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### Tetraethyl 1,1'-(ethane-1,2-diyl)bis(2,5dimethyl-1*H*-pyrrole-3,4-dicarboxylate)

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Key indicators: single-crystal X-ray study; T = 298 K; mean  $\sigma$ (C–C) = 0.010 Å; R factor = 0.062; wR factor = 0.194; data-to-parameter ratio = 8.6.

The asymmetric unit of the title compound,  $C_{26}H_{36}N_2O_8$ , comprises two independent molecules. In each molecule, the two pyrrole rings are linked by a -CH2CH2- bridge, with dihedral angles between the two pyrrole rings of 14.5 (3) and 16.4  $(3)^{\circ}$  in the two molecules. Each pyrrole ring carries 2- and 5-methyl substituents and ethoxycarbonyl groups at the 3- and 5-positions.

#### **Related literature**

For background to the biological applications of bispyrrole and its derivatives, see: Dairi et al. (2006); Bordner & Rapoport (1965); Rapoport & Castagnoli (1962). For the synthesis and biological properties of pyrrole derivatives containing Nsubstituent groups, see: Banik et al. (2004); Sagyam et al. (2007). For details of the the Paal-Knorr condensation reaction, see Amarnath et al. (1991). For representative bondlength data, see: Allen et al. (1987).



#### **Experimental**

#### Crystal data

C <sub>26</sub> H <sub>36</sub> N <sub>2</sub> O <sub>8</sub>	
$M_r = 504.57$	
Monoclinic, Pc	
a = 12.891 (3) Å	
<i>b</i> = 13.743 (3) Å	
c = 16.717 (3) Å	
$\beta = 113.350 \ (14)^{\circ}$	

#### Data collection

Bruker SMART 1000 CCD diffractometer Absorption correction: multi-scan (SADABS; Bruker, 2001)  $T_{\min} = 0.982, T_{\max} = 0.985$ 

#### Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.062$ wR(F<sup>2</sup>) = 0.194 S = 0.995726 reflections 663 parameters

 $V = 2719.0 (10) \text{ Å}^3$ Z = 4Mo  $K\alpha$  radiation  $\mu = 0.09 \text{ mm}^-$ T = 298 K $0.20 \times 0.18 \times 0.17~\mathrm{mm}$ 

5726 measured reflections 5726 independent reflections 3020 reflections with  $I > 2\sigma(I)$  $R_{\rm int} = 0.000$ 

2 restraints H-atom parameters constrained  $\Delta \rho_{\rm max} = 0.29 \text{ e} \text{ Å}^{-3}$  $\Delta \rho_{\rm min} = -0.18 \text{ e} \text{ Å}^{-3}$ 

Data collection: SMART (Bruker, 2007); cell refinement: SAINT (Bruker, 2007); data reduction: SAINT; program(s) used to solve structure: SHELXTL (Sheldrick, 2008): program(s) used to refine structure: SHELXTL; molecular graphics: SHELXTL; software used to prepare material for publication: SHELXTL.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: SJ5043).

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Tetraethyl 1,1'-(ethane-1,2-diyl)bis(2,5-dimethyl-1*H*-pyrrole-3,4-dicarboxylate)

### Shi-Fan Wang, Chao Li and Shuai Chen

#### S1. Comment

Bis-pyrrole and its derivatives play important roles in some bioactive pyrrole natural products, (Dairi *et al.*, 2006; Bordner & Rapoport, 1965; Rapoport & Castagnoli, 1962). Recently, the synthesis of pyrrole derivatives with Nsubstituent groups aroused great interest because of their significant biological activity (Banik *et al.*, 2004; Sagyam *et al.*, 2007). As an intermediate for further synthesis of pyrrole derivatives containing N-substituent groups, we have prepared the title compound by the Paal-Knorr condensation reaction (Amarnath *et al.*, 1991) and obtained its structure is reported here.

In the asymmetric unit of the title compound, Fig. 1, there are two independent molecules, A and B. The dihedral angle between the two pyrrole rings in one molecule is  $14.5 (3)^\circ$ , and that in the other molecule is  $16.4 (3)^\circ$ . All the bond lengths are within normal ranges (Allen *et al.*, 1987).

#### **S2. Experimental**

12.8 ml of ethyl acetoacetate (0.10 mol) and 2.28 g (0.10 mol) of sodium metal were added into 300 ml dry ether under stirring at room temperature. Then, the mixed solution was refluxed for 24 h till the Na was depleted. 100 ml dry ether solution contained 12.5 g (0.050 mol)  $I_2$  was added dropwise. After all of the iodine solution had been added, the reaction mixture was refluxed for 12 h and then cooled to room temperature. The undissolved solid was filtered and the ether solution was evaporated to yield diacetyl butanedioic acid diethyl ester as a gray solid (8.64 g, 67%). 5.20 g (20 mmol) of diacetyl butanedioic acid diethyl ester as a gray solid (8.64 g, 67%). 5.20 g (20 mmol) of ethanol and acetic acid ( $\nu/\nu$ , 5:1). The mixture was then refluxed for 6 h and evaporated to remove the ethanol. The residue was poured into water to give the title compound as a white solid (4.91 g, 97%). A little of the solid was dissolved in mixed solvent of acetone-water ( $\nu/\nu$ , 20:1). After standing in air over a period of about five days, the acetone is evaporated, colourless crystals suitable for X-ray diffraction analysis were formed at the bottom of the vessel.

#### **S3. Refinement**

H atoms were positioned geometrically and refined using the riding-model approximation, with C–H = 0.93–0.97 Å, and  $U_{iso}(H) = 1.2U_{eq}(C)$  or  $U_{iso}(H) = 1.5U_{eq}(methyl C)$ . In the absence of significant anomalous dispersion effects, Friedel pairs were averaged. Displacement parameters on some of the atoms particularly of the ethyl groups of the ethylcarboxylate substituents were unusually large. However, a suitable disorder model could not be found for them.



### Figure 1

The structure of molecule A of the title compound with atom labels and 30% probability displacement ellipsoids for non-H atoms.



### Figure 2

The structure of molecule B of the title compound with atom labels and 30% probability displacement ellipsoids for non-H atoms.

Tetraethyl 1,1'-(ethane-1,2-diyl)bis(2,5-dimethyl-1*H*-pyrrole-3,4-dicarboxylate)

Crystal data	
$C_{26}H_{36}N_2O_8$	F(000) = 1080
$M_r = 504.57$	$D_{\rm x} = 1.233 {\rm ~Mg} {\rm ~m}^{-3}$
Monoclinic, Pc	Mo <i>K</i> $\alpha$ radiation, $\lambda = 0.71073$ Å
Hall symbol: P -2yc	Cell parameters from 2429 reflections
a = 12.891 (3) Å	$\theta = 2.5 - 24.5^{\circ}$
b = 13.743 (3) Å	$\mu = 0.09 \text{ mm}^{-1}$
c = 16.717 (3)  Å	T = 298  K
$\beta = 113.350 \ (14)^{\circ}$	Block, colourless
$V = 2719.0 (10) \text{ Å}^3$	$0.20 \times 0.18 \times 0.17 \text{ mm}$
Z = 4	

