.01108 (11)	0.5998 (3)	0.0745 (7)	
H7A	0.7580	-0.0264	0.5624	0.112*	
H7B	0.8311	0.0065	0.6958	0.112*	
H7C	0.8913	0.0186	0.5605	0.112*	
C8	0.5658 (3)	0.06042 (12)	0.6365 (3)	0.0760 (7)	
H8A	0.5011	0.0945	0.6071	0.114*	
H8B	0.5935	0.0621	0.7328	0.114*	
H8C	0.5168	0.0217	0.6117	0.114*	
C9	0.9165 (2)	0.14478 (10)	0.5816 (2)	0.0522 (5)	
C10	1.1194 (2)	0.19815 (9)	0.7161 (2)	0.0473 (5)	
C11	1.2001 (2)	0.14777 (11)	0.7713 (2)	0.0565 (5)	
H11	1.1545	0.1098	0.7811	0.068*	

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (\hat{A}^2)

C12	1.3491 (3)	0.15412 (13)	0.8119 (2)	0.0683 (7)
H12	1.4040	0.1202	0.8489	0.082*
C13	1.4170 (3)	0.21036 (14)	0.7978 (3)	0.0739 (7)
H13	1.5177	0.2142	0.8236	0.089*
C14	1.3366 (3)	0.26020 (13)	0.7462 (3)	0.0740 (7)
H14	1.3822	0.2984	0.7387	0.089*
C15	1.1871 (2)	0.25455 (10)	0.7048 (2)	0.0621 (6)
H15	1.1326	0.2888	0.6693	0.074*
C16	0.8725 (2)	0.24001 (9)	0.7137 (2)	0.0444 (5)
C17	0.7857 (2)	0.27642 (9)	0.6197 (2)	0.0521 (5)
H17	0.7830	0.2689	0.5280	0.063*
C18	0.7031 (2)	0.32397 (10)	0.6614 (3)	0.0636 (6)
H18	0.6440	0.3480	0.5974	0.076*
C19	0.7068 (2)	0.33616 (11)	0.7943 (3)	0.0666 (7)
H19	0.6507	0.3684	0.8212	0.080*
C20	0.7929 (3)	0.30110 (12)	0.8887 (3)	0.0686 (7)
H20	0.7960	0.3098	0.9800	0.082*
C21	0.8759 (2)	0.25253 (11)	0.8494 (2)	0.0588 (6)
H21	0.9337	0.2284	0.9142	0.071*