Data collection

Bruker SMART 1000 CCD diffractometer Radiation source: fine-focus sealed tube Graphite monochromator $\omega$ scans Absorption correction: multi-scan ( <i>SADABS</i> ; Bruker, 2001) $T_{min} = 0.982, T_{max} = 0.985$ <i>Padinament</i>	5726 measured reflections 5726 independent reflections 3020 reflections with $I > 2\sigma(I)$ $R_{int} = 0.000$ $\theta_{max} = 27.0^{\circ}, \theta_{min} = 1.5^{\circ}$ $h = -16 \rightarrow 15$ $k = 0 \rightarrow 17$ $l = 0 \rightarrow 21$
Refinement $\Sigma^2$	
Least-squares matrix: full $R[F^2 > 2\sigma(F^2)] = 0.062$ $wR(F^2) = 0.194$ S = 0.99 5726 reflections 663 parameters 2 restraints	map Hydrogen site location: inferred from neighbouring sites H-atom parameters constrained $w = 1/[\sigma^2(F_o^2) + (0.1027P)^2]$ where $P = (F_o^2 + 2F_c^2)/3$ $(\Delta/\sigma)_{max} = 0.001$
Primary atom site location: structure-invariant direct methods	$\Delta \rho_{\rm max} = 0.29 \text{ e } \text{\AA}^{-3}$ $\Delta \rho_{\rm min} = -0.18 \text{ e } \text{\AA}^{-3}$

#### Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes. **Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$ 

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(Å^2)$ 

are statistically about twice as large as those based on F, and R- factors based on ALL data will be even larger.

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	
01	0.6385 (7)	0.3819 (5)	0.1367 (4)	0.133 (3)	
O2	0.6668 (5)	0.4974 (4)	0.2316 (3)	0.0819 (15)	
03	0.7288 (7)	0.4428 (7)	0.4836 (4)	0.173 (5)	
O4	0.8112 (5)	0.4230 (4)	0.3945 (3)	0.0933 (16)	
05	0.0805 (4)	-0.1379 (4)	0.0950 (3)	0.0823 (15)	
O6	0.1269 (4)	-0.2452 (3)	0.2036 (3)	0.0707 (13)	
O7	0.3049 (4)	-0.2263 (4)	0.4369 (3)	0.0765 (14)	
08	0.1351 (3)	-0.1624 (3)	0.3687 (3)	0.0678 (12)	
N1	0.4959 (5)	0.2503 (4)	0.3016 (3)	0.0456 (13)	
N2	0.3699 (5)	0.0020 (4)	0.2865 (3)	0.0449 (13)	
C1	0.5129 (6)	0.2823 (5)	0.2310 (4)	0.0522 (17)	
C2	0.5991 (6)	0.3500 (5)	0.2616 (4)	0.0565 (19)	
C3	0.6301 (6)	0.3564 (5)	0.3544 (4)	0.0519 (17)	
C4	0.5637 (5)	0.2912 (5)	0.3764 (4)	0.0505 (17)	
C5	0.4492 (7)	0.2512 (6)	0.1411 (4)	0.075 (2)	
H5A	0.4740	0.1876	0.1326	0.112*	

H5B	0.4618	0.2964	0.1020	0.112*
H5C	0.3701	0.2493	0.1295	0.112*
C6	0.5673 (7)	0.2669 (6)	0.4622 (5)	0.078 (2)
H6A	0.6291	0.3005	0.5060	0.117*
H6B	0.5774	0.1980	0.4714	0.117*
H6C	0.4977	0.2861	0.4658	0.117*
C7	0.7231 (7)	0.4142 (7)	0.4190 (6)	0.077 (3)
C8	0.9070 (9)	0.4896 (9)	0.4463 (6)	0.130 (4)
H8A	0.8798	0.5560	0.4420	0.156*
H8B	0.9374	0.4707	0.5072	0.156*
C9	0.9903 (9)	0.4839 (11)	0.4143 (11)	0.196 (7)
H9A	1.0497	0.5290	0.4451	0.294*
H9B	0.9590	0.4998	0.3534	0.294*
H9C	1.0203	0.4191	0.4221	0.294*
C10	0.6377 (7)	0.4101 (6)	0.2051 (5)	0.065(2)
C11	0.7157 (8)	0.5562 (7)	0.1838 (5)	0.103 (3)
H11A	0.7847	0.5262	0.1856	0.124*
H11B	0.6633	0.5614	0.1234	0.124*
C12	0.7393 (9)	0.6497 (7)	0.2222 (8)	0.126 (4)
H12A	0.6773	0.6926	0.1919	0.189*
H12B	0.8068	0.6747	0.2185	0.189*
H12C	0.7499	0.6454	0.2823	0.189*
C13	0.4084 (5)	0.1770 (4)	0.2939 (4)	0.0460 (16)
H13A	0.3417	0.1892	0.2414	0.055*
H13B	0.3874	0.1826	0.3434	0.055*
C14	0.4509 (5)	0.0752 (5)	0.2907 (4)	0.0518 (18)
H14A	0.4695	0.0694	0.2400	0.062*
H14B	0.5196	0.0644	0.3420	0.062*
C15	0.3637(5)	-0.0487(5)	0.3554(4)	0.0467(16)
C16	0.2756 (5)	-0.1119(4)	0.3244 (3)	0.0388 (14)
C17	0.2231 (5)	-0.0999(5)	0.2330(4)	0.0431 (16)
C18	0.2818(5)	-0.0299(5)	0.2104(4)	0.0443 (16)
C19	0.2710(7)	0.0107 (6)	0.1232(4)	0.071 (2)
H19A	0.2518	0.0785	0.1201	0.106*
H19B	0.2127	-0.0238	0.0772	0.106*
H19C	0.3414	0.0031	0.1170	0.106*
C20	0.4437 (6)	-0.0241(6)	0.4472 (4)	0.063(2)
H20A	0.4261	-0.0633	0.4877	0.094*
H20B	0.4360	0.0434	0.4585	0.094*
H20C	0.5200	-0.0368	0.4539	0.094*
C21	0 2419 (6)	-0.1726(5)	0 3819 (4)	0.0485 (16)
C22	0.0935(7)	-0.2215(6)	0.4220 (6)	0.089 (2)
H22A	0.0929	-0.2895	0.4063	0.107*
H22B	0.1432	-0.2144	0.4830	0.107*
C23	-0.0193(8)	-0.1911 (9)	0.4089 (8)	0.152(5)
H23A	-0.0162	-0.1285	0.4352	0.228*
H23B	-0.0517	-0.2376	0.4351	0.228*
H23C	-0.0649	-0.1870	0.3476	0.228*
	0.0012	0.10/0	0.01/0	0.220

C24	0.1352 (6)	-0.1593 (5)	0.1703 (4)	0.0509 (18)
C25	0.0423 (7)	-0.3109 (6)	0.1489 (6)	0.098 (3)
H25A	0.0602	-0.3318	0.1005	0.117*
H25B	-0.0310	-0.2794	0.1259	0.117*
C26	0.0408 (9)	-0.3958 (7)	0.2035 (7)	0.127 (4)
H26A	0.1167	-0.4177	0.2358	0.191*
H26B	-0.0026	-0.4474	0.1668	0.191*
H26C	0.0072	-0.3770	0.2432	0.191*
09	0.5561 (4)	0.9699 (4)	0.1424 (3)	0.0949 (18)
O10	0.7295 (4)	0.9161 (3)	0.2169 (3)	0.0663 (12)
011	0.7871 (4)	0.8930 (4)	0.4889 (3)	0.0920 (17)
012	0.7420 (4)	0.9967 (3)	0.3800 (3)	0.0659 (12)
013	0.1588 (5)	0.2854 (4)	0.1302 (3)	0.0999 (18)
014	0.0572 (4)	0.3395 (4)	0.2025 (3)	0.0784 (14)
015	0.2457 (5)	0.3679 (4)	0.4697 (3)	0.0921 (17)
016	0.2027 (4)	0.2573 (3)	0.3677 (3)	0.0643 (12)
N3	0.4994 (4)	0.7494 (4)	0.3027(3)	0.0445 (13)
N4	0.3782 (5)	0.5013 (4)	0.2989(3)	0.0490 (14)
C27	0.5838(5)	0.7816 (5)	0.3766(4)	0.0465 (17)
C28	0.6412(5)	0.8515(5)	0.3522(4)	0.0469(17)
C29	0.5865(5)	0.8617(5)	0.2585(4)	0.0467 (15)
C30	0.4989(5)	0 7976 (5)	0 2309 (4)	0.0466 (15)
C31	0.4202 (6)	0.7749(5)	0.2309(1) 0.1407(4)	0.0597(19)
H31A	0.4222	0.7064	0.1303	0.090*
H31B	0.4425	0.8102	0.1005	0.090*
H31C	0.3450	0.7935	0.1326	0.090*
C32	0.6010 (6)	0.7457(5)	0.1520 0.4635(4)	0.090
H32A	0.6363	0.6829	0.4035 (4)	0.005*
H32R	0.5294	0.7406	0.4683	0.095*
H32C	0.6487	0.7902	0.4065	0.095*
C33	0.6200 (6)	0.9234 (6)	0.3000	0.0550 (18)
C34	0.0200 (0)	0.9254 (0)	0.2012(4) 0.1622(5)	0.0500(10)
С34 Н344	0.7673 (0)	1.0438	0.1022 (5)	0.000 (2)
1134A 1124D	0.7304	0.0500	0.1/10	0.103*
C35	0.7243 0.8860 (7)	0.9555 (8)	0.1015	0.103
СЭЭ Н35л	0.03800 (7)	0.9555 (8)	0.1858 (0)	0.17(5)
H35R	0.9284	0.9708	0.2445	0.176*
H35D H35C	0.9110	0.9895	0.1409	0.176*
C36	0.8907 0.7301 (5)	0.0000	0.1317 0.4137(4)	$0.170^{\circ}$
C30	0.7301(3)	1.0645(6)	0.4137(4) 0.4232(5)	0.0339(19)
U27A	0.8280 (7)	1.0043 (0)	0.4332 (3)	0.097 (3)
П3/А Ц27D	0.0177	1.0789	0.4601	0.110*
П3/Д	0.9023	1.0549	0.4495	0.110
U30	0.8238 (8)	1.1300 (0)	0.38/3 (8)	0.129 (4)
проч	0.0//0	1.1901	0.4248	0.193*
H39R	0./493	1.1//8	0.3085	0.193*
H38C	0.8410	1.13/0	0.3377	0.193*
C39	0.4157 (5)	0.6754 (4)	0.3000 (4)	0.0459 (16)
H39A	0.3479	0.6841	0.2474	0.055*

H39B	0.3955	0.6843	0.3495	0.055*
C40	0.4601 (6)	0.5742 (5)	0.3016 (4)	0.0532 (19)
H40A	0.4803	0.5655	0.2520	0.064*
H40B	0.5278	0.5656	0.3541	0.064*
C41	0.3053 (6)	0.4518 (5)	0.2249 (4)	0.0477 (16)
C42	0.2423 (5)	0.3905 (5)	0.2500 (4)	0.0458 (16)
C43	0.2723 (5)	0.4021 (4)	0.3397 (4)	0.0422 (15)
C44	0.3576 (5)	0.4694 (4)	0.3699 (3)	0.0446 (16)
C45	0.3057 (7)	0.4778 (6)	0.1375 (4)	0.068 (2)
H45A	0.2878	0.5455	0.1258	0.103*
H45B	0.2504	0.4392	0.0930	0.103*
H45C	0.3791	0.4652	0.1378	0.103*
C46	0.4253 (6)	0.5073 (5)	0.4589 (4)	0.0613 (19)
H46A	0.4093	0.4697	0.5010	0.092*
H46B	0.4060	0.5742	0.4624	0.092*
H46C	0.5043	0.5026	0.4705	0.092*
C47	0.1503 (7)	0.3337 (6)	0.1879 (4)	0.062 (2)
C48	-0.0347 (8)	0.2802 (9)	0.1476 (6)	0.123 (4)
H48A	-0.0690	0.3093	0.0902	0.148*
H48B	-0.0069	0.2162	0.1415	0.148*
C49	-0.1135 (10)	0.2716 (11)	0.1827 (9)	0.194 (7)
H49A	-0.0957	0.3158	0.2308	0.291*
H49B	-0.1135	0.2062	0.2028	0.291*
H49C	-0.1869	0.2869	0.1392	0.291*
C50	0.2382 (6)	0.3448 (5)	0.3992 (4)	0.0548 (18)
C51	0.1578 (7)	0.1949 (6)	0.4156 (5)	0.089 (2)
H51A	0.2116	0.1905	0.4757	0.106*
H51B	0.0886	0.2231	0.4154	0.106*
C52	0.1351 (8)	0.1011 (6)	0.3792 (6)	0.099 (3)
H52A	0.0690	0.1030	0.3257	0.148*
H52B	0.1224	0.0575	0.4192	0.148*
H52C	0.1984	0.0787	0.3677	0.148*

Atomic displacement parameters  $(Å^2)$ 

	$U^{11}$	<i>U</i> <sup>22</sup>	$U^{33}$	$U^{12}$	$U^{13}$	U <sup>23</sup>
01	0.213 (8)	0.129 (5)	0.093 (4)	-0.075 (5)	0.100 (5)	-0.036 (4)
O2	0.117 (4)	0.063 (3)	0.089 (3)	-0.018 (3)	0.067 (3)	-0.002 (3)
03	0.164 (7)	0.287 (11)	0.093 (4)	-0.142 (7)	0.079 (5)	-0.110 (6)
O4	0.076 (3)	0.111 (4)	0.080 (3)	-0.031 (3)	0.016 (3)	-0.005 (3)
05	0.075 (3)	0.097 (4)	0.052 (3)	-0.018 (3)	0.001 (2)	0.001 (2)
06	0.069 (3)	0.050 (3)	0.075 (3)	-0.019 (2)	0.009 (2)	0.002 (2)
O7	0.071 (3)	0.097 (4)	0.066 (3)	0.014 (3)	0.031 (2)	0.035 (3)
08	0.050 (3)	0.079 (3)	0.082 (3)	0.005 (2)	0.034 (2)	0.031 (2)
N1	0.055 (3)	0.034 (3)	0.052 (3)	-0.007 (3)	0.026 (3)	-0.003 (2)
N2	0.048 (3)	0.049 (3)	0.036 (3)	-0.010 (3)	0.015 (2)	-0.006 (2)
C1	0.058 (4)	0.052 (4)	0.050 (4)	-0.006 (4)	0.025 (3)	-0.006 (3)
C2	0.063 (4)	0.061 (5)	0.058 (4)	-0.002 (4)	0.037 (3)	-0.001 (3)