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	U^{23}
Cl1	0.0740 (4)	0.1102 (6)	0.0929 (5)	0.0004 (4)	-0.0339 (4)	0.0028 (4)
F1	0.105 (6)	0.125 (6)	0.095 (4)	-0.004 (4)	-0.010 (4)	-0.058 (5)
F2	0.079 (3)	0.134 (7)	0.074 (3)	0.000 (4)	0.005 (3)	-0.020 (5)
F3	0.135 (7)	0.135 (5)	0.104 (5)	-0.029 (5)	0.041 (5)	0.025 (4)
F1′	0.103 (5)	0.094 (3)	0.112 (5)	-0.001 (3)	0.013 (4)	-0.025 (3)
F2′	0.081 (2)	0.128 (6)	0.076 (3)	-0.022 (3)	0.0197 (18)	-0.023 (4)
F3′	0.140 (7)	0.161 (5)	0.070 (3)	-0.007 (4)	0.021 (4)	0.033 (3)
01	0.0450 (8)	0.0741 (10)	0.0785 (11)	0.0020 (7)	0.0097 (7)	-0.0341 (9)
N1	0.0402 (8)	0.0436 (9)	0.0607 (10)	-0.0005 (7)	0.0063 (7)	-0.0123 (8)
C1	0.090 (2)	0.089 (2)	0.0554 (16)	-0.0193 (17)	-0.0049 (15)	-0.0049 (16)
C2	0.0611 (13)	0.0561 (13)	0.0569 (14)	-0.0085 (11)	-0.0086 (11)	0.0024 (11)
C3	0.0467 (11)	0.0594 (13)	0.0579 (14)	-0.0005 (10)	-0.0041 (10)	-0.0032 (11)
C4	0.0409 (10)	0.0512 (12)	0.0669 (14)	0.0016 (9)	-0.0023 (10)	-0.0055 (11)
C5	0.0501 (12)	0.0486 (12)	0.0617 (14)	-0.0026 (10)	0.0081 (10)	-0.0088 (11)
C6	0.0424 (11)	0.0460 (12)	0.0740 (15)	0.0006 (9)	0.0068 (10)	-0.0165 (10)
C7	0.0812 (17)	0.0595 (15)	0.0812 (17)	0.0102 (13)	0.0081 (13)	0.0081 (13)
C8	0.0708 (16)	0.0765 (17)	0.0849 (18)	-0.0165 (13)	0.0252 (13)	-0.0172 (14)
C9	0.0468 (11)	0.0495 (12)	0.0599 (13)	-0.0007 (10)	0.0071 (10)	-0.0109 (11)
C10	0.0410 (10)	0.0492 (12)	0.0520 (12)	0.0002 (9)	0.0080 (9)	-0.0095 (10)
C11	0.0550 (12)	0.0571 (13)	0.0557 (13)	0.0045 (11)	0.0039 (10)	-0.0044 (11)
C12	0.0585 (14)	0.0866 (18)	0.0575 (14)	0.0222 (13)	0.0017 (11)	-0.0091 (13)
C13	0.0442 (12)	0.102 (2)	0.0748 (17)	-0.0020 (14)	0.0063 (12)	-0.0263 (15)
C14	0.0519 (14)	0.0751 (17)	0.0971 (19)	-0.0140 (13)	0.0184 (13)	-0.0202 (15)
C15	0.0514 (12)	0.0518 (13)	0.0837 (16)	-0.0025 (10)	0.0128 (11)	-0.0073 (12)
C16	0.0417 (10)	0.0407 (11)	0.0521 (12)	-0.0068 (9)	0.0111 (9)	-0.0072 (9)

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C17	0.0576 (12)	0.0478 (12)	0.0521 (12)	0.0015 (10)	0.0120 (10)	0.0005 (10)
C18	0.0583 (13)	0.0469 (13)	0.0854 (18)	0.0058 (11)	0.0109 (12)	0.0011 (12)
C19	0.0548 (13)	0.0531 (14)	0.097 (2)	-0.0060 (11)	0.0264 (13)	-0.0219 (14)
C20	0.0665 (15)	0.0822 (17)	0.0622 (15)	-0.0136 (14)	0.0256 (12)	-0.0277 (13)
C21	0.0568 (13)	0.0690 (15)	0.0508 (13)	-0.0025 (11)	0.0087 (10)	-0.0044 (11)

Geometric parameters (Å, °)