C3	0.051 (4)	0.061 (4)	0.042 (3)	-0.002 (4)	0.017 (3)	-0.014 (3)
C4	0.048 (4)	0.061 (4)	0.049 (4)	-0.006 (3)	0.026 (3)	-0.003(3)
C5	0.086 (5)	0.086 (5)	0.046 (4)	-0.027 (4)	0.020 (3)	-0.009 (4)
C6	0.101 (6)	0.083 (5)	0.058 (4)	-0.022(5)	0.039 (4)	-0.006 (4)
C7	0.059 (5)	0.106 (8)	0.066 (5)	-0.016 (5)	0.024 (4)	-0.019 (5)
C8	0.089 (7)	0.171 (11)	0.097 (6)	-0.036(7)	0.004 (5)	0.006 (7)
C9	0.076 (7)	0.241 (17)	0.268 (18)	-0.045 (8)	0.064 (10)	0.011 (13)
C10	0.076 (5)	0.072 (6)	0.054 (4)	-0.020(4)	0.034 (4)	-0.003(4)
C11	0.143 (7)	0.101(7)	0.085 (5)	-0.062(6)	0.065 (5)	0.003 (5)
C12	0.132 (8)	0.086 (7)	0.193 (11)	-0.014(6)	0.099 (8)	0.028(7)
C13	0.051(4)	0.034(4)	0.055 (4)	-0.001(3)	0.024(3)	-0.007(3)
C14	0.031(1) 0.048(4)	0.051(1) 0.061(5)	0.033(1) 0.048(4)	-0.012(4)	0.021(3)	-0.007(3)
C15	0.041(3)	0.001(3) 0.048(4)	0.046(3)	-0.002(3)	0.021(3)	-0.002(3)
C16	0.045(3)	0.030(3)	0.010(3)	-0.002(3)	0.012(3)	-0.003(3)
C17	0.041(3)	0.030(3) 0.040(4)	0.030(3) 0.045(3)	0.000(3)	0.012(3)	0.005(5)
C18	0.041(3)	0.040(4) 0.049(4)	0.049(3)	-0.004(3)	0.014(3)	-0.003(3)
C10	0.041(5)	0.049(4)	0.038(3)	-0.024(4)	0.011(3)	-0.003(3)
$C_{19}$	0.064(3)	0.033(5)	0.041(3)	-0.024(4)	0.021(3)	-0.003(3)
C20	0.004(4)	0.074(3)	0.040(3)	-0.003(4)	0.009(3)	0.003(3)
C21	0.030(4)	0.044(4)	0.047(3)	-0.003(3)	0.014(3)	0.002(3)
C22	0.094(0)	0.097(0) 0.218(12)	0.094(3) 0.183(10)	-0.003(3)	0.037(3)	0.030(4)
C23	0.097(7)	0.210(13)	0.183(10)	0.010(7)	0.100(7)	0.072(9)
C24 C25	0.030(4)	0.033(3)	0.049(4)	-0.012(3)	0.018(3)	-0.001(3)
C25	0.084(0)	0.085(0)	0.109(0)	-0.030(3)	0.020(3)	-0.027(3)
020	0.138(9)	0.084 (7)	0.156 (9)	-0.064(6)	0.052(7)	-0.029(6)
09	0.062 (3)	0.142 (5)	0.073(3)	0.011 (3)	0.019 (3)	0.056 (3)
010	0.057(3)	0.079 (3)	0.070(3)	-0.001 (2)	0.034 (2)	0.023 (2)
011	0.085 (4)	0.114 (4)	0.051 (3)	-0.044(3)	-0.001(3)	0.011 (3)
012	0.061 (3)	0.070 (3)	0.058 (2)	-0.023 (2)	0.014 (2)	-0.003 (2)
013	0.095 (4)	0.127 (4)	0.073 (3)	-0.027 (3)	0.029 (3)	-0.055 (3)
014	0.049 (3)	0.102 (4)	0.083 (3)	-0.020 (2)	0.025 (2)	-0.025 (3)
015	0.137 (5)	0.094 (4)	0.065 (3)	-0.050(3)	0.062 (3)	-0.025 (3)
016	0.081 (3)	0.057 (3)	0.063 (3)	-0.019 (2)	0.037 (2)	0.000(2)
N3	0.039 (3)	0.042 (3)	0.053 (3)	-0.005(2)	0.019 (2)	0.004 (2)
N4	0.053 (3)	0.057 (4)	0.041 (3)	-0.006(3)	0.023 (2)	-0.003 (2)
C27	0.049 (4)	0.051 (4)	0.040 (3)	0.002 (3)	0.018 (3)	0.003 (3)
C28	0.037 (3)	0.061 (4)	0.042 (3)	-0.002 (3)	0.015 (3)	0.004 (3)
C29	0.038 (3)	0.057 (4)	0.047 (3)	0.001 (3)	0.020 (3)	0.006 (3)
C30	0.041 (3)	0.058 (4)	0.045 (3)	0.003 (3)	0.021 (3)	0.004 (3)
C31	0.054 (4)	0.069 (5)	0.047 (3)	-0.002 (3)	0.010 (3)	-0.004 (3)
C32	0.070 (4)	0.068 (5)	0.047 (3)	-0.012 (4)	0.018 (3)	0.011 (3)
C33	0.049 (4)	0.078 (5)	0.037 (3)	-0.002 (4)	0.013 (3)	0.006 (3)
C34	0.078 (5)	0.111 (7)	0.079 (5)	-0.011 (4)	0.044 (4)	0.028 (4)
C35	0.079 (6)	0.188 (10)	0.098 (6)	-0.007 (6)	0.049 (5)	0.032 (6)
C36	0.037 (4)	0.070 (6)	0.050 (4)	-0.007 (3)	0.012 (3)	-0.001 (3)
C37	0.106 (6)	0.081 (6)	0.088 (5)	-0.046 (5)	0.023 (5)	-0.008 (4)
C38	0.086 (6)	0.058 (5)	0.216 (11)	-0.019 (5)	0.031 (7)	0.005 (6)
C39	0.045 (4)	0.032 (4)	0.064 (4)	-0.002 (3)	0.025 (3)	0.003 (3)
C40	0.046 (4)	0.065 (5)	0.054 (4)	-0.004 (4)	0.026 (3)	0.006 (3)

C41	0.060 (4)	0.040 (4)	0.049 (3)	-0.006 (3)	0.029 (3)	0.001 (3)
C42	0.056 (4)	0.038 (3)	0.048 (3)	-0.011 (3)	0.025 (3)	-0.005 (3)
C43	0.046 (4)	0.040 (4)	0.044 (3)	-0.007 (3)	0.021 (3)	-0.002 (3)
C44	0.053 (4)	0.043 (4)	0.042 (3)	-0.001 (3)	0.023 (3)	0.004 (3)
C45	0.083 (5)	0.081 (5)	0.046 (4)	-0.004 (4)	0.032 (3)	0.003 (3)
C46	0.069 (4)	0.060 (4)	0.049 (3)	-0.015 (3)	0.017 (3)	0.002 (3)
C47	0.076 (5)	0.063 (5)	0.050 (4)	-0.015 (4)	0.028 (4)	-0.005 (3)
C48	0.081 (6)	0.192 (11)	0.090 (6)	-0.079 (7)	0.025 (5)	-0.036 (6)
C49	0.118 (10)	0.270 (18)	0.150 (11)	-0.095 (11)	0.007 (9)	-0.029 (11)
C50	0.059 (4)	0.062 (5)	0.052 (4)	-0.010 (3)	0.031 (3)	-0.010 (3)
C51	0.107 (6)	0.087 (6)	0.082 (5)	-0.023 (5)	0.047 (4)	0.018 (5)
C52	0.123 (7)	0.070 (6)	0.116 (7)	-0.006 (5)	0.061 (6)	0.010 (5)

### Geometric parameters (Å, °)

O1—C10	1.210 (9)	O9—C33	1.187 (8)
O2—C10	1.282 (9)	O10—C33	1.333 (8)
O2—C11	1.444 (8)	O10—C34	1.446 (7)
O3—C7	1.123 (9)	O11—C36	1.212 (8)
O4—C7	1.356 (10)	O12—C36	1.305 (8)
O4—C8	1.505 (11)	O12—C37	1.454 (8)
O5—C24	1.210 (7)	O13—C47	1.211 (9)
O6—C24	1.327 (8)	O14—C47	1.318 (9)
O6—C25	1.432 (7)	O14—C48	1.431 (8)
O7—C21	1.208 (7)	O15—C50	1.186 (8)
O8—C21	1.314 (8)	O16—C50	1.321 (8)
O8—C22	1.456 (7)	O16—C51	1.443 (8)
N1—C4	1.332 (8)	N3—C27	1.356 (7)
N1—C1	1.357 (9)	N3—C30	1.368 (8)
N1—C13	1.480 (8)	N3—C39	1.470 (8)
N2—C15	1.375 (8)	N4—C44	1.386 (8)
N2	1.399 (7)	N4—C41	1.397 (8)
N2	1.432 (8)	N4—C40	1.443 (9)
C1—C2	1.384 (10)	C27—C28	1.369 (8)
C1—C5	1.462 (9)	C27—C32	1.466 (9)
C2—C3	1.443 (9)	C28—C29	1.448 (8)
C2C10	1.482 (10)	C28—C36	1.475 (9)
C3—C4	1.386 (9)	C29—C30	1.361 (9)
C3—C7	1.486 (10)	C29—C33	1.467 (10)
C4—C6	1.456 (9)	C30—C31	1.479 (8)
C5—H5A	0.9600	C31—H31A	0.9600
С5—Н5В	0.9600	C31—H31B	0.9600
С5—Н5С	0.9600	C31—H31C	0.9600
С6—Н6А	0.9600	C32—H32A	0.9600
С6—Н6В	0.9600	C32—H32B	0.9600
С6—Н6С	0.9600	C32—H32C	0.9600
C8—C9	1.378 (15)	C34—C35	1.447 (11)
C8—H8A	0.9700	C34—H34A	0.9700

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(11) (7) (8) (9) (8) (9)
C9—H9B $0.9600$ C35—H35B $0.9600$ C9—H9C $0.9600$ C35—H35C $0.9600$ C11—C12 $1.416$ (12)C37—C38 $1.397$ C11—H1A $0.9700$ C37—H37A $0.9700$ C11—H1B $0.9700$ C37—H37B $0.9700$ C12—H12A $0.9600$ C38—H38A $0.9600$ C12—H12B $0.9600$ C38—H38B $0.9600$ C12—H12C $0.9600$ C38—H38C $0.9600$ C13—C14 $1.510$ (7)C39—C40 $1.500$ C13—H13A $0.9700$ C39—H39A $0.9700$ C13—H13B $0.9700$ C39—H39B $0.9700$ C14—H14B $0.9700$ C40—H40A $0.9700$ C15—C16 $1.359$ (8)C41—C42 $1.347$ C15—C20 $1.510$ (8)C41—C45 $1.507$ C16—C17 $1.415$ (8)C42—C43 $1.401$ C16—C21 $1.461$ (9)C42—C47 $1.455$ C17—C18 $1.366$ (8)C43—C50 $1.466$ C18—C19 $1.515$ (9) $C44$ —C46 $1.488$	(11) (11) (7) (8) (9) (8)
C9—H9C $0.9600$ $C35$ —H35C $0.9600$ C11—C121.416 (12)C37—C381.397C11—H11A $0.9700$ C37—H37A $0.9700$ C11—H11B $0.9700$ C37—H37B $0.9700$ C12—H12A $0.9600$ C38—H38A $0.9600$ C12—H12B $0.9600$ C38—H38B $0.9600$ C12—H12C $0.9600$ C38—H38C $0.9600$ C13—C14 $1.510$ (7)C39—C40 $1.500$ C13—H13A $0.9700$ C39—H39A $0.9700$ C13—H13B $0.9700$ C39—H39B $0.9700$ C14—H14A $0.9700$ C40—H40A $0.9700$ C15—C16 $1.359$ (8)C41—C42 $1.347$ C15—C20 $1.510$ (8)C41—C45 $1.507$ C16—C17 $1.415$ (8)C42—C43 $1.401$ C16—C21 $1.461$ (9)C42—C47 $1.455$ C17—C18 $1.366$ (8)C43—C50 $1.466$ C18—C19 $1.515$ (9) $C44$ —C46 $1.488$	(11) (7) (7) (8) (9) (8)
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(8) (9) (8)
C14—H14A       0.9700       C40—H40A       0.9700         C14—H14B       0.9700       C40—H40B       0.9700         C15—C16       1.359 (8)       C41—C42       1.347         C15—C20       1.510 (8)       C41—C45       1.507         C16—C17       1.415 (8)       C42—C43       1.401         C16—C21       1.461 (9)       C42—C47       1.455         C17—C18       1.366 (8)       C43—C44       1.371         C17—C24       1.453 (8)       C43—C50       1.466         C18—C19       1.515 (9)       C44—C46       1.489	(8) (9) (8)
C14—H14B       0.9700       C40—H40B       0.9700         C15—C16       1.359 (8)       C41—C42       1.347         C15—C20       1.510 (8)       C41—C45       1.507         C16—C17       1.415 (8)       C42—C43       1.401         C16—C21       1.461 (9)       C42—C47       1.455         C17—C18       1.366 (8)       C43—C44       1.371         C17—C24       1.453 (8)       C43—C50       1.466         C18—C19       1.515 (9)       C44—C46       1.489	(8) (9) (8)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(8) (9) (8) (0)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(9) (8)
C16—C17       1.415 (8)       C42—C43       1.401         C16—C21       1.461 (9)       C42—C47       1.455         C17—C18       1.366 (8)       C43—C44       1.371         C17—C24       1.453 (8)       C43—C50       1.466         C18—C19       1.515 (9)       C44—C46       1.489	(8)
C16—C21       1.461 (9)       C42—C47       1.455         C17—C18       1.366 (8)       C43—C44       1.371         C17—C24       1.453 (8)       C43—C50       1.466         C18—C19       1.515 (9)       C44—C46       1.489	(1)
C17—C18       1.366 (8)       C43—C44       1.371         C17—C24       1.453 (8)       C43—C50       1.466         C18—C19       1.515 (9)       C44—C46       1.489	. 71
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	(8)
$C18\_C19$ 1 515 (9) $C44\_C46$ 1 489	(9)
$\sqrt{10}$ $\sqrt{17}$ $\sqrt{17}$ $\sqrt{10}$	(8)
C19—H19A 0.9600 C45—H45A 0.9600	(-)
C19—H19B 0.9600 C45—H45B 0.9600	
C19—H19C 0.9600 C45—H45C 0.9600	,
C20—H20A 0.9600 C46—H46A 0.9600	,
C20—H20B 0.9600 C46—H46B 0.9600	
C20—H20C 0.9600 C46—H46C 0.9600	,
C22-C23 1.443 (12) C48-C49 1.365	(15)
C22—H22A 0.9700 C48—H48A 0.9700	(10)
C22—H22B 0.9700 C48—H48B 0.9700	
C23—H23A 0.9600 C49—H49A 0.9600	
C23—H23B 0.9600 C49—H49B 0.9600	
C23—H23C 0.9600 C49—H49C 0.9600	
$C_{25}$ — $C_{26}$ 1.485 (12) $C_{51}$ — $C_{52}$ 1.407	(11)
C25—H25A 0.9700 C51—H51A 0.9700	
C25—H25B 0.9700 C51—H51B 0.9700	,
C26—H26A 0.9600 C52—H52A 0.9600	,
C26—H26B 0.9600 C52—H52B 0.9600	,
C26—H26C 0.9600 C52—H52C 0.9600	
C10—O2—C11 117.6 (6) C33—O10—C34 115.4	(5)
C7-04-C8 118.4 (7) C36-012-C37 119.2	(5)
C24—O6—C25 117.4 (5) C47—O14—C48 115.5	6
C21—O8—C22 117.0 (5) C50—O16—C51 118.1	6
C4—N1—C1 114.1 (5) C27—N3—C30 111.4	5)
	(5)
C4—N1—C13 124.2 (5) C27—N3—C39 124.6	