Cl1—C2	1.721 (2)	C8—H8A	0.9600
F1—C1	1.324 (8)	C8—H8B	0.9600
F2—C1	1.357 (7)	C8—H8C	0.9600
F3—C1	1.334 (8)	C10—C15	1.375 (3)
F1′—C1	1.340 (7)	C10—C11	1.378 (3)
F2′—C1	1.328 (6)	C11—C12	1.381 (3)
F3′—C1	1.336 (7)	C11—H11	0.9300
O1—C9	1.221 (2)	C12—C13	1.377 (4)
N1—C9	1.385 (3)	C12—H12	0.9300
N1-C16	1.437 (2)	C13—C14	1.357 (4)
N1-C10	1.439 (2)	C13—H13	0.9300
C1—C2	1.480 (4)	C14—C15	1.385 (3)
C2—C3	1.317 (3)	C14—H14	0.9300
C3—C4	1.460 (3)	C15—H15	0.9300
С3—Н3	0.9300	C16—C17	1.380 (3)
C4—C5	1.508 (3)	C16—C21	1.382 (3)
C4—C6	1.529 (3)	C17—C18	1.378 (3)
C4—H4	0.9800	C17—H17	0.9300
С5—С7	1.502 (3)	C18—C19	1.353 (3)
C5—C8	1.514 (3)	C18—H18	0.9300
C5—C6	1.523 (3)	C19—C20	1.363 (3)
С6—С9	1.481 (3)	C19—H19	0.9300
С6—Н6	0.9800	C20—C21	1.387 (3)
C7—H7A	0.9600	C20—H20	0.9300
С7—Н7В	0.9600	C21—H21	0.9300
С7—Н7С	0.9600		
C9—N1—C16	124.86 (16)	C5—C8—H8A	109.5
C9—N1—C10	117.84 (16)	C5—C8—H8B	109.5
C16—N1—C10	116.81 (15)	H8A—C8—H8B	109.5
F1—C1—F3	105.7 (11)	C5—C8—H8C	109.5
F2'—C1—F3'	106.3 (6)	H8A—C8—H8C	109.5
F2'—C1—F1'	107.5 (6)	H8B—C8—H8C	109.5
F3'—C1—F1'	106.0 (8)	O1—C9—N1	120.42 (18)
F1—C1—F2	103.4 (8)	O1—C9—C6	122.70 (19)
F3—C1—F2	106.5 (7)	N1C9C6	116.76 (18)
F1—C1—C2	109.6 (8)	C15-C10-C11	119.9 (2)
F2′—C1—C2	112.3 (5)	C15—C10—N1	120.15 (18)
F3—C1—C2	118.7 (8)	C11—C10—N1	119.98 (18)
F3'—C1—C2	107.6 (7)	C10—C11—C12	119.6 (2)

F1′—C1—C2	116.6 (6)	C10-C11-H11	120.2
$F_{2} = C_{1} = C_{2}$	111.7 (6)	C12-C11-H11	120.2
C_{3} C_{2} C_{1}	1240(2)	C_{13} C_{12} C_{11}	120.2 120.4(2)
$C_3 C_2 C_1$	124.0(2) 122.0(2)	C_{13} C_{12} H_{12}	110.8
$C_1 = C_2 = C_1$	122.9(2) 113.06(17)	$C_{13} - C_{12} - H_{12}$	119.8
$C_1 = C_2 = C_1$	115.00(17) 126.0(2)	C14 $C12$ $C12$	119.8
$C_2 = C_3 = C_4$	120.0 (2)	C14 - C13 - C12	119.8 (2)
C2C3H3	117.0	С12—С13—Н13	120.1
C4 - C3 - H3	117.0	C12—C13—H13	120.1
$C_3 - C_4 - C_5$	121.75 (18)	C13 - C14 - C15	120.5 (2)
C3—C4—C6	121.70 (18)	C13—C14—H14	119.8
C5—C4—C6	60.22 (14)	C15—C14—H14	119.8
C3—C4—H4	114.2	C10—C15—C14	119.9 (2)
C5—C4—H4	114.2	C10—C15—H15	120.1
C6—C4—H4	114.2	C14—C15—H15	120.1
C7—C5—C4	120.27 (19)	C17—C16—C21	118.89 (19)
C7—C5—C8	113.9 (2)	C17—C16—N1	121.07 (18)
C4—C5—C8	116.37 (19)	C21—C16—N1	119.96 (18)
C7—C5—C6	121.44 (19)	C18—C17—C16	120.2 (2)
C4—C5—C6	60.57 (14)	C18—C17—H17	119.9
C8—C5—C6	114.21 (18)	C16—C17—H17	119.9
C9—C6—C5	120.64 (17)	C19—C18—C17	120.8 (2)
C9—C6—C4	122.29 (18)	C19—C18—H18	119.6
C5—C6—C4	59.21 (14)	C17—C18—H18	119.6
С9—С6—Н6	114.5	C18—C19—C20	119.9 (2)
C5—C6—H6	114 5	C18—C19—H19	120.0
C4—C6—H6	114 5	C20-C19-H19	120.0
$C_{2} = C_{2} = H_{2}$	109.5	C_{19} C_{20} C_{21} C_{21}	120.0 120.4(2)
C5-C7-H7B	109.5	C19 - C20 - H20	110.8
	109.5	$C_{21} C_{20} H_{20}$	110.8
$\Pi/A = C / = \Pi/B$	109.5	$C_{21} = C_{20} = 1120$	119.8 110.8(2)
	109.5	$C_{10} = C_{21} = C_{20}$	119.8 (2)
$\Pi/A - C - \Pi/C$	109.5	C10 - C21 - H21	120.1
H/B-C/H/C	109.5	C20—C21—H21	120.1
F1-C1-C2-C3	131.3 (10)	C16—N1—C9—C6	-19.7(3)
F2'-C1-C2-C3	-11.5(9)	C10 - N1 - C9 - C6	168.66 (18)
F_{3} C_{1} C_{2} C_{3}	-1072(10)	C5-C6-C9-01	47 4 (3)
$F_{3'} - C_{1} - C_{2} - C_{3}$	-1280(8)	C4-C6-C9-01	-233(3)
$F_1' = C_1 = C_2 = C_3$	113.2(8)	C_{5} C_{6} C_{9} N_{1}	-1285(2)
$F_2 = C_1 = C_2 = C_3$	113.2(0) 173(11)	$C_4 C_6 C_9 N_1$	120.3(2) 160 74 (10)
$F_1 = C_1 = C_2 = C_3$	-50.5(10)	C_{1} C_{1} C_{1} C_{1} C_{1}	100.74(17) 126.5(2)
$F_{1} = C_{1} = C_{2} = C_{11}$	166.7(9)	$C_{16} = N_{1} = C_{10} = C_{15}$	-45.8(2)
$F_2 = C_1 = C_2 = C_{11}$	700.7(0)	$C_{10} = N_{1} = C_{10} = C_{13}$	+3.0(3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(10)	$C_{1} = C_{1} = C_{1$	34.3(3)
$F_{3} = -C_{1} = -C_{2} = -C_{1}$	30.2(8)	C10 - N1 - C10 - C11	133.2(2)
$r_1 - c_1 - c_2 - c_1$	-08.0(8)	$CI_{3} - CI_{0} - CI_{1} - CI_{2}$	-1.5(3)
$F_2 = C_1 = C_2 = C_1$	-104.3(11)	NI - CI0 - CII - CI2	1/9.52 (19)
C1 - C2 - C3 - C4	1//.4 (2)	C10—C11—C12—C13	0.2 (3)
C11—C2—C3—C4	-0.7 (3)	C11—C12—C13—C14	1.3 (4)
C2-C3-C4-C5	134.6 (2)	C12—C13—C14—C15	-1.4(4)