C15—N2—C18	107.9 (5)	C44—N4—C41	108.3 (5)
C15—N2—C14	126.8 (5)	C44—N4—C40	125.4 (5)
C18—N2—C14	125.3 (5)	C41—N4—C40	126.4 (5)
N1—C1—C2	106.1 (5)	N3—C27—C28	106.9 (5)
N1—C1—C5	125.6 (6)	N3—C27—C32	123.0 (6)
C2—C1—C5	128.2 (6)	C28—C27—C32	130.0 (6)
C1—C2—C3	106.2 (6)	C27—C28—C29	107.6 (6)
C1—C2—C10	124.2 (6)	C27—C28—C36	124.3 (6)
C3—C2—C10	129.2 (7)	C29—C28—C36	127.4 (7)
C4—C3—C2	108.0 (6)	C30—C29—C28	106.6 (6)
C4—C3—C7	124.0 (6)	C30—C29—C33	124.9 (6)
C2—C3—C7	127.8 (7)	C28—C29—C33	128.3 (6)
N1-C4-C3	105.6 (5)	$C_{29}$ $C_{30}$ N <sub>3</sub>	107.5 (5)
N1-C4-C6	125.5 (6)	$C_{29} = C_{30} = C_{31}$	128.5 (6)
C3-C4-C6	128.9 (6)	N3-C30-C31	123.8 (6)
C1C5H5A	109 5	C30—C31—H31A	109 5
C1	109.5	$C_{30}$ $C_{31}$ $H_{31B}$	109.5
H5A-C5-H5B	109.5	H31A-C31-H31B	109.5
C1 - C5 - H5C	109.5	$C_{30}$ $C_{31}$ $H_{31C}$	109.5
$H_{5A}$ $C_{5}$ $H_{5C}$	109.5	$H_{31}A = C_{31} = H_{31}C$	109.5
H5B-C5-H5C	109.5	$H_{31B}$ $C_{31}$ $H_{31C}$	109.5
C4-C6-H6A	109.5	$C_{27}$ $C_{32}$ $H_{32A}$	109.5
C4-C6-H6B	109.5	$C_{27} = C_{32} = H_{32R}$	109.5
H6A - C6 - H6B	109.5	$H_{32}A = C_{32} = H_{32}B$	109.5
C4-C6-H6C	109.5	$C_{27}$ $C_{32}$ $H_{32C}$	109.5
H6A - C6 - H6C	109.5	$H_{32}A = C_{32} = H_{32}C$	109.5
H6B_C6_H6C	109.5	H32B_C32_H32C	109.5
03-C7-04	121.0 (8)	09-033-010	107.5 122.5(7)
03-07-03	127.7(8)	09-033-010	122.3(7) 124.3(7)
03 - 07 - 03	127.7(0) 111 1(7)	$0_{3} - 0_{3} - 0_{2}$	124.3(7) 1130(6)
$C_{1}^{0} C_{2}^{0} C_{3}^{0}$	100.4(10)	010  C34  C35	107.7(7)
$C_{0}$ $C_{8}$ $H_{8A}$	109.4 (10)	010  C34  H34A	110.2
$C_{2} = C_{3} = H_{3} A$	109.8	$C_{35}$ $C_{34}$ $H_{34A}$	110.2
$C_{1}$ $C_{2}$ $C_{3}$ $H_{2}$ $H_{2}$	109.8	$C_{33} - C_{34} - H_{34} - H$	110.2
$C_{2} = C_{3} = H_{3}B$	109.8	$C_{35} = C_{34} = H_{34B}$	110.2
	109.8	H24A C24 H24B	10.2
	100.5	$C_{34}$ $C_{35}$ $H_{35A}$	100.5
	109.5	$C_{34} = C_{35} = H_{35R}$	109.5
	109.5	H25A C25 H25B	109.5
	109.5	$C_{24}$ $C_{25}$ $H_{25}$ $H_{25}$	109.5
	109.5	$H_{254} = C_{25} = H_{25}C$	109.5
	109.5	$H_{25R} = C_{25} = H_{25C}$	109.5
$119D - C_{2} - 119C$	109.5	1135B - C35 - 1135C	109.5
01 - 010 - 02	121.0(7) 123.7(8)	011 - 036 - 012	121.9(0) 124.6(7)
$0^{-}$ $0^{-$	123.7(0) 115.2(6)	012 C36 C28	124.0(7) 1125(6)
$C_1^{-10} = C_2^{-10} = C_2^{-10}$	113.2(0) 108.7(7)	$C_{12} = C_{30} = C_{20}$	110.5(0) 110.6(7)
$C_{12} = C_{11} = C_{2}$	110.7 (7)	$C_{38} C_{37} U_{27} M_{27}$	100.5
$C_{12}$ $C_{11}$ $H_{11A}$	110.0	$C_{30} - C_{37} - H_{37} A$	109.5
02 - 011 - 011A	110.0	$U12 - U3 / - \Pi3 / A$	109.3

C12—C11—H11B	110.0	С38—С37—Н37В	109.5
O2—C11—H11B	110.0	О12—С37—Н37В	109.5
H11A—C11—H11B	108.3	H37A—C37—H37B	108.1
C11—C12—H12A	109.5	C37—C38—H38A	109.5
C11—C12—H12B	109.5	C37—C38—H38B	109.5
H12A—C12—H12B	109.5	H38A—C38—H38B	109.5
C11—C12—H12C	109.5	С37—С38—Н38С	109.5
H12A—C12—H12C	109.5	H38A—C38—H38C	109.5
H12B—C12—H12C	109.5	H38B—C38—H38C	109.5
N1—C13—C14	111.0 (4)	N3—C39—C40	111.8 (4)
N1—C13—H13A	109.4	N3—C39—H39A	109.3
С14—С13—Н13А	109.4	С40—С39—Н39А	109.3
N1—C13—H13B	109.4	N3—C39—H39B	109.3
C14—C13—H13B	109.4	С40—С39—Н39В	109.3
H13A—C13—H13B	108.0	H39A—C39—H39B	107.9
N2—C14—C13	112.6 (5)	N4—C40—C39	112.0 (5)
N2—C14—H14A	109.1	N4—C40—H40A	109.2
C13—C14—H14A	109.1	C39—C40—H40A	109.2
N2—C14—H14B	109.1	N4—C40—H40B	109.2
C13—C14—H14B	109.1	C39—C40—H40B	109.2
H14A—C14—H14B	107.8	H40A—C40—H40B	107.9
C16-C15-N2	108.8 (5)	C42-C41-N4	107.9(5)
$C_{16} - C_{15} - C_{20}$	131.4 (6)	C42 - C41 - C45	133.2 (6)
N2-C15-C20	119.6 (6)	N4—C41—C45	118.9 (6)
$C_{15}$ $C_{16}$ $C_{17}$	107.8 (6)	C41 - C42 - C43	108.5(5)
$C_{15}$ $C_{16}$ $C_{21}$	122.4 (5)	C41 - C42 - C47	122.3 (6)
C17 - C16 - C21	129.6 (5)	C43 - C42 - C47	122.3 (6)
C18 - C17 - C16	107.6 (5)	C44 - C43 - C42	120.0(0) 108.2(5)
C18 - C17 - C24	123.7 (6)	C44-C43-C50	121.6 (6)
$C_{16} - C_{17} - C_{24}$	128.0 (6)	C42 - C43 - C50	129.5 (6)
C17 - C18 - N2	107.9 (5)	C43—C44—N4	107.2 (5)
C17 - C18 - C19	132.5 (5)	C43—C44—C46	132.2(5)
$N_{2}$ C18 C19	119.5 (6)	N4—C44—C46	120.6(5)
C18—C19—H19A	109 5	C41—C45—H45A	109.5
C18—C19—H19B	109.5	C41—C45—H45B	109.5
H19A—C19—H19B	109.5	H45A—C45—H45B	109.5
C18—C19—H19C	109.5	C41—C45—H45C	109.5
H19A—C19—H19C	109.5	H45A—C45—H45C	109.5
H19B—C19—H19C	109.5	H45B—C45—H45C	109.5
C15—C20—H20A	109.5	C44—C46—H46A	109.5
C15—C20—H20B	109.5	C44—C46—H46B	109.5
H20A—C20—H20B	109.5	H46A—C46—H46B	109.5
C15—C20—H20C	109.5	C44—C46—H46C	109.5
H20A—C20—H20C	109.5	H46A—C46—H46C	109.5
H20B—C20—H20C	109.5	H46B—C46—H46C	109.5
07-C21-O8	122.4 (6)	O13—C47—O14	123.9 (7)
O7—C21—C16	124.4 (7)	O13—C47—C42	123.8 (8)
O8—C21—C16	113.2 (5)	O14—C47—C42	112.3 (6)

C23—C22—O8	109.8 (7)	C49—C48—O14	110.0 (8)
C23—C22—H22A	109.7	C49—C48—H48A	109.7
O8—C22—H22A	109.7	O14—C48—H48A	109.7
С23—С22—Н22В	109.7	C49—C48—H48B	109.7
O8—C22—H22B	109.7	O14—C48—H48B	109.7
H22A—C22—H22B	108.2	H48A—C48—H48B	108.2
C22—C23—H23A	109.5	C48—C49—H49A	109.5
C22—C23—H23B	109.5	C48—C49—H49B	109.5
H23A—C23—H23B	109.5	H49A—C49—H49B	109.5
C22—C23—H23C	109.5	C48—C49—H49C	109 5
$H_{23}A = C_{23} = H_{23}C$	109.5	H49A - C49 - H49C	109.5
$H_{23B} = C_{23} = H_{23C}$	109.5	H49B - C49 - H49C	109.5
05 C24 06	107.5	$\begin{array}{c} 11470 \\ -247 \\ -11470 \\ -247 \\ -11470 \\ -247$	107.5
05 - 024 - 017	122.9 (0)	015 - C50 - C43	121.2(0)
05 - 024 - 017	125.5(0)	015 - 050 - 043	127.1(0)
06 - 024 - 017	111.3(0) 107.2(7)	010 - 030 - 043	111.0(3)
06 - 025 - 025	107.2 (7)	$C_{52} = C_{51} = 0.16$	111.5 (7)
06—C25—H25A	110.3	С52—С51—Н51А	109.4
С26—С25—Н25А	110.3	O16—C51—H51A	109.4
O6—C25—H25B	110.3	C52—C51—H51B	109.4
С26—С25—Н25В	110.3	O16—C51—H51B	109.4
H25A—C25—H25B	108.5	H51A—C51—H51B	108.0
C25—C26—H26A	109.5	C51—C52—H52A	109.5
C25—C26—H26B	109.5	C51—C52—H52B	109.5
H26A—C26—H26B	109.5	H52A—C52—H52B	109.5
С25—С26—Н26С	109.5	С51—С52—Н52С	109.5
H26A—C26—H26C	109.5	H52A—C52—H52C	109.5
H26B—C26—H26C	109.5	H52B—C52—H52C	109.5
C4—N1—C1—C2	0.0 (8)	C30—N3—C27—C28	-1.1(7)
C13—N1—C1—C2	179.5 (6)	C39—N3—C27—C28	-178.5 (6)
C4—N1—C1—C5	-178.7 (7)	C30—N3—C27—C32	177.2 (7)
C13 - N1 - C1 - C5	0.8 (11)	$C_{39}$ N3 $C_{27}$ C32	-0.1(10)
N1-C1-C2-C3	-0.8(8)	N3-C27-C28-C29	0.7(7)
$C_{5}$ $C_{1}$ $C_{2}$ $C_{3}$	177 9 (8)	$C_{32}$ $C_{27}$ $C_{28}$ $C_{29}$	-1775(7)
$N_1 - C_1 - C_2 - C_{10}$	-1741(7)	$N_{3}$ $C_{27}$ $C_{28}$ $C_{36}$	171.8 (6)
$C_5 C_1 C_2 C_{10}$	1/4.1(7)	$C_{32}$ $C_{27}$ $C_{28}$ $C_{36}$	-6.4(11)
$C_{1} = C_{2} = C_{10}$	1.3(8)	$C_{22} = C_{23} = C_{23} = C_{30}$	0.4(11)
$C_1 = C_2 = C_3 = C_4$	1.3(8) 1741(8)	$C_{27} = C_{28} = C_{29} = C_{30}$	-170.8(7)
C10-C2-C3-C4	1/4.1(6) 175.0(8)	$C_{30} = C_{20} = C_{30} = C_{30}$	-170.8(7)
C1 - C2 - C3 - C7	1/5.9 (8)	$C_2/-C_{28}-C_{29}-C_{33}$	-1/6.4(7)
C10 - C2 - C3 - C/	-11.2(13)	$C_{36} = C_{28} = C_{29} = C_{33}$	12.9 (12)
C1—N1—C4—C3	0.8 (8)	C28—C29—C30—N3	-0.6 (7)
C13—N1—C4—C3	-178.7 (6)	C33—C29—C30—N3	175.9 (7)
C1—N1—C4—C6	-176.8 (7)	C28—C29—C30—C31	-176.1 (7)
C13—N1—C4—C6	3.7 (11)	C33—C29—C30—C31	0.4 (11)
C2—C3—C4—N1	-1.3 (7)	C27—N3—C30—C29	1.1 (7)
C7—C3—C4—N1	-176.2 (7)	C39—N3—C30—C29	178.5 (6)
C2—C3—C4—C6	176.2 (8)	C27—N3—C30—C31	176.9 (6)
C7—C3—C4—C6	1.3 (12)	C39—N3—C30—C31	-5.8 (10)