C2—C3—C4—C6	-153.1 (2)	C11—C10—C15—C14	1.3 (3)
C3—C4—C5—C7	-0.4 (3)	N1-C10-C15-C14	-179.7 (2)
C6—C4—C5—C7	-111.4 (2)	C13—C14—C15—C10	0.2 (4)
C3—C4—C5—C8	-144.8 (2)	C9—N1—C16—C17	-53.0 (3)
C6—C4—C5—C8	104.2 (2)	C10-N1-C16-C17	118.7 (2)
C3—C4—C5—C6	111.0 (2)	C9—N1—C16—C21	130.3 (2)
C7—C5—C6—C9	-2.2 (3)	C10-N1-C16-C21	-58.1 (2)
C4—C5—C6—C9	-111.7 (2)	C21—C16—C17—C18	-0.6 (3)
C8—C5—C6—C9	140.5 (2)	N1-C16-C17-C18	-177.38 (17)
C7—C5—C6—C4	109.5 (2)	C16—C17—C18—C19	0.7 (3)
C8—C5—C6—C4	-107.8 (2)	C17—C18—C19—C20	-0.1 (3)
C3—C4—C6—C9	-2.1 (3)	C18—C19—C20—C21	-0.6 (3)
C5—C4—C6—C9	109.0 (2)	C17—C16—C21—C20	-0.1 (3)
C3—C4—C6—C5	-111.1 (2)	N1-C16-C21-C20	176.72 (18)
C16—N1—C9—O1	164.25 (19)	C19—C20—C21—C16	0.7 (3)
C10-N1-C9-O1	-7.4 (3)		