C8—O4—C7—O3	-12.6 (15)	C34—O10—C33—O9	5.2 (11)
C8—O4—C7—C3	172.6 (8)	C34—O10—C33—C29	-180.0 (6)
C4—C3—C7—O3	-31.7 (16)	C30—C29—C33—O9	46.6 (11)
C2—C3—C7—O3	154.5 (11)	C28—C29—C33—O9	-137.6 (8)
C4—C3—C7—O4	142.8 (7)	C30-C29-C33-O10	-128.1 (7)
C2—C3—C7—O4	-31.1 (12)	C28—C29—C33—O10	47.7 (10)
C7—O4—C8—C9	176.5 (10)	C33—O10—C34—C35	-177.7 (7)
C11—O2—C10—O1	-8.6 (13)	C37—O12—C36—O11	2.0 (11)
C11—O2—C10—C2	174.0 (7)	C37—O12—C36—C28	-178.6(6)
C1-C2-C10-O1	-34.0 (13)	C27—C28—C36—O11	24.6 (11)
$C_{3}$ $C_{2}$ $C_{10}$ $C_{10}$	154 3 (9)	$C_{29}$ $C_{28}$ $C_{36}$ $-011$	-1661(7)
C1 - C2 - C10 - O2	143 3 (8)	$C_{27}$ $C_{28}$ $C_{36}$ $O_{12}$	-154.7(6)
$C_{3}$ $C_{2}$ $C_{10}$ $O_{2}$	-284(12)	$C_{29}$ $C_{28}$ $C_{36}$ $C_{12}$	145(10)
$C_{10} = 0^{2} = C_{11} = C_{12}$	178 7 (8)	$C_{25} = C_{20} = C_{30} = C_{12}$	-176.6(8)
$C_{10} = 02 = C_{11} = C_{12}$	-98.2(6)	$C_{27} N_3 C_{39} C_{40}$	-835(7)
$C_{1} = N_{1} = C_{13} = C_{14}$	98.2 (0) 82.3 (7)	$C_{27} = N_{3} = C_{39} = C_{40}$	83.3(7)
CI = NI = CI3 = CI4	02.5(7)	$C_{30} = 103 = C_{39} = C_{40}$	99.5 (0)
C13 - N2 - C14 - C13	-95.1(7)	C44 - N4 - C40 - C39	-81.7(7)
C18 - N2 - C14 - C13	84.4 (7)	C41 - N4 - C40 - C39	97.3(7)
N1 - C13 - C14 - N2	1//.8 (6)	N3-C39-C40-N4	-180.0 (6)
C18 - N2 - C15 - C16	0.8 (7)	C44—N4—C41—C42	-0.5 (7)
C14—N2—C15—C16	-1/9.7 (6)	C40—N4—C41—C42	-179.7 (6)
C18—N2—C15—C20	-175.6 (6)	C44—N4—C41—C45	176.3 (6)
C14—N2—C15—C20	4.0 (10)	C40—N4—C41—C45	-2.9 (10)
N2—C15—C16—C17	-0.9 (7)	N4—C41—C42—C43	1.5 (7)
C20-C15-C16-C17	174.9 (7)	C45—C41—C42—C43	-174.7 (7)
N2—C15—C16—C21	-176.2 (6)	N4—C41—C42—C47	174.4 (6)
C20-C15-C16-C21	-0.4 (11)	C45—C41—C42—C47	-1.7 (12)
C15—C16—C17—C18	0.7 (7)	C41—C42—C43—C44	-1.9 (7)
C21—C16—C17—C18	175.5 (7)	C47—C42—C43—C44	-174.3 (7)
C15—C16—C17—C24	171.3 (7)	C41—C42—C43—C50	-172.0 (7)
C21—C16—C17—C24	-13.8 (12)	C47—C42—C43—C50	15.6 (12)
C16—C17—C18—N2	-0.2 (7)	C42—C43—C44—N4	1.5 (7)
C24—C17—C18—N2	-171.4 (6)	C50—C43—C44—N4	172.6 (6)
C16—C17—C18—C19	176.3 (7)	C42—C43—C44—C46	-177.1 (7)
C24—C17—C18—C19	5.1 (11)	C50—C43—C44—C46	-6.0 (11)
C15—N2—C18—C17	-0.3(7)	C41—N4—C44—C43	-0.6(7)
C14 - N2 - C18 - C17	-179.9(6)	C40 - N4 - C44 - C43	178.5 (6)
$C_{15} N_{2} C_{18} C_{19}$	-1774(6)	$C_{41}$ N4 $C_{44}$ C46	178.2 (6)
C14 N2 C18 C19	30(9)	C40—N4— $C44$ — $C46$	-2.7(10)
$C_{22}^{22} = 08 = C_{21}^{21} = 07$	-1.9(10)	$C_{48} - 014 - C_{47} - 013$	30(12)
$C_{22} = 08 = C_{21} = 07$	1.9 (10)	$C_{48} = 014 = C_{47} = 013$	-175.0(7)
$C_{22} = 08 = C_{21} = C_{10}$	-54.0(10)	$C_{40} = 014 = C_{47} = C_{42}$	173.9(7)
$C_{13}$ $C_{10}$ $C_{21}$ $C_{10}$ $C_{21}$ $C_{10}$ $C_{21}$ $C_{10}$ $C_{21}$ $C$	34.0(10) 121.9(9)	$C_{41} = C_{42} = C_{47} = C_{13}$	+7.1(11) -120 4 (9)
$C_{1} = C_{10} = C_{21} = O/$	131.0(0) 135.2(7)	$C_{43} - C_{42} - C_{47} - O_{13}$	$-139.4(\delta)$
C13 - C10 - C21 - O8	123.2(7)	$C_{41} - C_{42} - C_{47} - O_{14}$	-131.9(7)
$C_1/-C_{10}-C_{21}-O_{8}$	-49.0 (9)	C43 - C42 - C47 - O14	39.3 (10) 162.8 (11)
$C_{21} = 08 = C_{22} = C_{23}$	1/1.4 (8)	C4/-O14-C48-C49	163.8 (11)
C25—O6—C24—O5	-5.4 (11)	C51—O16—C50—O15	8.7 (11)
C25—O6—C24—C17	179.3 (6)	C51—O16—C50—C43	-175.2 (6)

C18—C17—C24—O5	-23.1 (11)	C44—C43—C50—O15	28.1 (12)
C16—C17—C24—O5	167.7 (7)	C42—C43—C50—O15	-163.0 (8)
C18—C17—C24—O6	152.1 (6)	C44—C43—C50—O16	-147.8 (6)
C16—C17—C24—O6	-17.2 (10)	C42—C43—C50—O16	21.2 (10)
C24—O6—C25—C26	-173.5 (7)	C50—O16—C51—C52	-173.6 (7)